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*Shown with accessory touch tone pad

Top view showing controls

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TEMPO PRESENTS THE WORLD'S FIRST SYNTHESIZED 800 CHANNEL HAND HELD TRANSCEIVER

This amazing pocket sized radio represents the year's biggest breakthrough in 2-meter communications.

Other units that are larger, heavier and are similarly priced can offer only 6 channels. The SYNCOM'S price includes the battery pack, charger, and a telescoping antenna. But, far more important is the 800 channels offered by the S1.

The optional touch tone pad adds greatly to its convenience and the addition of a Tempo solid state amplifier adds tremendously to its power.

SPECIFICATIONS

Frequency Coverage:	144 to 148 MHz
Channel Spacing:	Receive every 5 kHz, transmit Simplex or +600 kHz
Power Requirements:	9.6 VDC
Current Drain:	17 ma-standby 500 ma-transmit
Batteries:	8 pieces ni-cad battery included
Antenna Impedance:	50 ohms
Dimensions:	40 mm x 62 mm x 165 mm (1.6" x 2.5" x 6.5")
RF Output:	Better than 1.5 watts
Sensitivity:	Better than .5 microvolts

SUPPLIED ACCESSORIES

Telescoping whip antenna, ni-cad battery pack, charger.

OPTIONAL ACCESSORIES

Touch tone pad: $55 • Tone burst generator: $29.95 • CTCSS sub-audible tone control: $29.95 • Rubber flex antenna: $8 • Leather holster: $16 • Cigarette lighter plug mobile charging unit: $6 • Matching 30 watt output 13.8 VDC power amplifier (S30): $89 • Matching 80 watt output power amplifier (S80): $149

Price... $349.00 With touch tone pad... $399.00

The Tempo line also features a fine line of extremely compact UHF and VHF pocket receivers. They're low priced, dependable, and available with CTCSS and 2-tone decoders

The Tempo FMT-2 & FMT-42 (UHF) provides excellent mobile communications and features a remote control head for hide-away mounting.

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30W	130W	130A30	$199
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30W	80W	80A30	$159
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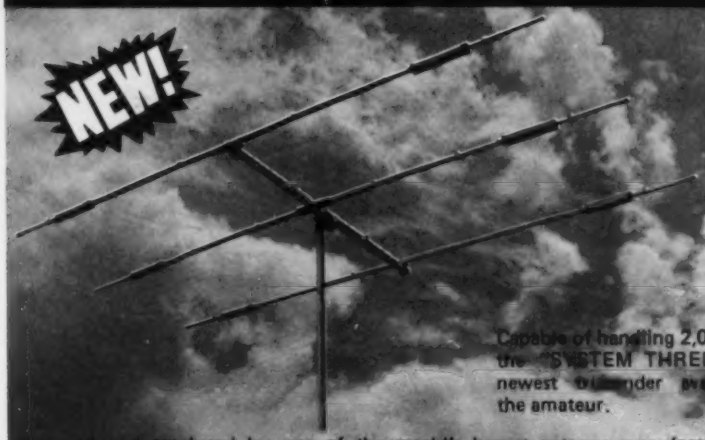
Top Performance for 20 - 15 - 10 Meters!



Capable of handling 2,000 watts, the "SYSTEM THREE" is the newest tribander available to the amateur.

Wilson

SY-3

SPECIFICATIONS

Band MHz	14-21-28
Maximum power input	Legal limit
Gain (dBd)	8 dB
VSWR at resonance	1.3:1
Impedance	50 ohms
F/B ratio	20 dB
Boom (O.D. x length)	2" x 14' 4"
No. of elements	3
Longest element	27' 4"
Turning radius	15' 9"
Maximum mast diameter	2" O.D.
Surface area	5.7 sq. ft.
Wind loading at 80 mph	114 lbs.
Assembled weight (approx.)	37 lbs.
Shipping weight (approx.)	42 lbs.
Direct 52 ohm feed or balun	
Maximum wind survival	100 mph

Designed and produced by one of the world's largest antenna manufacturers, the traditional quality of workmanship and materials continues on with the "SYSTEM THREE". The special heavy-duty vise-like extruded aluminum clamps on the reflector and director are a key point in the design of strength and durability. Superior clamping power is obtained with the use of a rugged ¼" thick aluminum plate for boom to mast mounting. The use of large diameter High-Q Traps in the "SYSTEM THREE" makes it a high performing tri-bander with a very economical price. A complete step-by-step illustrated instruction manual guides you to easy assembly and the lightweight antenna makes installation of the "SYSTEM THREE" quick and simple.

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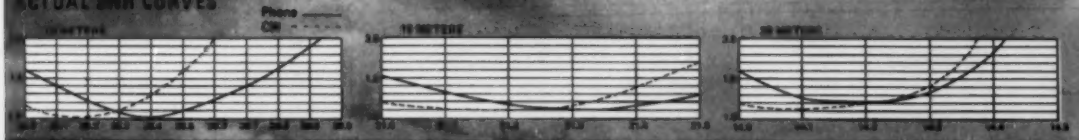
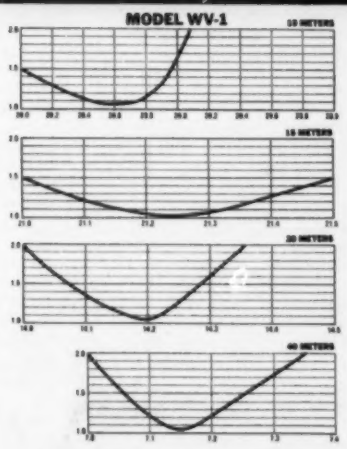


40 THRU 10 METERS VERTICAL TRAP



WV-1 WILSON VERTICAL TRAP ANTENNA

No bandswitching necessary with this vertical. An excellent low cost DX antenna with an electrical quarter wavelength on each band and low angle radiation. Advanced design provides low SWR and exceptionally flat response across full width of each band. Featured is the Wilson large diameter High-Q traps which will maintain resonant points with varying temperatures and humidity. Easily assembled, the WV-1 is supplied with base mount bracket to attach to vent pipe or to mast driven in the ground. The new WV-1 Antenna is value priced . . . and ships via UPS!

SPECIFICATIONS

Input Impedance: 50 ohms • Powerhandling capability: Legal Limit • Two High-Q Traps with large diameter coils • Low Angle Radiation Omnidirectional performance • Taper Swaged Aluminum Tubing • Automatic Bandswitching • Mast Bracket furnished • SWR: 1.1:1 on all Bands • 1½" O.D. heavy wall aluminum tubing • Does not require guying • Overall length: 19' 8".

W2

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NEVER SAY DIE
editorial by Wayne Green

ATLANTA IN JUNE

Dayton is still the largest hamfest in the country, but Atlanta is undoubtedly the second largest—and closing in on Dayton. Atlanta has two major pluses and one minor plus which Dayton doesn't have. The biggest plus is the city of Atlanta, with its incredible variety of entertainment and restaurants. That in itself is worth the visit. The second big plus is the masterful planning and enthusiasm of Chaz Cone W4GKF, the magician who has put this show together.

Chaz, with the help of co-chairman Bob Verlander W4BCD, has organized a fast-paced and well-run show. They get the best in exhibits and somehow manage to bring in standing-room-only crowds for the forums. Perhaps it is the number and quality of the prizes that are responsible for keeping the place packed, even on Sunday. This is the *only* hamfest I've ever seen where it is even more packed on Sunday than on Saturday.

The minor plus, at least to some of us, is that I have an opportunity to speak in Atlanta . . . which I don't at Dayton. Last year at Atlanta, I held one session on current events in amateur radio and another on current events in microcomputing. I expect I'll be doing the same this year.

My ham session might be a good place for ARRL cultists to come to discover what many amateurs already know . . . that I don't hate the ARRL. It may be time to bring this out in the open and talk about it. You know, it's funny about that . . . when I'm critical of the FCC, everyone nods in agreement, and I don't hear any cries of anguish about me being anti-FCC. When I'm critical of our government, I don't get anything but agreement. When I'm critical of the League, then I'm "slamming" them. Baloney. Why should the League be a sacred cow, with people having apoplexy at criticism? Is the ARRL a religion? Let's put these things into perspective and not let a cult mind rule out intelligent discussion of ham events.

Sure, I suppose I should be more political and not so direct. If you don't offend anyone, you have no enemies . . . but neither have you any share in the satisfaction of helping to improve the world a notch. When I see something wrong, I speak out and try to do something about it, a trait which makes politicians nervous. I speak out about the government, about the FCC, the ARRL, civil defense, and anything else where I see things going wrong. Yes, and I expect to get stoned for my trouble . . . though I don't enjoy it. Can you name one person who has spoken out who didn't make people angry?

One of the things I believe in is amateur radio. I believe that our hobby is one of the reasons why the United States is so outstanding in electronics and communications. Over a million of the people in this country have been hams at one time or another, and this personal spark of self-interest sets them aside from the strictly professional technician or engineer. A ham will usually go that extra distance to get something done, while the "professional" knocks off at 5:00 pm to go home and watch television.

Amateur radio has changed the lives of these million kids . . . and the course of events for our country. Just look at the amazing correlation between the development of foreign countries and the number of their hams listed in the *Callbook* . . . do you really think that is a coincidence? We all know that hams discovered and pioneered most of the presently-used radio techniques . . . and would have worked out a lot more if they hadn't had the FCC fighting them at every turn for years.

Whether amateur radio means rag chewing, building special projects, civil defense, emergency nets, contests, DX-ing, repeaters . . . whatever it means, I feel that amateurs are part of a special breed which is very important to the world. Before you put down the jerk who sits there clunking the repeater, remember that with the right motivation this fellow may suddenly get into some special interest in amateur radio and pioneer a whole new mode of communications. I try to provide as much of this spark as I can with the articles in *73*.

When I hear or read that I'm trying to tear down amateur radio, I wonder who could possibly believe such bunk. I've built most of my life around amateur radio for the last 25 years . . . and that *is* most of my life. I've made it my business to keep up with just about everything going on and the people involved. I've participated with enthusiasm in just about every phase of the hobby, starting out back in the 1930s with CW on 40m and 2½m VHF work. I've been into DXing, DXpeditioning, contests, RTTY, SSB, and SSTV, got into FM and repeaters in the 60s with my own repeater, and have a reasonable score via OSCAR in mode B (the hard one). No, I'm not about to tear down amateur radio.

Come to Atlanta, and let's get together to see if we all aren't

Continued on page 166

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- UNLOCK indicator...an LED that indicates transceiver protection when the frequency selector switches are improperly positioned or the PLL is not locked.

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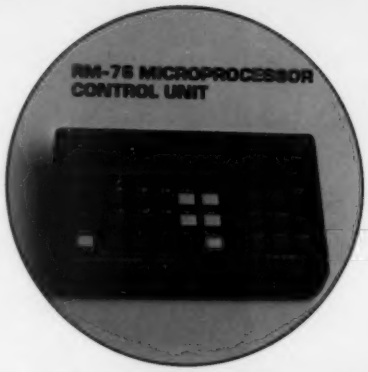
- Scan for busy or open channel.
- Display indicates frequency (even while scanning) and functions (such as auto-scan, lower scan frequency limit, upper scan limit, and error, i.e. transmitting out of band).



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RTTY Loop

Marc I. Leavey, M.D. WA3AJR
4006 Winlee Road
Randallstown MD 21133

Last month we started to investigate the design and construction of one type of RTTY "stunt box." Over the next few sessions, I hope to fully explain a solid-state way to generate any desired RTTY code sequence.

Fig. 1 is a reminder of what we are talking about. The desired data is encoded in some manner and passed in an intelligent manner to a device which puts it out in the standard format. Understanding how that data is encoded is this month's goal.

Consider the circuit in Fig. 2. Each light is connected to one vertical matrix conductor. Forming a grid with these three are an equal number of horizontal conductors. Each horizontal is connected to one, and only one, vertical member. It should be fairly obvious that grounding any numbered horizontal conductor will cause the circuit of the corresponding bulb to be completed and the lamp to light. So far, so good, OK? Now, just suppose that I want *both* lights one and three to light, with one switch action. If I add another horizontal, as pictured in Fig. 3, then grounding that wire, number four, will certainly accomplish the required task. But the dotted arrow demonstrates the current path when wire number one is grounded alone. A path to light three still exists, through that extra wire, and it will continue to light. Clearly, what we need are little one-way valves at each junction which will let current flow one way but not the other.

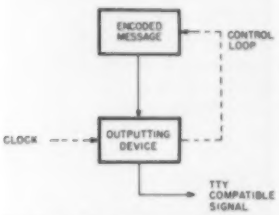

Fig. 1. Block diagram of "stunt box."

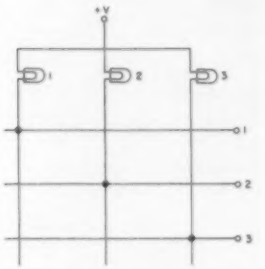

Fig. 2. One kind of matrix.

73
Study Guides and Code Tapes — The Best Available
see page 204

After spending a few hours at the hardware store looking for such a valve and leaving empty-handed, I wandered into the Radio Shack next door. There I found just the ticket, little tiny chunks of silicon and germanium—*diodes*! Seriously, though, recall that one of the many uses of diodes is as switches. Also, note that conventional current flow, a la Benny Franklin, is from positive to negative and is represented in the diode symbol by the direction of the arrow.

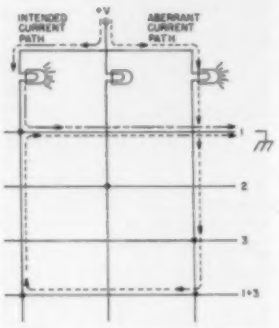

Fig. 3. A matrix with a problem.

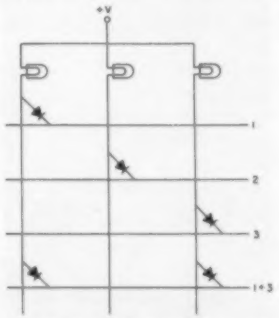

Fig. 4. The solution to the problem.

Now let's replace each of the direct connections shown in Fig. 3 with a diode, oriented so that the "arrow" points to ground. Fig. 4 shows what I mean. Grounding wire one will now light only light bulb one, and wire four lights only one and three. The current path shown previously no longer exists; it is blocked by the diodes used as one-way valves at the matrix junctions. Take my word for it that in a properly-designed matrix, no other aberrant pathways will exist, either.

What we have constructed here is called a *diode matrix*, for what should by now be obvious reasons, and, although a three-by-four matrix is diagrammed, it is certainly not the most useful item in the world. I hope you can see, however, how one uses the matrix to individually select any of a set of possible outputs, encoded by strategically located diodes. By increasing the number of columns to five, the Baudot code can be represented. As many rows as needed may be provided for, one row per character. Encoding will place a diode in the matrix for each space bit in each character. The table in Fig. 5 shows where diodes go, represented by "X", for each character.

Now all you need to do is decide on a message, like "DE WA3AJR MARC," that you would like to encode, and construct a matrix as shown in Fig. 6. Note particularly the need for a FIGS and LTRS around the "3". Since LTRS is all marks, no diodes are needed, and any blanks come out as LTRS. Neat, huh? Next month we will see what we can do with data encoded in this fashion.

LTRS	FIGS	1	2	3	4	5
A	-			X	X	X
B	?		X	X		
C	:	X				X
D	$		X	X		X
E	3		X	X	X	X
F	!		X			X
G	&	X		X		
H	stop	X	X		X	
I	8	X			X	X
J	'			X		X
K	(					X
L	)	X		X	X	
M	.	X	X			
N	,		X	X		X
O	9	X	X	X		
P	0	X			X	
Q	1				X	
R	4	X		X		X
S	bell		X		X	X
T	5	X	X	X	X	
U	7				X	X
V	;	X				
W	2			X	X	
X	/		X			
Y	6		X		X	
Z	"		X	X	X	
BLANK		X	X	X	X	X
LETTERS						
FIGURES				X		
CAR RET		X	X	X		X
LIN FEED		X		X	X	X
SPACE		X	X		X	X

Fig. 5. Diode encoding.

While I won't say that I have been inundated with response to my question on what kind of RTTY gear you all are running out there, preliminary returns have been quite interesting. Model 15s, 28s, and 32s appear to be represented, along with a smattering of Kleinschmidts. Those of you who are into microcomputers are using everything from 8080s to 6800s, Altairs, SWTPCs, and Digital Groups. I am going to let the survey run a bit longer before trying to compile a meaningful list, but it looks good.

Several of you have sent little notes regarding RTTY art. While there are quite a few pictures and such on the air over the winter holiday season, newcomers who want to obtain a few, or those who want a particular one, may need an alternate source. Well, a few days ago, I received a catalog from a firm called Teleprinter Art, Ltd. Perusing it revealed listings for all kinds of RTTY art, everything from portraits (JFK, FDR, LBJ, Ike, or whoever), nudes, cartoon characters, and holidays. Prices are reasonable enough, with many items under a dollar, almost all under two. If you are interested, drop them a line at: Teleprinter Art, Ltd., 601 S. Dodson, Urbana, Illinois 61801. Tell them you saw it here, in RTTY Loop, OK?

Next month we will get into putting the data, as encoded by our matrix, out to the TTY loop. For this we will use a device known as a UART. If that word is totally foreign to you, you have one month to study! 'Til then, BCNU on RTTY!

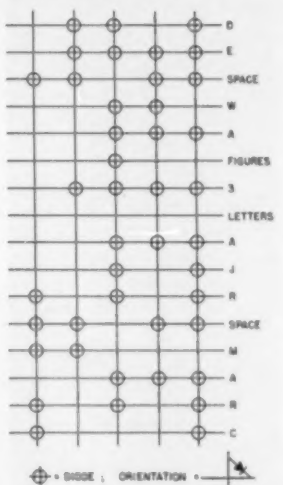

Fig. 6. A sample message.

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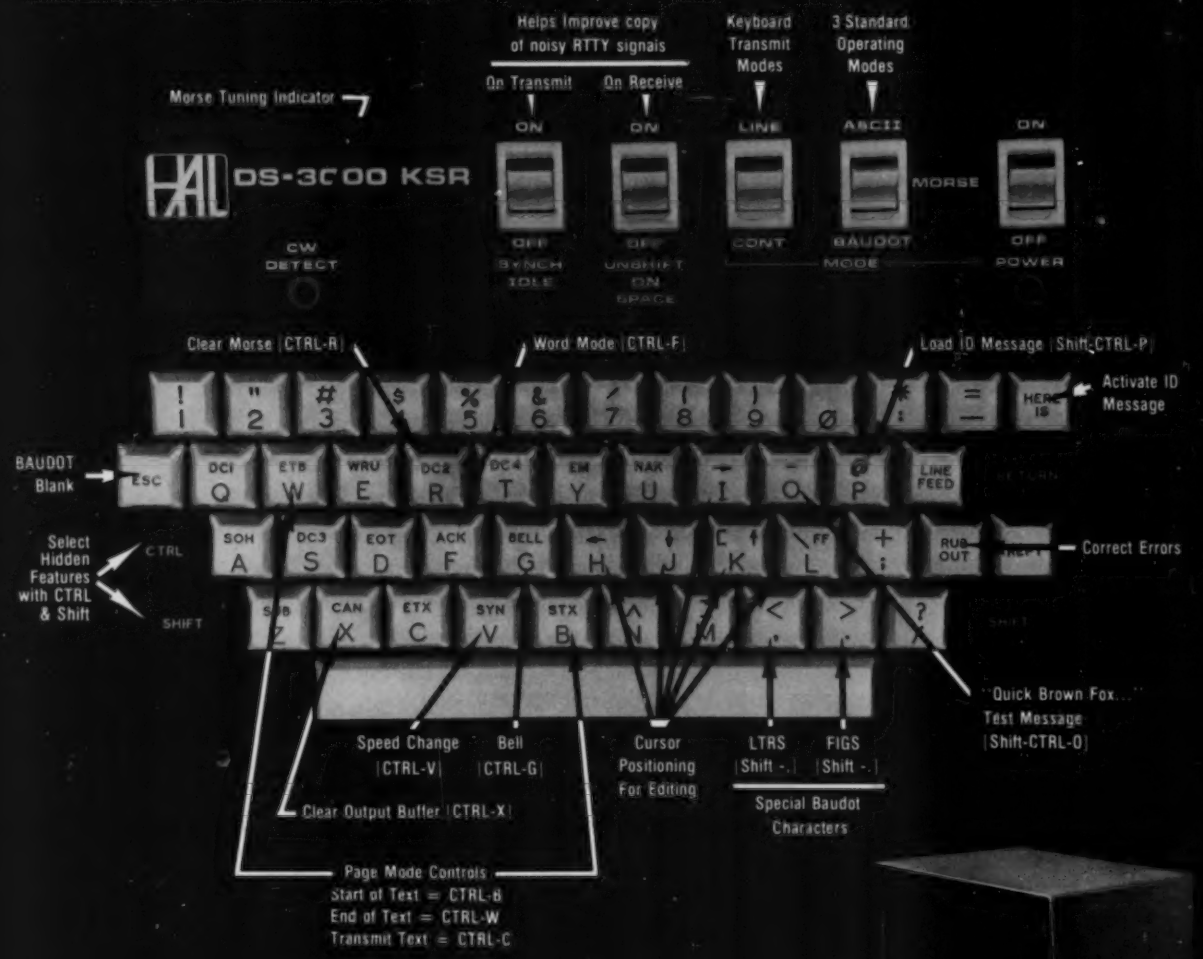

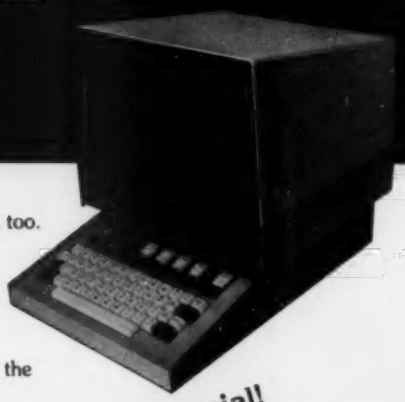

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3550W	50Hz - 550MHz	1 PPM 65° - 85°F	25MV	25MV	75MV	8	.5 Inch	115VAC or 8.2 - 14.5VDC	2¼"H x 8"W x 5"D

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DX PROFILE

Herb Lehmann WA6BJS of San Carlos, California, is best known to most of us as the gravel-voiced, no-nonsense MC of the fifteen meter Afrikaner Net.

Herb's first exposure to the mysteries of shortwave radio came in 1916 when, at the tender age of only eight years, a neighbor acquired a commercial crystal set which he shared with Herb. But before long, World War I came along and all antennas had to be removed.

In 1920, Herb's interest in radio was renewed when a friend asked Herb to accompany him to town to purchase some transmitter parts. Shortly thereafter, Herb acquired some #18 enameled wire, a Quaker Oats box, two square brass rods with two-inch sleeves which he cut into sliders, a suspender clip swiped from his grandpa, a condenser, and a pair of headphones. All of this strange equipment was connected to about 400 feet of "aerial wire" and Herb was ready for some serious DXing.

His SWL hobby continued on and off for the next few years, and Herb began monitoring the ham bands more and more. In 1941, Herb moved to his present QTH in San Carlos and the roof was soon covered with dipoles. In 1956, by now completely addicted to the ham bands, Herb purchased a 40-foot tower, a TV rotator, and a TA-33 JR triband beam.

Forced into early retirement in 1964 due to a medical disability, Herb settled in for some first-class SWLing. He birddogged the DXpeditions for the local DXers and logged better than 300 countries for himself.

For some reason, during all these years of SWLing the ham bands, Herb never really considered getting his own ham ticket until 1968 when some of the local youngsters began to encourage him. After several code lessons, Herb nervously took the Novice exam and shortly thereafter WN6BJS was licensed. In January of 1970, Herb passed his General exam and began DXing in earnest. His Advanced class license, his new Drake TR-4 transceiver, his 100th country, and his 63rd birthday arrived all in the same week.

Herb Lehmann WA6BJS. Those of us who have listened to Herbie run the Afrikaner Net for the past several years never thought he could look so serene.

FLASH!

The *73 Magazine* 10 Meter DX Decade Award #1 goes to Bill Gosney WB7BFK. Watch for a profile on Bill in an upcoming column.

In 1972, a chance encounter on fifteen meters with several W2 stations on Long Island in a round table with several African stations resulted in the formation of the world famous Afrikaner Net which meets seven days a week on 21355 kHz at 1800Z. Stations from all over the world check in and give new country contacts to stateside stations.

Along with Cal W2PPG and Leo W0GX, Herb has been the guiding force of the net since its inception.

Herb says that one of the highlights of his hamming career was a trip through the midwest in 1976 when he got to meet personally with some of the many friends he has met on the air.

Much of Herb's time is devoted to amateur radio, but he also enjoys classical music and sports, especially tennis and baseball. WA6BJS, known affectionately to his many friends as "Herbie," is one of the class acts that makes amateur radio the great hobby that it is.

CARIBE 1978

The Caribe 1978 Dxpedition which took place this past July and August is now history. Operations took place from Dutch Sint Maarten using the call PJ8USA and from Montserrat using the call VP2MBC. Alex W1CDC and Mac WA1ZSW were highly successful in their efforts to put these two islands into many logbooks. Following an intense satellite and low-frequency operating schedule, the first contacts were made via the OSCAR 8 satellite, modes A and J. A number of contacts were also made via the OSCAR 7 satellite using modes A and B. Using high-speed CW, better than 105 satellite contacts were made with stations in North America, South America, Central America, and Europe.

In addition to the satellite and VHF operations, low-band activity netted 3200 plus contacts, with CW again being the primary mode. Bands used were 10, 15, 20, and 40 meters, with major target areas being the Far East and the Orient. The Caribbean is rare DX for those areas of the world.

The only regret they had is that due to bad weather and a tight travel schedule, they were unable to operate from Anguilla VP2E and Guadeloupe FG7 as planned, but there is always next year and Caribe 1979.

DX NOTEBOOK

Dodecanese SV

WA4ICK has been running weekly skeds with SV1JH there on Rhodes. It is also possible that SV1JH could show on the 14225 morning net. Those skeds with WA4ICK are on 14300 kHz at 1300Z on Saturdays and 1900Z on Sundays. Make every effort to work this one, as it isn't often available.

Seychelles S79

Recent word out of the Seychelles reports that no new amateur licenses will be issued. Also, any present licenses will not be renewed upon expiration. This action was taken after a raise in the license application fee to $80.00 had no effect. Apparently S79 will become an endangered species. Better work one now while you still have the opportunity.

Qatar A7XAH

Ahmed has been showing recently on the long path on 14270 kHz after 1530Z, sometimes assisted in the pileups by a JY or 9K2. His QSL manager, DJ9ZB, says that 14270 kHz is indeed the frequency to watch. Ahmed is a Qatar ambassador and apparently the only A7 in existence.

Kerguelen Island FB8X

F6DZL arrived in December for a tour of duty on this rare French possession. Look for him in the usual DX alleys on ten, fifteen, and twenty.

South Sandwich LU3ZY

The operators at LU3ZY, Guillermo on SSB and Roberto on CW, left for Argentina last December. While on the island, they managed to rack up over 3,200 QSOs. The new crew on the island apparently will not be so productive, but it is heartening to note that there is at last a permanent station set up down there for any visiting operators to use. All QSLs for LU3ZY should be sent to the Radio Club at LU2CN.

Somalia 6O1

I2FGP should be showing from Somalia again soon. This time Giampaolo is planning on

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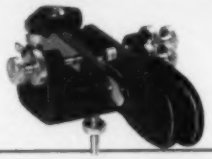

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some CW action and he will also be equipped for split-frequency operation. He has been one of the top European contesters for several years, so he is not afraid of pileups.

Franz Josef Land

UK1PAA was reported recently, so there does seem to be some activity. It has been reported that both UK1PAA and UK1PAD are on Franz Josef, UK1PAA on CW and UK1PAD on SSB. Regardless, work them first and worry later.

Saudi Arabia HZ1AB

This station is located at the US Military Training Mission at Dharan. No amateurs have been in the contingent for over a year now and any operating is done by visitors or by amateurs working in the Dharan area. Bill Gary K8CSG recently visited the area and found about 250 QSLs waiting to be answered. Most had been opened and everything but the QSL card had been removed. Bill says that the best way to QSL HZ1AB is to send the card along with an SASE to Leo Fry K8PYD, 5740 North Meadows, Columbus OH 43229. Copies of HZ1AB logs are sent to Leo and he takes care of the demand. If you need a card for a contact with HZ1AB, try Leo. If he has the logs, you will receive your card in short order.

Vatican City HV3SJ

W3US, who has operated HV3SJ in the past, passes along some information on the possibility of a second Vatican station. This will be HV2VO, located at Castle Gondolfo south of Rome. The suffix "VO" stands for "Vatican Observatory." The operator for this second station holds the call LU9LAZ and previously operated from VU2SX. This one may pose an interesting question as to its DXCC status. Vatican City is a separate state, but Castle Gondolfo is located in the Italian countryside. HV3SJ is usually active on Saturday mornings around 21280 kHz or 21410 kHz. QSL to W6KNH.

Marcus Island KA1MI

This is Dick Kobylarz WB1GXU and he plans to be on regularly until next summer. Look on 21375 kHz on Monday, Wednesday, and Friday. KA1NC is also active from Marcus on ten meters around 28630 kHz. Best time to look for these stations is after 2100Z. This counts the same as JD1.

Niger 5U7AG

K1VSK has made arrangements for 5U7AG to be active on Sundays on 14265 kHz after 500Z. The station is looking especially for those needing Niger for a new country and ego contacts are discouraged.

"MOST NEEDED" LIST

It's always interesting to run a "Most Needed" list because we can check and see how we stand compared to what others need. The following list is the result of a poll taken by the North Jersey DX Association. How many are on your list?

1. Okino-Torishima 7J1
2. Saudi-Iraq NZ8Z4
3. South Sandwich LU/VP8
4. Spratly 1S
5. Bouvet 3Y
6. China BY
7. Burma XZ2
8. Kamaran
9. Bhutan A5
10. Khmer XU
11. San Felix CE0X
12. Heard Island VK0
13. Laccadive Island VU
14. Mayotte FH0
15. Mellish VK9
16. Crozet FB8W
17. Glorioso FR7
18. Mt. Athos SV
19. Central African Empire TL8
20. Andam/Nicobar Island VU7

NOVICE CORNER

In reading through the mail this month, it seems that questions regarding the phenomenon of long-path DXing pop up the most often. First we will explain what it means to work a DX station via the long path, and then we will make an attempt at explaining the causes of long-path DX openings.

Generally speaking, working a station via the long path means working a station with your beam pointed the opposite direction from the shortest distance to the station. In other words, to work Europe and the Mideast from the United States via the long path requires pointing your antenna southwest, toward New Zealand.

Long-path openings occur most often on twenty meters, with less frequent openings on fifteen and ten. If everyone else is giving a DX station 5 by 9 reports and you can barely hear him, rotate your antenna around 180 degrees. If there is a long-path opening, he will probably be booming in now. Long-path signals are usually much stronger than those received on the regular short path.

Radio waves, like everything else in electronics, follow the path of least resistance. During the winter months, the Northern Hemisphere is tilted away from the sun; this causes the sun's rays to strike the Northern Hemisphere at an angle. This results not only in colder weather, but also in less ionization of the atmosphere. Meanwhile, the Southern Hemisphere is tilted towards the sun and is receiving the sun's rays more directly. The result here is longer, warmer days and a more heavily ionized atmosphere. It is this ionization of the atmosphere that allows us to make DX contacts.

Long-path openings occur because the Southern Hemisphere is more heavily ionized than the Northern Hemisphere. Even though the distance is greater, the more heavily ionized atmosphere is the path of least resistance.

I would like to mention one more item concerning beam pointing. Directions are not what we were led to believe by the old Mercator projection maps which hung from the blackboard in school. I strongly recommend the purchase of a Great Circle map of the world. These maps show true direction from the center of the United States. If you live on the east or west coast, it would be better to purchase a map centered on your area. If you can't locate such a map, there are several companies which will sell you a list of beam headings based exactly on your QTH. Don't be surprised if you find out you have been pointing your antenna the wrong direction all this time.

THANKS, KENT!

The following letter is from Tom Walilko K8NOQ to Kent Goddard, holder of the call ZD8KG. It chronicles the trials and tribulations of a quickie, unplanned DXpedition.

Kent Goddard
Pan American Airways
Patrick AFB FL 32925

Dear Kent,

Thanks very much for the use of your call, ZD8KG. To explain, our USAF C-135 was traveling

Continued on page 167

The Caribe 1978 DXpedition was blessed with overwhelming success on the satellites and low bands. Shown here on the island of Sint Maarten are Mac WA1ZSW and Alex W1CDC the day before making their departure for Montserrat, where they put VP2MBC on the air.

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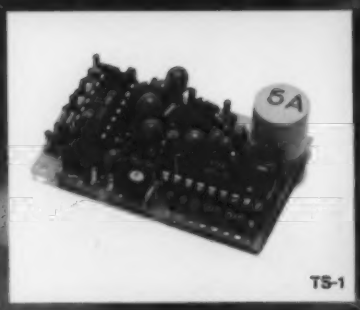
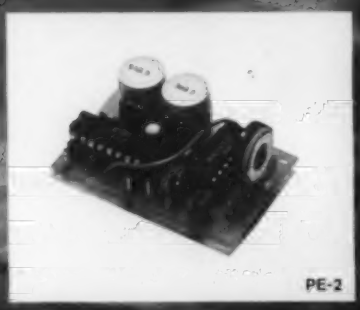
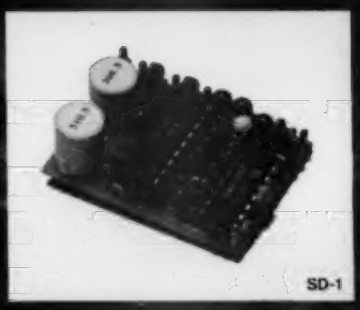
Reader Service—see page 211







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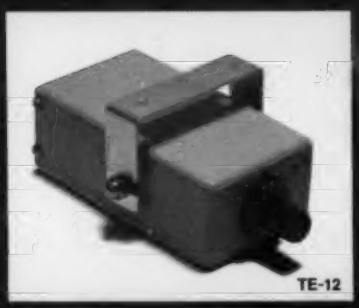
TE-8


TE-12

ST-1

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LETTERS

JONESTOWN

We believe that radio broadcasts were made from Guyana to San Francisco on the day before and the day that Congressman Leo Ryan was killed in Guyana.

Our office would appreciate your magazine printing a request for any ham radio operator who had contact with the People's Temple radio on November 17 and/or November 18, 1978, to contact the San Francisco District Attorney's Office at either (415)-553-1505 or (415)-553-1054 (call collect).

Thank you for your service.

Douglas N. Keener
Investigator
District Attorney's Office
San Francisco CA

AMMUNITION

As I was stuffing my husband's numerous magazines in the usual 99% of the closet (headache of wives of all hobbyists), I happened to drop your Aug., '77 issue of *Kilobaud*. It fell open to an article entitled, "Sooo, You Want To Be An Author." With nothing else to read in the house but medicine bottles and vegetable cans, I read it. I cannot possibly tell you of my utter amazement at having my husband so perfectly described. The excuses used by your aspiring authors(?) were classic—he's used every one of them, several times, in fact.

Believe me when I say that I am sick and tired of being used as a sounding board for ideas, criticisms, and comments perpetrated by your magazines (he's an avid *73/Kilobaud* reader). My question is this: Why discuss these subjects with a totally unwilling victim when there are people out there who would be happy to hear them? You must realize that I haven't the faintest idea what he's talking about.

I have tried tactful suggestions like "Why don't you get off your backside and write down your ideas and send them in?" Well, the answer, of course, is obvious. Just look at the list given in that article.

I finally drew the line when an article appeared in your magazine this month. The author had the same ideas that my husband had four months ago. And you paid the man one hundred dollars for it.

Just this month, my husband was wishing that there was some way he could buy the computer he wanted so he could start sending in programs (he's a computer technician working for his BSEE). He has the knowledge and the intelligence, but he has no confidence in himself. So, like the dutiful and loving wife that I am, I exercised my right to nag him until he actually sat down and started to write. It's been two days since he started and it's almost finished. Though I am by far no expert, I think it's great.

So, Mr. Green, thank you for supplying the ammunition that was needed for a short but productive battle.

Be looking for a superb article written by a very proud WB0FGO.

Jean M. Johnson
Sioux City IA

WRONGLY POINTED?

I am an avid reader of *73 Magazine* and appreciate your many disclosures of vendors who do not live up to their claims. I do feel it my duty, however, to advise you when it appears the finger has been wrongly pointed. Reference the letter entitled "Skin Disease" on page 118 of the October issue: I sympathize strongly with Mr. Carver about his treatment from Kensco Communications. His accusations towards Southeastern Communications, while certainly understandable, are not warranted, however.

I have dealt with this firm three times in the last six months, each time with excellent service. Actually, this firm seems to go out of its way to please. Upon receipt of the first order of six crystals, which arrived one week after order, one crystal was bad (no one's perfect). It was mailed back on Thursday, and its replacement arrived the following Wednesday. The second order was back-ordered and then shipped special delivery at Southeastern's expense when they were advised of the urgent need. The third was requested on a Thursday evening by phone and arrived the following Tuesday.

I don't know what more to say. Hopefully, it will not be long before service such as this is recognized. It seems unfair that a company should acquire the reputation of another just because they buy their stock.

Thanks for the chance to put in a good word for a good company. I hope you'll print this so others can see both sides of the story.

Keep up the good work, Wayne. You certainly help make an already interesting hobby more interesting.

Joe Bushel N4ARJ
Orange Park FL

SEEING THE LIGHT

After years of putting down "Chicken Banders," the light suddenly dawned that I might be missing something. My unfair speeding ticket for 50 mph in a country "30 mph zone" was the final clincher. I couldn't help but notice, as the polite but firm officer was writing my summons, that all cars with CB antennas were leisurely proceeding through the speed trap at a mere 29 mph.

I muttered all the way home: "I just gotta get me a CB." My XYL only shook her head—she's used to my muttering.

A short time later, while wandering through a local hamfest flea market, I encountered an enterprising CB dealer who was selling new (outlawed) 23-channel CB radios, sans mike, as "CB monitors" for only $7.00 each. He assured me that there was no transmitter in the case, only the receiver. Hmm—perhaps he was "mistaken" about the "missing transmitter." My sporting blood said "buy," but my intuition does not always give me the best advice. For instance, the bumper sticker on my Edsel used to say "AM—YES, SSB—NO." You get the drift!

So I bought the $7.00 wonder and after further searching and dickering bought a microphone for $1.00 and a used Hustler mobile CB antenna for $2.00.

Not wanting to wait until I arrived home to test the rig, I nervously connected power leads to fuse block and ground, plugged in the dollar mike, temporarily connected my 5/8-wave 2 meter FM antenna, and turned on the switch. Immediately my car was filled with rasping, squawking CB signals! At least the receiver section worked. Now for the acid test. I turned the channel selector to a relatively quiet channel, squeezed the push-to-talk switch, and timidly requested a signal report. "Wall to wall and treetop tall" came back the report from a mobile station claiming to be eight miles from my location! Success! I had achieved "Good Buddy" status for only $10.00. Could have had it for only $8.00, if I hadn't bought the antenna! Say, wonder if the guy who sold me the $2.00 Hustler will take it back at next year's Syracuse Hamfest?

Charles Willson K2GMZ
Palmyra NY

GOOD-BYE

I have received a notice that it is time to renew my long-standing subscription to *73 Magazine*. I have decided not to renew. Among the reasons for this decision, the following are the most pertinent.

The editorial policy of your magazine appears to promote unlawful activities and to encourage your readers to be scofflaws. I refer especially to your articles about radar jamming. Amateur radio does not need a spokesman who advocates this type of activity, and I certainly do not care to support the distribution of this type of material. Your proposal for the formation of a religious cult to further impede enforcement of the law borders on the ridiculous.

It would seem to me that if you would devote your talents to the enrichment of amateur radio instead of filling your editorial columns with attacks on the ARRL and the FCC, your magazine would benefit. One cannot build a desirable reputation by degrading others!

Your conduct is hurting not only amateur radio, but also your pocketbook, which, if I read between the lines correctly, is very near to your heart! It is my understanding that many others feel as I do and are not renewing their subscriptions. I was a charter subscriber to both *Byte* and *Kilobaud*, and when my *Kilobaud* subscription expires, it will not be renewed.

Mel Hart W0RV
St. Louis MO

MORE ON KM1CC

I was glad to read the article, "The KM1CC Story," in the October issue of *73 Magazine*. However, I should correct the statement made about the equipment loaned to KM1CC by RCA Global Communications, Inc. The reference to "a modern WCC inked-paper readout receiver" isn't quite correct.

First, the inked-paper re-

ceiver, more appropriately recorder, isn't a receiver as most of us would think of a receiver. Typically, when we speak of receivers in the amateur radio vernacular, we are talking about devices used to detect radio signals and convert them to a form of audio signal. The above-mentioned recorder does not detect radio signals; rather, it uses audio to control the deflection of a stylus, thus yielding an inked trace of the input audio.

Neither would I describe the equipment as *modern*, because it dates back before World War II and hasn't been used at WCC since about that time. Incidentally, the receiver loaned with the recorder was an old Radiomarine AR-67, an LF and MF band receiver used at WCC quite a few years ago and hardly modern.

The equipment loaned by WCC was to enable the nonamateur to observe a visual display of CW signals. In this case, the recorder and the AR-67 receiver were used to monitor the WCC 500 kHz, A-2, CW signal.

I felt these points should be brought out so that the astute reader doesn't get the impression that we (WCC) are still using the *old* inked-paper recorder and calling it *modern*.

Wm. H. Farris, Jr. K1WF
Chatham MA

PAINT RIP-OFF

This note is to notify your readers of a new rip-off. It's called "Paint falling off your car due to rf." This BS is being passed around to auto dealerships and auto paint shops—that rf makes paint fall off cars in the area of the antenna. In my case, my new '78 car's trunk lid is discolored and the paint is chipping off. The dealer says that my radios are making it do that and that they are not going to fix it. I have talked to several other radio ops and they were told the same thing about the paint on their cars.

If this happens to anyone else, call the local Consumer Affairs Office and raise hell. I did, and it worked.

Jim Menefee WA4KKY
Jacksonville FL

CODE SUCCESS

Your long-standing theory on teaching Morse characters at high speed while spacing them out to make 5 wpm is working out well for a class of prospective Novices I'm teaching. I explained that I was doing this in order to have them learn letter sounds instead of having them go through the double step of counting dots and dashes and then translating that to letters. They accepted the logic of this and seem to be having no trouble copying letters at 15 wpm, spaced to about 7.

Linc Thorner WDØCLB
Minot AFB ND

TOMBSTONE GAMBLING

"New Life for Old Transformers" in the January, 1978, issue was excellent, but one cringes when instructed to connect 110 volts to "what you suspect are the primary leads"! Gamble wrong and the author's address of Tombstone could become sadly appropriate.

A safe and constructive suggestion is offered: First, set the ac voltmeter to its highest range. Energize a separate 6.3-volt transformer and apply its low voltage to the unknown windings. When approximately 110 volts is measured across another winding, *that* is the primary, and the energized winding is a 6.3-volt winding. *Now* it is safe to apply 110 V ac to the primary and identify any remaining windings.

Gene Brizendine W4ATE
Hunstville AL

BOX-BUSTER

Well, Wayne, you have done it again!! Here I am looking at my nice new set of library shelf boxes and wondering how the heck I am going to get the December issue of *73* into one of them which already contains the first eleven issues! Leave it to Green to sell you a product and then have such a thick set of magazines that you can't possibly fit a whole year's worth of mags into it. I didn't have any problem fitting in some of the other mags! Oh well, I guess I'll just have to put the December issue alongside the box when I get it! Keep up the good work, and keep those RTTY articles coming.

Robert J. Farrell Jr. WB2COY
Poughkeepsie NY

THE WORD FROM JEDDAH

My friend W9MXU receives current copies of *73 Magazine* here in Jeddah (costs $5.05 US to mail the copies to him each month). I would say you have a devoted subscriber indeed!!

What is great is that he shares *73* with me and now I want to be a subscriber—enclosed is my subscription for 3 years. Please send *73* to my home QTH in the USA.

There are many hams here in Jeddah from all over the world, as well as many from the U.S.A.—all we can do is listen to all those beautiful CQs on all the ham bands! I'm using a portable Toshiba RP-2000F receiver covering FM broadcast through 30 MHz; it also has a bfo for SSB and CW. It's a fine little receiver and I had not seen it in the U.S.A. before leaving for Arabia.

I hope when I arrive home I will have my first issue of *73*—that would be great. The very best to you and your organization on the outstanding job you do for amateur radio.

David O. Finnell W5LCL
Jeddah, Saudi Arabia

COMMON SENSE

My hat is off to Wayne Green and his magazine as the finest amateur radio publication on the market. Contrary to Merrill Eidson's comments that Wayne should stop attacking the ARRL and stick to improving *73*, I feel that Wayne is justified in his comments on the ARRL.

Merrill mentioned being a solid member of the ARRL for fifty years in his letter. This is indicative of quite a few members of the organization. Most are from the spark-gap era and the big guns running the organization operate it with this antiquated style.

I have been a ham for a number of years and feel that a magazine such as *73* is progressive and certainly represents the modern technology and operating practices of amateur radio. The only value I ever received from *QST* was who made DXCC, WAS, etc. As for technical articles of value, *QST* never did impress me.

The ARRL certainly needs to work more for the interests of all hams instead of trying to promote measures that will benefit the elite group. A more down-to-earth approach by the ARRL would restore my faith in the organization.

Wayne, keep up the good work. You have my full support. Your common-sense approach to amateur radio is needed to keep things in their perspective.

Dick Sullivan KØDQG
Des Moines IA

PETTING

Thanks to Paul A. Lilie for his fine article on the Commodore PET ("Look What Followed Me Home!", page 142, November, 1978). One of his "complaints" regarding the tape-handling system is the difficulty he experienced finding the end of program B on a tape when he wants to load a new program, A, on the same tape (he listens on an audio cassette deck for the end of the noise).

I have a better suggestion: Ask PET to VERIFY "B". PET will search for B, find it, compare it with A in memory and report a "VERIFY ERROR." No matter, you've found the *end* of B, which is what you need before asking PET to save "A". PET stops at the end of the VERIFY process.

The PET's implementation of the IEEE-488 bus makes it a truly professional machine, well beyond the mere "hobby video game" class.

How about some articles on the use of PET as a Morse/RTTY terminal?

Paul Birman WA2JPJ
Flushing NY

Ham Help

We would like to swap club newsletters with other amateur radio clubs. If interested, contact:

Sterling-Rock Falls Amateur Radio Society
c/o Donald Van Sant WA9PBS
1104 5th Ave.
Rock Falls IL 61071

In the last few years, I have been looking for a list of the frequency bands and power limitations of amateur stations in foreign countries. It is my opinion that such data would prove valuable to many amateurs, both foreign and domestic. Most of the information on the American amateur bands is widely published and well-known, but that of many foreign countries is believed to be considerably restricted. Help in directing me to a source of this type of information would certainly be appreciated. Thanks for any information anyone may be able to provide.

Paul Wiegert W8TH
1205 East Franklin St.
Centerville OH 45459

I would appreciate (and pay reasonable expenses, if necessary) info on solid-stating (ICs?) a WWII-type BC-221-m frequency meter. If I build modular, why can't I use it for CW vfo? All responses acknowledged. Thanks.

Justin B. Snyder WA9MQO
403 North Ave
Lake Bluff IL 60044

Contests

Robert Baker WB2GFE
15 Windsor Dr.
Atco NJ 08004

THE WEST AUSTRALIAN 150TH YEAR CELEBRATION CONTEST

The aim of the contest is for amateurs on all continents to contact amateurs in Western Australia (VK6) on all bands using all modes, this being to commemorate the 150th year celebration of the foundation of Western Australia.

The contest will commence at 1600Z on 31 December, 1978, and end at 1600Z on 31 December, 1979.

All authorized amateur bands may be used between 1.8 MHz and 28 MHz using any of the modes appropriate to the regulations applying to the entrant. Operators are encouraged to operate both phone and CW.

The three highest scores from each continent for mixed and individual modes will receive a commemoration certificate. This contest is also open to SWLs.

For VK amateurs and SWLs, the three highest scores from each state will be eligible for a certificate, while VK6 participants who have more than 100 out-of-state QSOs will get an award.

SCORING:

One contact in each mode is allowed in each band every day with the same station, for which the following scores and multipliers will apply: CW—5 points per contact; phone—3 points per contact; RTTY—6 points per contact. Multipliers: One point per band used, provided that 30 QSOs are obtained on that band, except for 1.8 and 3.5 MHz, where 1 QSO will count. Final score = total points × total multipliers.

LOGS:

Contest logs should show date, time, call, band, mode, RST out, RST in, points scored, and include a running total. The log should bear a front cover sheet bearing the following: call, address, claimed score, and signature. Contest logs are to be forwarded to: The Contest Manager, 150th Celebration Contest, PO Box 6250, Hay Street East, Perth 6000, Western Australia.

NEW HAMPSHIRE QSO PARTY
2000 GMT February 3 to
0500 GMT February 4
1400 GMT February 4 to
0200 GMT February 5

The contest is sponsored by the Concord Brasspounders, Inc., W1OC, to promote the Worked New Hampshire Award. Stations may be worked once per band per mode. NH stations may work each other.

EXCHANGE:

NH stations send RS(T) and county, others send RS(T) and ARRL section or country.

SCORING:

NH stations score 1 point per QSO times the number of ARRL sections plus countries plus NH counties. Others score 5 points per NH QSO times the number of NH counties.

FREQUENCIES:

CW—1810, 3555, 7055, 14055, 21055, 28130; Phone—1820, 3975, 7235, 14280, 21380, 28575; Novice—3730, 7130, 21130, 28130; VHF—50.115, 145.015, FM simplex (no repeaters!).

AWARDS:

Top scorer in each NH county and top scorer in each state, province, and country (50 points min.). Additional certificates available for confirmation of all 10 NH counties. Send logs, summary, and checksheets to: Concord Brasspounders, Inc., C. Halloway, 9 Via Tranquilla, Concord NH 03301. Mailing deadline is March 12. Include a business size SASE for results and/or award.

TEN-TEN INTERNATIONAL NET WINTER QSO PARTY
0000 TO 2400 GMT on
February 4 and
February 11

The contest is open to all amateurs, but only members are eligible for awards. All contacts must be made on 10 meters. Classes of operation include: single-op, multi-op, and QRP (20 Watts PEP or less). A station may be counted only once; all logs must be in GMT. Stations with new calls must list old callsign. All QRP stations must list equipment used.

Calendar

Feb 2-11	ARRL Novice Roundup
Feb 3-5	NH QSO Party
Feb 4, 11	10-10 Net Winter QSO Party
Feb 10-11	QCWA QSO Contest—CW
Feb 17-19	Two-Land QSO Party
Feb 17-Mar 4	University of Cape Town Festival Station
Feb 24-25*	French Contest—Phone
Mar 3-4	ARRL DX Competition—Phone
Mar 10-11	QCWA QSO Contest—Phone
Mar 17-18	ARRL DX Competition—CW
Mar 24-26	BARTG Spring RTTY Contest
Mar 31-Apr 1	International 10-10 Net Canterbury Chapter QSO Party North Dakota QSO Party
Apr 7-8	ARRL Open CD Party—CW QRP QSO Party
Apr 21-22	ARRL Open CD Party—Phone ARRL EME Contest
May 19-20	ARRL EME Contest
June 9-10	ARRL VHF QSO Party
June 23-24	ARRL Field Day
July 4	ARRL Straight Key Night
July 14-15	ARRL IARU Radiosport Competition
Aug 4-5	ARRL UHF Contest
Sept 8-9	ARRL VHF QSO Party
Sept 15-16	Scandinavian Activity—CW
Sept 22-23	Scandinavian Activity—Phone
Oct 13-14	ARRL CD Party—CW
Oct 20-21	ARRL CD Party—Phone
Nov 3-4	ARRL Sweepstakes—CW
Nov 17-18	ARRL Sweepstakes—Phone
Dec 1-2	ARRL 160 Meter Contest
Dec 8-9	ARRL 10 Meter Contest

* = described in last issue.

THE 73 MAGAZINE 10 METER AWARDS

The return of vigorous solar activity means that 10 meters is once again a band to be reckoned with. Ol' Sol's 11-year cycle of sunspot production is about to hit a peak, with the result that QRP 10 meter DX is possible.

Now's the perfect time to convert that old CB rig to 10. American Crystal Supply makes a variety of simple and inexpensive conversion kits, or you can do-it-yourself from the articles in 73. True appliance operators can purchase ready-made rigs from Bristol Electronics or Standard Communications. To give you an added incentive, 73 is offering two nifty Certificates of Achievement for 10 meter channelized communications.

For domestic types, there is the 10-40 Award. This one should be pretty easy—just work 40 of the 50 states. The DX Decade Award goes to DXers who work 10 or more foreign countries with a channelized 10 meter rig. We have endorsement stickers, too—the whole bit.

To give everyone an equal shot at award #1, only contacts made October 1, 1978, or after will be valid.

Well, don't just sit there. Get out your soldering iron, order some crystals, and put that CB rig on 10. This is going to be fun, so don't miss out!

RULES

1) All contacts must be made in the 10 meter amateur band using channelized AM equipment. Both converted Citizens Band equipment and commercially-produced units may be used.

2) To be eligible for award credit, all contacts must be made October 1, 1978, or after.

3) The 10-40 Award is available to applicants showing proof of contact with stations in at least 40 of the 50 United States. A special endorsement sticker will be available to those working all 50 states.

4) The DX Decade Award is available to applicants showing proof of contact with at least 10 foreign countries. Endorsement stickers will be awarded for 25, 50, 75, and 100 countries.

5) A log of stations worked, with the date, time, and type of equipment used for each contact, must be submitted when applying for each award or endorsement.

6) Each application for an award or endorsement must be accompanied by a signed statement that all claimed contacts are valid. No QSL cards need be sent, but they must be in the possession of the applicant.

7) To cover costs, a fee of $5.00 must accompany each application for the 10-40 or DX Decade Award. The fee for endorsement stickers will be $2.00 each.

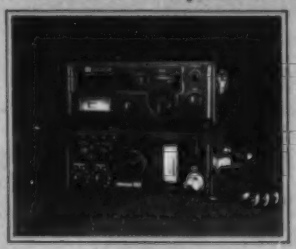
8) All award applications should be mailed to: Chuck Stuart N5KC, 5115 Menefee Drive, Dallas TX 75227.

Introducing the Tenham-153 two-meter FM radio.

Meet the Tenham-153. A brand new radio for American Amateurs featuring a brand new idea in flexibility: an outboard VFO for continuous coverage of the 144-148 MHz band.

Alone, the Tenham-153 is a 24-channel crystal-controlled (one crystal per channel) 10-watt 2-meter FM rig. A compact, rugged radio built in the solid-state-of-the-art design tradition of Fujitsu Ten, one of the world's most famous names in electronics for the past 40 years.

The Tenham-153 comes complete with 146.94 MHz crystals in place. Controls include a simplex/repeater (±600 kHz splits) switch, plus a handy priority channel switch right on the MIC for instant access. A built-in regulator compensates for DC voltage variations. A high/low power switch makes long-range simplex or close-range repeater operation convenient.



Add the optional VFO832B outboard variable frequency oscillator and get complete coverage of the 144-148 MHz band. A large LED readout tells you exactly the frequency you dial up. It's the ultimate in flexibility. What's more, the VFO832B acts as a handy frequency counter when you're netting crystals in the Tenham-153. A range check circuit prevents out-of-band operation. The oscillator disables itself and a warning light flashes on the front panel. There's even an RIT and fine tuning knob. Plus a built-in tuning meter for accurate tuning like you've never experienced before.

See the exciting Fujitsu Ten line-up of quality Amateur gear at your dealer's today. Or write us direct for complete information.

TEN **FUJITSU TEN CORP. OF AMERICA**
1135 East Janis St., Carson, CA 90746. Phone: (213) 537-8930

Stations can credit any chapter with their score as long as they hold a certificate from that chapter.

EXCHANGE:

Call, 10X number, ARRL section, and name.

SCORING:

Continental USA contacts are 1 point, 2 points if 10X member. DX (outside continental USA) are 2 points or 3 points if 10X member. QRP contacts are 2 points or 4 points if 10X member.

ENTRIES:

Members only send logs to Robert C. Mugherini WA1AKS, PO Box 169, Randolph MA 02368. Logs must be received no later than March 11. Results will be published in the 10-10 Net spring bulletin.

AWARDS:

For each class, 1st place certificate to each US district, KL7, KH6, and other US Pacific Islands; each VE district, Central America, and Caribbean; So. America; Europe; Africa; and So. Atlantic, Asia, Australia, New Zealand, and So. Pacific.

Results

RESULTS OF WASHINGTON STATE QSO PARTY FOR 1978
Sponsored by Boeing Employees' Amateur Radio Society (BEARS)

TOP SCORES, OUT-OF-STATE:

State	Call	QSOs	Mult.	Total
Alabama	K4ZGB	85	23	3910
Arizona	W7RIR	35	17	1190
California	N6PE	104	30	6240
Colorado	K0MT	62	28	3472
Connecticut	W1VH	50	19	1900
Delaware	N3AHA	2	2	8
Florida	K4DDB	68	19	2584
Georgia	N4NX	98	31	6076
Idaho	K7TAK	29	12	696
Illinois	K9BG	103	27	5562
Indiana	WB9BAI	70	18	2520
Iowa	WB0UIT	24	9	432
Kansas	K0FPC	22	9	396
Kentucky	WA4QMQ	28	14	784
Louisiana	W5WG	116	30	6960
Maine	W1DLC	46	13	1196
Maryland	W3PYZ	38	17	1292
Massachusetts	W1AQE	39	20	1560
Michigan	WA8VJE	44	12	1056
Minnesota	WB0LNO	39	14	1092
Missouri	K0RWL	15	10	300
Nevada	W7HI	32	14	896
New Jersey	WB2VFT	92	20	3680
New York	W2NRD	33	14	924
North Carolina	N4GF	9	6	108
Ohio	AD8J	41	14	1148
Oregon	K7DRD	5	4	40
Pennsylvania	WA3JXW	26	11	572
Rhode Island	WB1DET	20	10	400
South Carolina	K4BZD	37	12	888
South Dakota	WA0BZD	42	14	1176
Tennessee	WA4CMS	27	12	648
Texas	W5VGX	44	15	1320
Utah	W7LN	13	9	234
Virginia	W4KMS	33	11	726
Wisconsin	K9GTQ	41	18	1476
Ontario, Can.	VE3KK	52	20	2080
Nova Scotia, Can.	VE1BNN	5	4	40
Brazil	PY1BAR	16	9	288
Japan	JR1NRP	18	8	288
Sweden	SM3BCZ	15	10	300

TOP SCORES, WASHINGTON STATE:

County	Call	QSOs	Mult.	Total
Adams	W7GHT/M7	10	9	180
Asotin	W7GHT/M7	19	12	456
Chelan	N7RC	109	30	6540
Clark	N7ZZ	2090	114	476,520
Columbia	W7GHT/M7	18	12	432
Cowlitz	WA7PMW	466	62	57,784
Douglas	W7GHT/M7	28	13	728
Ferry	W7GHT/M7	20	10	400
Franklin	W7GHT/M7	25	17	850
Garfield	W7GHT/M7	25	16	800
Grant	W7WMO	393	53	41,658
Island	W7UMX	1053	90	189,540
King	K7GR	403	55	44,330
Kitsap	WA7UWE	620	56	69,440
Lincoln	W7GHT/M7	33	19	684
Okanogan	W7GHT/M7	14	11	308
Pend Orielle	W7GHT/M7	18	20	360
Skagit	WA7GVM	749	76	113,848
Snohomish	K7II	125	36	9000
Spokane	W7GHT/M7	29	16	928
Stevens	W7GHT/M7	38	21	1596
Thurston	N7RV	190	45	17,100
Wahkiakum	WB7OVA	46	19	1738
Whatcom	WA7YCZ	1430	71	203,060
Whitman	W7GHT/M7	19	13	494

QCWA MEMBERSHIP QSO CONTEST
CW:
0001 GMT Saturday, February 10 to 2400 GMT Sunday, February 11
Phone:
0001 GMT Saturday, March 10 to 2400 GMT, Sunday, March 11

Historically, the QCWA membership contest has been held on a single weekend for both modes of operation. For greater participation in 1979, the contest will be held on two weekends separated by one month. For additional interest and point-scoring purposes, three global areas have been established. Frequencies, confirmation texts, and related contest rules and guidelines are available in the *QCWA News*.

TWO-LAND QSO PARTY
2100 GMT Saturday, February 17 to 0700 GMT Sunday, February 18
1300 GMT Sunday, February 18 to 0300 GMT Monday, February 19

This is a new contest organized by the South Jersey Contest Coalition. There is no operating time limit within the contest periods, but there is a mandatory 6-hour rest period from 0700 to 1300 on Sunday. The same station may be worked once per band and mode, and mobiles and portables may be worked each time they change counties. The states of New Jersey and New York, with 83 counties, will try to work the world and vice versa!

EXCHANGE:

RS(T), county, and state for Two-Land stations. RS(T) and state, province, or country for others.

FREQUENCIES:

CW—1805, 3560, 7060, 21060, 28060; SSB—1815, 3900, 7230, 14280, 21355, 28600; Novice—3725, 7125, 21125, 28125.

SCORING:

Each QSO counts 2 points. For Two-Land stations, the multiplier is the number of states, provinces, and DX countries (by DXCC) plus the number of Two-Land counties. For all others, the multiplier is only the number of Two-Land counties (83 max.).

AWARDS:

Certificates to the top scoring station in each Two-Land county, each state, province, and DX country. Second- and third-place awards will be issued where justified. Awards also for top mobile, portable, multi-operator, Novice, and club.

ENTRIES:

Logs with over 200 QSOs should include a dupe sheet. Indicate each new multiplier as worked. Also, include a summary sheet and usual declaration. For results, include a large SASE; DX stations include a large SAE. Send entries to: South Jersey Contest Coalition, c/o AB2E, Darrell Neron, 322 S. Cummings Avenue, Glassboro NJ 08028.

THE UNIVERSITY OF CAPE TOWN FESTIVAL AND AWARD, 1979

To commemorate the 150th anniversary of the University of Cape Town, Cape Town, Republic of South Africa, the Cape Town branch of the SARL will operate a special festival station with call ZS1UCT (ZS1-*U*niversity of *C*ape *T*own) and issue an award.

The University of Cape Town Festival Station will operate Saturday, February 17, to Sunday, March 4, 1979, Saturdays and Sundays 0600 to 2000 GMT, and weekdays 0700 GMT to 1000 GMT, 1500 GMT to 2000 GMT.

FREQUENCIES:

Use for calling. Actual frequency will depend on QRM. 40 meters—7.050 MHz. 20 meters—14.210 MHz. 15 meters—21.200 MHz. 10 meters—28.580 MHz. 2 meters—145.500 MHz.

TRANSMISSION MODES:

SSB, CW, RTTY, and FM.

SARL Bureau, P.O. Box 3037, Cape Town 8000, Republic of South Africa.

RULES AND AWARDS:

The award is open to all licensed amateurs and shortwave listeners (SWLs). DX stations and SWLs must log ZS1UCT plus two (2) other ZS1 stations (ZS1 contacts to be logged between February 15 and March 15, 1979). ZS and ZR stations log ZS1UCT plus 5

Continued on page 172

This NEW MFJ Versa Tuner II . . .

has SWR and dual range wattmeter, antenna switch, efficient airwound inductor, built in balun. Up to 300 watts RF output. Matches everything from 1.8 thru 30 MHz: dipoles, inverted vees, random wires, verticals, mobile whips, beams, balanced lines, coax lines.

MFJ LOWER PRICES!

NEW, IMPROVED MFJ-941B HAS . . .
- More inductance for wider matching range
- More flexible antenna switch
- More sensitive meter for SWR measurements down to 5 watts output

NEW LOWER PRICE

$79.95

Transmitter matching capacitor. 208 pf. 1000 volt spacing.

Sets power range, 300 and 30 watts. Pull for SWR.

Meter reads SWR and RF watts in 2 ranges.

Efficient airwound inductor gives more watts out and less losses.

Antenna matching capacitor. 208 pf. 1000 volt spacing.

Only MFJ gives you this MFJ-941B Versa Tuner II with all these features at this price:

A SWR and dual range wattmeter (300 and 30 watts full scale) lets you measure RF power output for simplified tuning.

An antenna switch lets you select 2 coax lines direct or thru tuner, random wire/balanced line, and tuner bypass for dummy load.

A new efficient airwound inductor (12 positions) gives you less losses than a tapped toroid for more watts out.

A 1:4 balun for balanced lines. 1000 volt capacitor spacing. Mounting brackets for mobile installations (not shown).

With the NEW MFJ Versa Tuner II you can run your full transceiver power output — up to 300 watts RF power output — and match your transmitter to **any** feedline from 160 thru 10 Meters whether you have coax cable, balanced line, or random wire.

ANTENNA SWITCH lets you select 2 coax lines direct or thru tuner, wire/balanced line, dummy load.

You can tune out the SWR on your dipole, inverted vee, random wire, vertical, mobile whip, beam, quad, or whatever you have.

You can even operate all bands with just one existing antenna. No need to put up separate antennas for each band.

Increase the usable bandwidth of your mobile whip by tuning out the SWR **from inside your car.** Works great with all solid state rigs (like the Atlas) and with all tube type rigs.

It travels well, too. Its ultra compact size 8x2x6 inches fits easily in a small corner of your suitcase.

This beautiful little tuner is housed in a deluxe eggshell white Ten-Tec enclosure with walnut grain sides.

SO-239 coax connectors are provided for transmitter input and coax fed antennas. Quality five way binding posts are used for the balanced line inputs (2), random wire input (1), and ground (1).

NEW 300 WATT MFJ VERSA TUNER II'S: SELECT FEATURES YOU NEED.

NEW MFJ-945 HAS SWR AND DUAL RANGE WATTMETER. NEW LOWER PRICE

$69.95

Same as MFJ-941B but less 6 position antenna switch.

NEW MFJ-944 HAS 6 POSITION ANTENNA SWITCH ON FRONT PANEL. NEW LOWER PRICE

$69.95

Same as MFJ-941B but less SWR/Wattmeter.

NEW MFJ-943 MATCHES ALMOST ANYTHING FROM 1.8 THRU 30 MHz. NEW LOWER PRICE

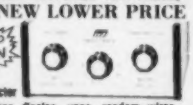
$59.95

Same as MFJ-941B, less SWR/Wattmeter, antenna switch, mounting bracket. 7x2x6 in.

ULTRA COMPACT 200 WATT VERSA TUNERS FOR ALL YOUR NEEDS.

MFJ-901 VERSA TUNER MATCHES ANYTHING, 1.8 THRU 30 MHz. NEW LOWER PRICE

$49.95



Efficient 12 position air inductor for more watts out. Matches dipoles, vees, random wires, verticals, mobile whips, beams, balanced lines, coax. 200 watts RF, 1:4 balun, 5x2x6 in.

MFJ-900 ECONO TUNER MATCHES COAX LINES/RANDOM WIRES. NEW LOWER PRICE

$39.95

Same as MFJ-901 but less balun for balanced lines. Tunes coax lines and random lines.

MFJ-16010 RANDOM WIRE TUNER FOR LONG WIRES. NEW LOWER PRICE

$29.95

1.8 thru 30 MHz. Up to 200 watts RF output. Matches high and low impedances. 12 position inductor. SO-239 connectors. 2x3x4 inches. Matches 25 to 200 ohms at 1.8 MHz. Does not tune coax lines.

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Reader Service—see page 211

New Products

CSC INTRODUCES NEW SWEEPABLE FUNCTION GENERATOR, THE MODEL 2001

Continental Specialties Corporation is again broadening its line of inexpensive troubleshooting and design hardware with the introduction of its new Model 2001 four-waveform function generator, electronically sweepable over a 10:1 to 100:1 range.

The 2001 offers sine, triangle, square, and TTL square waves from 1 Hz to 100 kHz in five push-button-selectable overlapping ranges, tuned with a 10:1 vernier dial featuring 50 increments and an accuracy of ±5% of the dial setting.

The TTL output will drive 10 TTL loads with rise and fall times of less than 25 nanoseconds.

Sine, square, and triangle waveform outputs are variable over a greater than 40 dB range. The high level output is rated at 0.1-10 V_{p-p} into an open circuit, and .05-5 V_{p-p} into a 600-Ohm load. A separate low level output, 40 dB down from the high level output, is rated at 1-100 mV into an open circuit, and .5-50 mV into a 600-Ohm load. The variable amplitude control, once set, holds the output signal to within less than ±0.5 dB over the entire frequency range.

The sinusoidal waveform offers less than 2% distortion. The triangular waveform is within less than 1% of linearity error. The standard (not TTL, which is a separate output) square wave features rise and fall times of less than 100 nanoseconds, and a time symmetry error of less than ±2%.

The voltage-controlled sweeping oscillator (sweep vco) may be zero-referenced from any frequency setting. The banana jack input will accept any signal from 0-±10 volts, and offers a 22k input impedance.

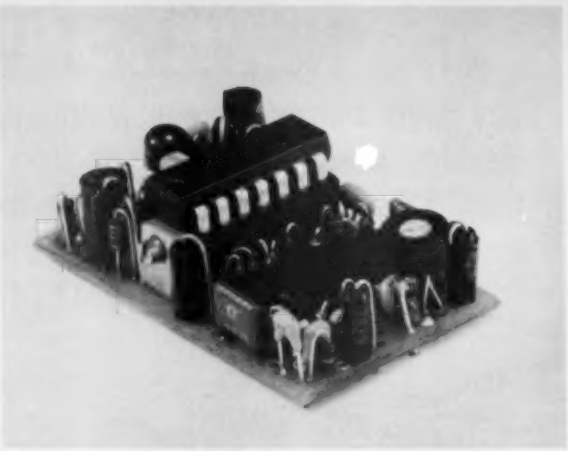
The 2001 is calibrated at 25° C. ±5° C., but operates over a 0-50° C. range. The 10" W × 3" H × 7" D package (25.4 × 7.6 × 17.8 cm) weighs in at 2.2 pounds (1.0 kg). Power requirements are 6 Watts at 105/125 V ac, 50/60 Hz.

A 220-240 V ac, 50/60 Hz-powered version is optionally available. Also available is a 20-dB banana jack adapter output attenuator.

For additional information, contact *Continental Specialties Corporation, 70 Fulton Terrace, New Haven CT 06509, or 351 California Street, San Francisco CA 94104.* Reader Service number C9.

VEGA ANNOUNCES THE WORLD'S SMALLEST TUNABLE SUBAUDIBLE TONE ENCODER-DECODER

Vega has introduced a new subminiature, subaudible tone encoder/decoder for hand-held radio as well as routine mobile radio applications. The Model 185 is completely tunable to any EIA CTCSS frequency without adding or changing any components. Measuring just 1.0" x 1.56" x 0.55", the unit includes a high-pass voice filter and adjustable output level. A unique self-squelching feature eliminates external squelch circuit connections in most applications, making installation simple and quick. The Model 185 exceeds all EIA specifications (including frequency stability) and comes with Vega's three-year warranty.



Vega's new Model 185 tone encoder/decoder.

For further information, contact *Vega, 9900 Baldwin Place, El Monte CA 91731; (213)-442-0782.* Reader Service number V21.

MIRAGE MP1 HF PEAK-READING WATTMETER

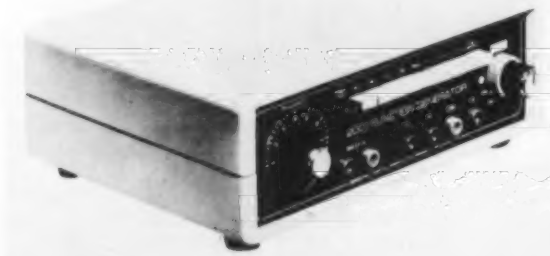
With the successful introduction of the MP2 VHF (50-200 MHz) peak-reading wattmeter, Mirage Communications is now offering the MP1 HF (1.8-30) peak-reading wattmeter.

The MP1 is designed to provide the amateur operator with a versatile fixed or portable wattmeter, without having to use cumbersome plug-ins or add-ons.

It has three power ranges (25, 200, and 2000 Watts) which provide easy reading, whether in use for low-power QRP operation or with the biggest DX setup. The MP1 will read both forward and reverse power at the flip of a switch.

The MP1 has the same fine features as the MP2, namely, the ability to display either an average or a peak power read-

Continued on page 170



CSC's Model 2001 function generator.

The Mirage MP1 wattmeter.

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There's a Telex Headphone that will let you do it better. Sure, sometimes you just can't hear them. But if there's a chance, it's easier with a Telex headphone. There's one for every discriminating choice. At better ham outlets everywhere, or write...

H4

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TRANSISTORS, ETC.

type		case	VCE	Ic	PD	Ft	HEP#	each	ten
MPSA10	NPN	TO92	40V	.1A	.3W	50Mhz	728	$.40	$3.50
MPSU52	PNP	TO202	40	1.5	1.0	150	S3031	.30	2.50
MPSU56	PNP	"	60	1.0	5.0	50	"	.35	3.00
MPSA55	PNP	TO92	60	.5	.5	50	708	.25	2.00
2N2222	NPN	TO92	30	.8	.5	250	736	.30	2.50
2N2322	SCR	TO-5	25V	1 AMP	.2ma	gate I		.30	2.50
2N2324	SCR	TO-5	100	1 AMP	.02ma	"		.40	3.50
2N2325	SCR	TO-5	150	1 AMP	.2ma	"		.45	4.00
2N2907	PNP	TO18	40	.6	.4	200	52	.35	3.00
2N3440	NPN	TO-5*	250	1.0	10.0	50	S3021	.60	5.00
2N3565	NPN	TO106*	30	.2	.3	40	55	.15	1.00
2N3639	PNP	TO92	12	.1	.2	350	57	.20	1.50
2N3640	PNP	TO106#	15	.2	.2	400	57	.15	1.00
2N3646	NPN	TO106#	15	.2	.2	400	50	.15	1.00
2N3704	NPN	TO92	30	.8	.3	100	735	.40	3.50
2N3903	NPN	TO92	40	.2	.3	300	736	.20	1.50
2N3904	NPN	TO92	40	.2	.3	300	736	.20	1.50
2N4248	PNP	TO92	40	.1	.2	40	715	.15	1.00
2N4250	PNP	TO92	40	.1	.2	50	57	.25	2.00
2N4400	NPN	TO92	40	.2	.3	200	736	.15	1.00
2N4437	NPN	TO106	30	.5	.2	250	736	.20	1.50
2N5138	PNP	TO106	30	.1	.2	30	52	.20	1.50
2N5172	NPN	TO92	25	.1	.2	120	56	.25	2.00
2N5210	NPN	TO92	50	.05	.3	80	728	.30	2.50
2N5910	PNP	TO106	20	.1	.3	700	52	.30	2.50
2N5964	NPN	TO92	150	.1	.5	100	S0005	.25	2.00
D16P1	NPN	TO98	12	(high gain lo-pwr DARL.)				.20	1.50
D40C1	NPN	TO220#	30	.5	6.	DARLINGTON		.30	2.50
D41D1	PNP	TO220	30	1.0	6.	150	S3027	.35	3.00
D44H8	PNP	TO220	60	10.0	50.	50		.50	4.50
RCA105	PNP	TO220						.35	3.00
MJE1091	"	TO220	60	5.0	70	PWR DARLINGTON		1.25	10.00
MJE1100	NPN	TO220	60	5.0	70	PWR DARLINGTON		1.25	10.00
TIP31A	NPN	TO220*	60	3.0	40W			.40	3.50
2N6101	NPN	TO220	80	10.0	75			.60	5.00
2N4304	N CHANNEL FET			TO106 CASE			sim. HEP802	.35	3.00
40327	NPN	TO-5	300	1.A	5W			.40	3.50

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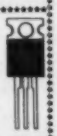

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Richard Bartholomew
Box 300 Butler Terrace
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Having seen several articles pertaining to automatic code identification, all using diode matrices or one-shots, I thought I'd share a circuit I developed for TV translators requiring much the same thing. This particular circuit uses only five ICs, three TTLs (cheap), one 5-volt regulator, and one 256-bit ROM (read only memory). There are also four transistors performing housekeeping chores such as inversion and pulse generation.

Referring to Fig. 1, the circuit operation can be explained as follows: IC1, an LM556 dual timer uses half of its internal circuitry to provide a 30-minute timer. The output of this timer is normally high. After timing-out, it goes low which turns off Q1 and forces the reset pin on the second half of the timer to go high. This enables the astable oscillator, and a clock stream, at about 8 Hz, toggles IC2, a dual 4-bit binary counter. This counter performs two functions. First, it addresses IC4, an 8-line-to-1-line multiplexer, which causes IC4 to selectively scan its inputs for a signal. Going back to IC2 now, it also addresses IC3, a 32 word, 8 bit/word ROM. The output of the first counter also drives the clock input of the second counter at a speed 8 times slower than the first half. This causes the multiplexer to scan each of its 8 inputs before the ROM address changes once.

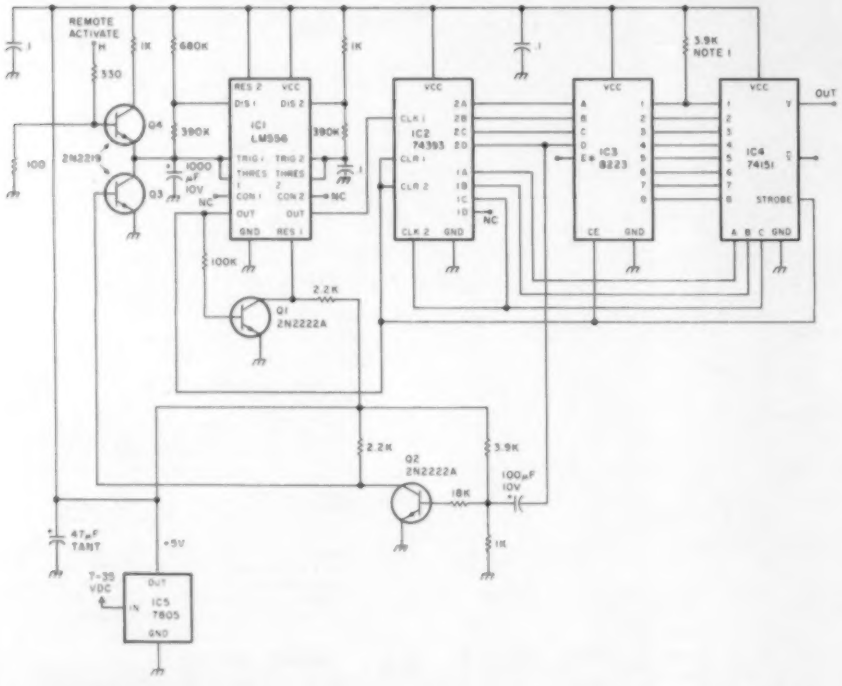

*Fig. 1. Schematic diagram of automatic code ID circuit. *Tie high or low depending on message desired. See text for details. Note: tie all output to +5 volts through 3.9k resistor. All resistors are ¼ W, 5%.*

The ROM is programmed as shown in Table 1. I always allow the first three bits at address 00000 to be 0. This allows for any clearing operations of the counters to complete before data starts flowing. In the example, I

used the letters "DE W79QY7." I allowed 3 consecutive 1s for a dash and one 1 for a dot. Spacing between letters is three 0s and spacing between words is seven 0s. The table is read from address 00000, A through H, then address 00001, A through H, and continuing down through binary address 01111. As can be seen, the ROM outputs 8 bits at a time to the 8 inputs of the multiplexer. This is the reason for running the multiplexer 8 times faster than the ROM. As each 8 bits appear on the inputs to the multiplexer, the inputs are scanned and converted to serial data at the Y output.

At the completion of binary count 16, the negative-going edge on the 2D output of IC2 turns off Q2 for a period of about 100 ms. This causes its collector to go high. This high voltage on the base of Q3 forces it into heavy saturation, discharging the time-out capacitor at TRIG 2 on IC1. This causes the timer to reset to zero and start timing out 30 minutes, when the sequence will repeat. Q4 was added to allow remote triggering of the timer. This is accomplished by either a logic 1 at the remote activation input or tying this point to +5 volts.

IC5 is simply a 5-volt regulator which takes anywhere from 7 to 35 volts input and converts it to 5 volts for the rest of the circuity.

This circuit can be programmed to provide two separate 128-bit messages, selectable at the flip of a switch. Input E on IC3, which is shown open on the schematic, can be tied to an SPDT switch which has one side grounded and the other tied to +5 volts. When switched to ground, the address to the ROM will start with 00000 and when switched to +5 volts, it will start with 10000.

Being a computer freak and not a ham, I am not sure if this circuit will be an aid to anyone, but if so, I would like to hear from you regarding your uses and any changes you might have made. (For amateur use, the 30-minute timer sequence would have to be shortened to 10 minutes. The sample call sounds like a rare one.—Ed.) ■

	Desired output of ROM							
BCD count to ROM	A	B	C	D	E	F	G	H
00000	0	0	0	1	1	1	0	0
00001	0	1	0	1	0	0	0	1
00010	0	0	0	0	0	0	0	1
00011	0	1	1	1	0	1	1	1
00100	0	0	0	1	1	1	0	1
00101	1	1	0	1	0	1	0	1
00110	1	1	0	1	1	1	0	1
00111	1	1	0	1	0	0	0	1
01000	1	1	0	1	1	1	0	1
01001	0	1	1	1	0	0	0	1
01010	1	1	0	1	0	1	1	1
01011	0	1	1	1	0	0	0	1
01100	1	1	0	1	1	1	0	1
01101	0	1	0	1	0	0	0	0
01110	0	0	0	0	0	0	0	0
01111	0	0	0	0	0	0	0	0
10000	0	0	0	0	0	0	0	0

Table 1. ROM programming sample. Sample indicated is W79QY7.

The Vacationer

—B&W's portable antenna

Steve Schwartz WA2ALT
2770 West 5 St. Apt. 18A
Brooklyn NY 11224

If you travel a lot or live in an apartment, there's a great little antenna for the low bands. B&W makes a low-band antenna covering 2-40 meters and it virtually takes up no space. The antenna is about 4½ feet long. When the antenna is disassembled, it can fit in a small suitcase with all your clothes. This antenna is the Vacationer™.

The antenna comes with four coils and a shorting bar for 6 and 2 meters. The Vacationer also comes with coax, counterpoise, and all mounting hardware.

Changing coils is a breeze. To change a coil, all you have to do is loosen two screws and the coil slides right off. Tuning the antenna is just as easy. The whip itself does not have to ever be touched (except on 2 meters). Tuning is done by adjusting the length of the counterpoise. The counterpoise can hang out the window or lie along the floor in the room.

There's nothing else to buy for the antenna. The antenna mounts on the window via a vise-type mechanism. It's also great for you apartment-dwellers who can't put up antennas.

The only "tool" needed for assembly and disassembly is a flat screwdriver.

The Vacationer antenna can be ordered from any store which stocks B&W parts. The number of the antenna is the Model 370-10. The antenna lists for approximately $32.50.

There is a previous model, number 370, which is less in price and does not include 40 meters. If you would like the specifications, write to Barker and Willamson, Inc., 10 Canal St., Bristol PA 19007.

It's a great little antenna and the swr is adjustable to 1.1:1. ■

Tone Decoder Improvements

—another step toward perfection

With a signal conditioner and valid-digit recognizer, you can't go wrong.

Rick Swenton WA1LMV
19 Allen Street
Bristol CT 06010

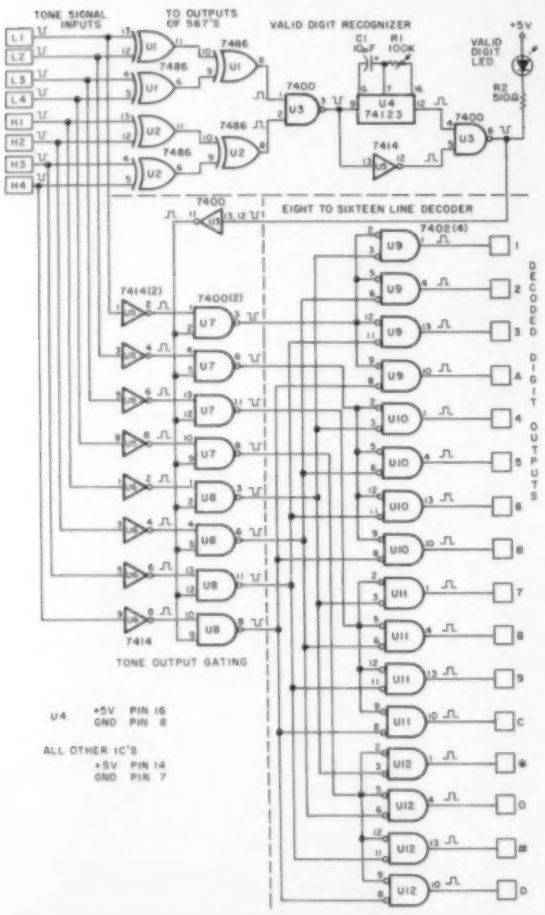

Fig. 1. Decoding system schematic.

The Signetics NE567 is my favorite toy. I'll never give it up. After working on several old telephone company decoders, I realized that they definitely leave something to be desired—especially if you were to attempt to build one from scratch! Also, after experiencing several commercial-quality state-of-the-art DTMF decoders, I realized that while they are terrific decoders, their price is out of sight. That leaves the NE567.

Mr. Everhart* described the limitations of the 567 in a very thorough presentation. However, its limitations can be worked around to yield a high quality, superior performing decoder. The 567 cannot stand alone without conditioning its output. The circuitry presented here is a sophisticated signal conditioner and valid-digit recognizer. It is an improved alternative to separate delay networks on the outputs of all eight 567s. (See Fig. 7 in referenced article.)

The block diagram of this system is in Fig. 2. It consists of two bandpass filters, one for the low-group tones, and one for the high-group tones, two limiters, eight frequency decoders, a valid-digit recognizer/signal conditioner, and an eight-to-sixteen-line decoder. To build your decoder, see Everhart's article for information on building the bandpass filters, limiters, and 567 decoders. The outputs of the eight 567 decoders are then fed into the valid-digit recognizer, Fig. 1. The valid-digit recognizer consists of U1 and U2 (7486 exclusive OR gates), U3 (7400 quad two-input NAND gate), U5 (7414 hex inverter), and U4 (74123 monostable multivibrator).

The function of U1 and U2 is to determine if the 567 decoders are sending only one low-tone signal and only one high-tone signal. The outputs of U1 and U2 are ANDed together by U3 so that the output of U3 (pin 3) goes low only when the following conditions are met: You

*J. H. Everhart WA3VXH, "Toward a More Perfect Touchtone Decoder," *73 Magazine*, November, 1976, pages 178-181.

must have only *one* low tone *and* only *one* high tone.

The next section of the valid-digit recognizer is the delay circuit consisting of U3, U4, and U5. R1 and C1 determine the time delay. The output of the valid-digit recognizer circuitry is U3, pin 3. Pin 3 of U3 goes low only when one low tone AND only one high tone are present and they must remain uninterrupted for the time duration set by R1 and C1. Optimum setting of R1 is from 0.25 to 0.5 seconds. This setting may vary for your particular setup. As a rule of thumb, set R1 to be fast enough for your signaling requirements, but slow enough to reject erratic pulsing. Remember that a condition could exist where a certain voice may be decoded as two tones which happen to be two touchtone™ frequencies. This would meet the requirements of only one low and only one high tone, but would not be decoded if R1 were set correctly.

Next, we use the output of the valid-digit recognizer to gate the outputs of the 567s into the eight-to-sixteen-line decoder. U5 and U6 are 7414 Schmitt triggers. They will further condition the outputs of the 567s and shape the output waveform. U7 and U8 (7400 NAND gates) provide the gating of the 567s to the sixteen-line decoder. Thus, no tone decoding can take place without valid-digit recognition because the outputs of the 567s are not being applied to the sixteen-line decoder unless valid-digit recognition has occurred. The outputs of the sixteen-line decoder, U9-U12 (7402s), are normally low and go high when the digit is decoded.

The system described here is in use at three repeaters in the Hartford CT area (WR1ABM: .28/.88 and 442.85-447.85 and WR1AFU: .75/.15) as autopatch and control decoders and are working well without any problems. With a 0.5-second response time, there has never been a false activation of any function. ■

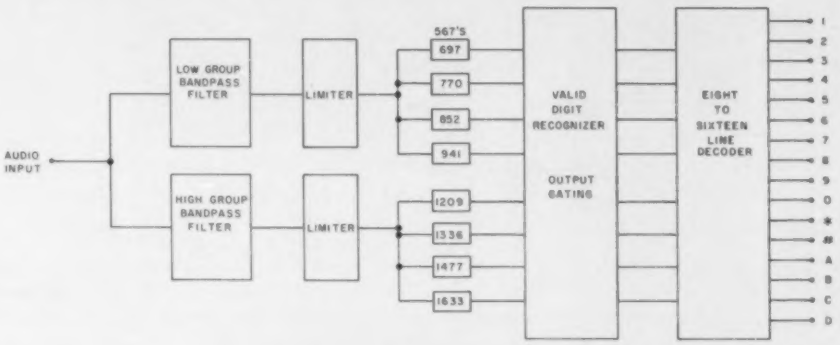

Fig. 2. Block diagram of decoding system.

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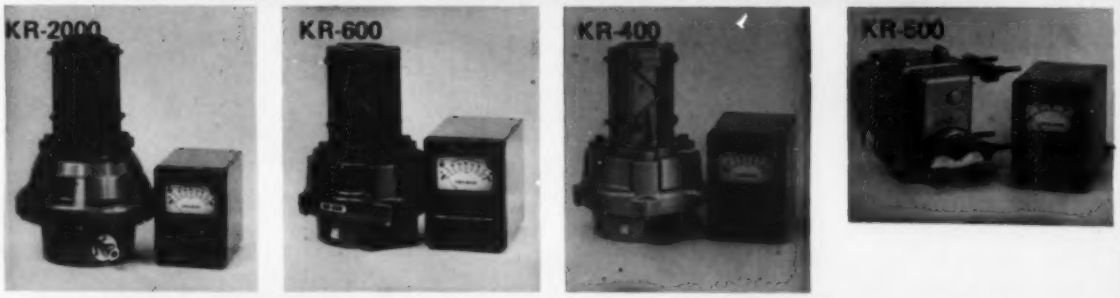

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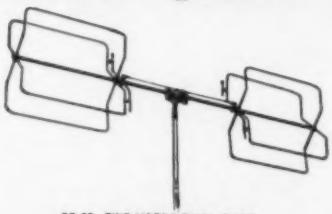

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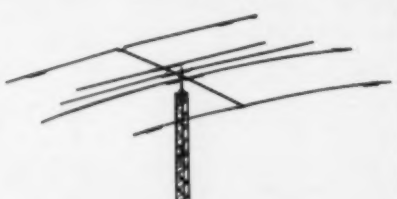

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The All-Wrong Power Supply

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Usually when one builds a power supply, one takes a currently vogue circuit and uses it verbatim. For solid-state rig advocates, the present norm is using a transformer, a diode-bridge rectifier, and a series pass transistor. While I have no qualms about this circuit, I know many hams who spend time and money looking for the "proper" parts when, in reality, they can use junk box parts in an equivalent circuit.

The circuit in Fig. 1 is the power supply I have been using for my Icom IC-230. It delivers about 3.5 Amps at 12 volts. When one looks at the schematic, however, the circuit *looks* wrong. First, the transformer voltage is too high and everyone *knows* there are four diodes in every power supply worth mentioning. How can it work?

First, consider the transformer, rectifier, and filter capacitor combination. The output voltage with transformer secondary voltage V_t, load current I_l, and capacitor C connected in a half-wave circuits is: $V_{out} = 1.4V_t - I_l/120C$. The ac ripple on this voltage will be: $V_{ripple} = I_{out}/210C$. Inserting our values we find the following: $V_{out} = 1.4(28V) - 4$ Amps/$(120 \times 4 \times 10^{-3}$ Farad$) = 30.87$ volts and $V_{ripple} = 4/(210 \times 4 \times 10^{-3}) = 4.76$ volts. Thus, the output is a dc level of 30.87 volts with a 4.76 volt ac voltage impressed upon top of it. Therefore, we have a varying voltage from 26 to 36 volts at the input to the regulator.

We have just shown why we are using a higher voltage transformer with a half-wave rectifier. The transformer chosen was a surplus one with a 28 V, 4 A secondary, bought for $1.00. This is in contrast to the 18-volt types usually chosen for a similar supply, then operated with a bridge rectifier.

Practically, what these equations show is that if our regulator can follow an input voltage from roughly 25 to 36 volts, we can use this circuit to make a regulated power supply at a variety of voltages. Before slapping a three-terminal regulator on the output and going to look for a "cold 807," one must do a little more designing.

Returning to the voltage output equation, we note that at zero current our voltage across the filter capacitor is 1.4×28 or 39.2 volts. This value is the maximum voltage across the capacitor. Then a capacitor with a working voltage of at least 60 volts should be used.

The standard three-terminal regulators have a maximum input voltage of about 35 volts. Therefore, one might damage or destroy the regulator if it were connected directly to the rectifier output. The zener diode (Z) and the resistor (R) in the schematic take this into account. The zener was chosen from the junk box and almost any power-type zener can be used as long as the regulating voltage is below 35 volts.

The value of resistor R can be easily found. The current through the regulator is roughly the base current of the transistor which is roughly the collector-emitter current divided by the gain of the transistor. Since a typical power transistor has a gain of about 50 and our maximum output current is about 3.5 Amps, we see that the base current is about 70 mA. Since our lowest voltage across the capacitor is about 25 volts, we want something like an 8-volt drop with 70 mA or about 100 Ohms.

Although the drop across the resistor is constant, the actual voltage input to the regulator will vary from 17 to 27 volts. This can influence the choice of zeners since a 25-volt zener will only draw power when the voltage is above 25 volts and, therefore, has a smaller duty cycle than would a 20-volt one. Maximum heating on a 25-volt zener would occur with no current drawn by the regulator. In this case, it would be about 10 mA, so a 1-Watt zener should do. The resistor will dissipate 10 volts at 80 mA, so a 2-Watt one will be fine.

The final bit of analysis deals with the diode (D2) on the ground leg of the three-terminal regulator.

This is used to raise the regulator voltage up by .7 V so a "12-volt" regulator will give a 12-volt output.

No analysis will be given of the power transistor since my only suggestions are to heat-sink it well, choose one with a gain of about 50, and a power of about 75 Watts. A 2N3055 is an inexpensive and usually safe choice. The small capacitor across the output is used for protection from oscillation. Although I have never had a supply oscillate, the capacitor is cheap insurance.

Parts List

D1	10A, 60 piv silicon diode
D2	1A, 15 piv silicon diode
U1	7812, 12-volt positive voltage regulator
Q1	2N3055 transistor
R,Z	See text

The supply was constructed on a piece of particle board with plywood sides and a U-shaped cane metal cover for ventilation. A little decorative stain made the XYL joyfully approve of the supply for use in the den instead of being hidden away.

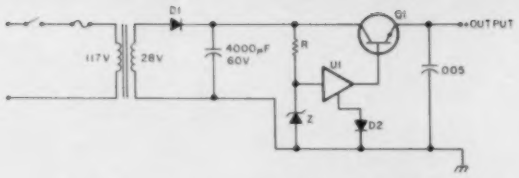

Fig. 1. Power supply schematic diagram.

The design of this supply is neither unique nor innovative, but it shows that one can build a power supply from the junk box that really works. ■

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The Hardhearted Rf Detector

—insensitive to harmonics

Over the years, the thermal, or calorimetric, wattmeter has remained the standard for all measurements of radio frequency power. Unfortunately, calorimetric power meters are very expensive and, therefore, are found only in the laboratory. Almost without exception, the front panel "power" meter found on a radio transmitter is really a peak-reading voltmeter calibrated to approximate a reading in Watts. Any harmonic energy from the transmitter due to misalignment or component failure can cause this meter to soar to a reading much higher than the true rms power output. The obvious solution has been overlooked. Every radio transmitter can be equipped with a simple power metering circuit offering accuracy and insensitivity to harmonics approaching that of a thermal-type meter.

In place of the usual detector followed by a capacitor input filter, the improved circuit will employ a choke input filter. This circuit, properly designed, will develop an output equal to the average dc level of the half-wave pulsating dc from the detector (resemblance to the choke input power supply filter is not accidental). An average reading voltmeter may be calibrated to read the true average power dissipated by a load. The ratio of average power to rms power remains relatively constant for extreme distortions of the sine wave, while the power, computed by the square of the peak voltage divided by twice the load resistance, may vary several decibels.

This simple high-accuracy circuit has but one special requirement. The input inductor must be chosen so that its effective inductance remains above the critical value required for voltage regulation to the average level over the frequency band of interest. Therefore, a choke approaching self-resonance at the operating frequency would not be suitable. The critical value is computed by: $L_{min} = (0.060/F)R_L$ henrys.

A typical circuit for use at a 50-Ohm termination, where $X_{C1} \leq 5$ Ohms and $X_{C2} \leq R_L/10$, is shown in Fig. 1, and the results from low-frequency (F = 40 kHz) test circuits (Figs. 2 and 3) are shown in Table 1. ■

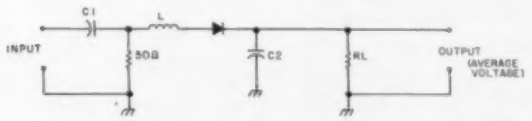

Fig. 1.

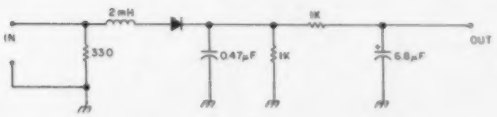

Fig. 2. Peak detector.

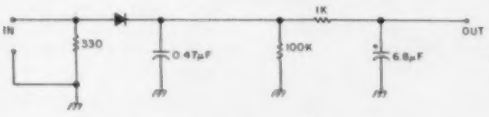

Fig. 3. Average detector.

Input	Calculated rms power	$E_{Peak\ det.}$	$E_{Avg.\ det.}$
8.0 V p-p triangle	0.016 W	3.5 V	1.0 V
6.5 V p-p sine	0.016 W	2.9 V (4.4 dB)	1.0 V
4.6 V p-p square	0.016 W	2.1 V	0.98 V

Table 1.

Custom-Designed Power Supplies

— try the 723

Bargain-basement fanatics will love this new approach.

Carl S. Griebno K2GEJ
R.D. #2 Kline Drive
Pennellville NY 13132

LSI, microcircuits, mass production, and high component costs are but a few of the many reasons that are leading to the demise of amateur radio home brewing. In spite of this, there are plenty of well-documented circuits for you to select from that will not wind up costing a fortune to build (see any issue of *73*). Unfortunately, most of them require a power supply which can wind up with a price tag as large or larger than the rest of the project.

If you are considering bargain-basement electronics, you should also anticipate the problems associated with quality, reliability, and aesthetic appeal. There are precious few units I would let adorn my operating table.

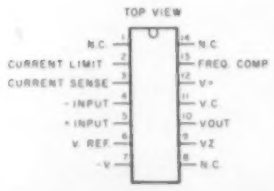

Fig. 1. Pin designation for the 723.

This article will show you how to custom-design your next supply, featuring the widely used 723 IC regulator. This will allow you to have the supply best suited to your application and provide the quality, reliability, and features you desire. All this is at a surprisingly low cost. You should find the design calculations relatively easy and the assembly straightforward.

The 723 Chip

There are many features of the 723 IC, one of which is a temperature-compensated and amplified reference voltage output (Fig. 1, pin 6). This output voltage is typically 7.15 volts and capable of supplying up to 15 mA of current. Current-sense terminals (pins 2, 3) allow the user to select the upper current limit of the supply. Also, the 723 has a built-in error amplifier directly coupled to an "on-board" series pass transistor. This combination is capable of supplying up to 150 mA. The line and load regulation of the supply will be typically 0.1%. Some of the 723's other features are low current drain, low temperature

drift, and high ripple rejection. Another good feature is the $.35 to $.50 price tag in single quantities. It is, in fact, uncommon not to find a 723 stuck somewhere in an OEM industrial supply.

External Components

Before we get into the design calculations, take a look at Fig. 2. T1, C1, and Q1 (or Q1 alternate) are the only external components needed for this supply, the remainder of the components being mounted on the PC board. Looking at T1, you can see I have drawn a center-tapped transformer. If you have this type of transformer, diodes D1 and D2 are used in a full-wave, center-tapped configuration using pads C, D, and E on the PC board. If your transformer has no center tap, use diodes D1 through D4. Connect the transformer leads to pads C and D on the board and you have a full-wave bridge configuration. I have found that a 12-volt filament transformer with a bridge rectifier works extremely well for output voltages from 2 to 7 volts and a 24-volt control type transformer with a bridge rectifier is an excellent choice for output voltages of from 9 to 25 volts. Make sure the transformer secondary current rating is high enough for your supply design. There will be some more comments about T1 later on.

Diodes D1 through D4 must be chosen to handle the current you design the supply for. The popular 1N4000 series diodes are excellent for current levels of up to 1 Amp. The 3-Amp epoxy "bullet" rectifiers are so inexpensive that I try to keep some on hand all the time (MR 500 series). If you are fortunate enough to be able to obtain some Motorola MR 751s, a 6-Amp device, these also may be used on the board. The diodes should have a piv rating of at least 50 volts. By using a glass-epoxy board material with 2 oz. copperclad, the runs on the board are easily wide enough to handle 6 Amps with less than 10° C temperature rise. For design currents higher than 6 Amps, the rectifiers, filter capacitor (C1), series pass transistors (Q1, alt.), and C3 may be wired externally with heavy wire. The circuit board can then be wired in as a control system for the regulated supply. (See Fig. 3.) If you use the board in this manner, do not use R7, which is the current-sensing resistor. Mount the fuseholder for F2 externally, instead of in the hole provided on the PC board, and fuse for the design current. Although not shown in Fig. 2, it is a good idea to wire diode D6 at the output terminals of the supply. This is a "free-wheeling" diode that will protect the regulator board from any inductive transients coming back to the supply from the load (e.g., a T-R relay). A 3-Amp, 200-piv device is suitable for D6.

At this time, it is worth mentioning that Q2 (Fig. 2) will require some heat sinking at the higher current output levels. To do this, you might even wire an externally mounted 2N3053 or 2N3055 to the Q2 pads located on the PC board.

Unless you have a river flowing nearby to cool Q1, a bit of caution must be exercised in what is done here. A 2N3055 has a power dissipation specification of 115 Watts if you can keep the case temperature at 25° C (77° F). Following a derating curve for this transistor, Q1 can dissipate up to 63 Watts at a case temperature of 100° C (212° F). What this translates to is approximately 4 Amps of current with a 15-volt drop from collector to emitter. Allow one 2N3055 for every 4 Amps of output current and, by all means, heat-sink them! Also, if you sink Q2 well, it is capable of driving up to four 2N3055s connected as shown in Q1 (alt.). The other alternative, as previously mentioned, is to externally mount Q2 and wire it into the board. The bottom line here is to keep

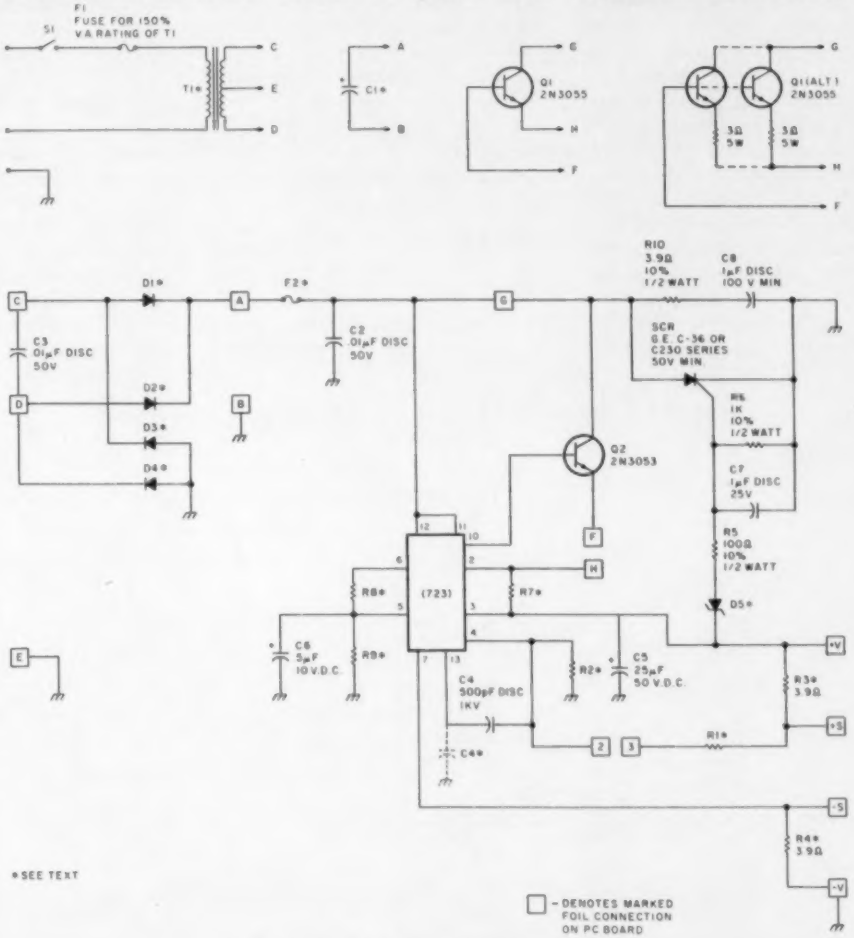

Fig. 2. Power supply schematic diagram.

the Q1 and Q2 case temperatures below 100° C to achieve the best reliability.

There will be a special section on C1 later on in this article.

Overvoltage Protection (ovp)

The ovp circuit, an SCR crowbar-type, is optional in that it has no effect on the operation of the regulator. If, in fact, you opt for a variable supply, it can be a nuisance. But, if you have a nice new SSB rig, it can save you a bundle. The circuit consists of an SCR, C8, R10, C7, R6, D5, and R5. The only variable in the circuit is zener diode D5. The zener should be rated 2 to 3 volts higher than the regulated output voltage and have a 5% tolerance. The ovp circuit operates as follows: Any rise in the output voltage above the rating of D5 will fire the SCR. After firing, it will remain in the on state until fuse F2 blows, thereby protecting the load from a gross overvoltage. Choose a rating for F2 approximately 20% above the design current. Resistor R6 prevents any anode-gate leakage current from inadvertently firing the SCR. Capacitor C7, along with R5, acts to prevent any power line switching transients from firing the SCR. This is especially true under no-load conditions. C8 and R10 form a dv/dt (voltage change to time change) network that prevents the SCR from turning itself on due to high rate-of-rise voltage excursions across the device. There are anode and gate pads for the SCR clearly marked on the board. Also, there is a hole drilled in the common foil, just below the SCR mounting hole, for the cathode connection. When mounting the SCR, use the insulating washer that usually comes with the device. The stud is the anode connection and, without the washer, the mounting nut will come in contact with the common foil. If there is no insulating washer with the SCR, one can be easily fabricated by peeling the copper from a small piece of circuit board material. The unclad material may then be used as the washer.

Remote Voltage Sensing (rvs)

Rvs, a feature of this supply, is seldom discussed in literature. To better understand the value of rvs, let's take a look at what can happen when it isn't used. All electrical connections are imperfect, as they have some resistance associated with them. The same holds true for wire. Consider a connector resistance of 50 milliohms and a power lead resistance of the same magnitude. That is like putting a resistor with a value of 0.15 Ohms (two terminations and a conductor) in each lead of the power cable. This comes to a total resistance of 0.3 Ohms. That doesn't sound like much, but, when multiplied by 10 Amps, the resultant voltage drop in the cable is 3 volts. Not good! Now, if we could sense voltage out at the load, the cable drop would still be there while the regulator is being "fooled" into putting out enough extra voltage to compensate for this drop. With this supply design, all that has to be done is to run two small wires in parallel with the power cable wires. Tie them together at the remote load location and you have rvs. (Connect the +S and the +V wires together, also the −S and the −V wires.) The reason you may use smaller wires is due to the fact that only a few milliamps of current are required to drive the error amplifier in the 723. Remember, the higher the current levels that you work with, the more important it becomes to use rvs. R3 and R4 are shown to be 3.9 Ohms. Any value you happen to have between 2 and 10 Ohms will be satisfactory here. If you do not wish to use remote sensing, a jumper may be installed in place of R3 and R4.

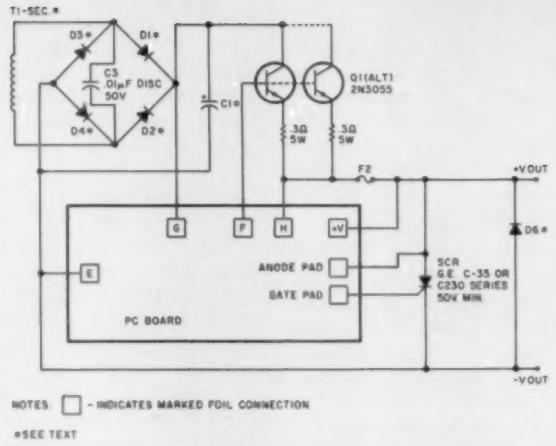

Fig. 3. Wiring arrangement when the 723 is used as a control system for an external regulated supply. Run rvs wires from PC board. Do not use jumper (Fig. 4).

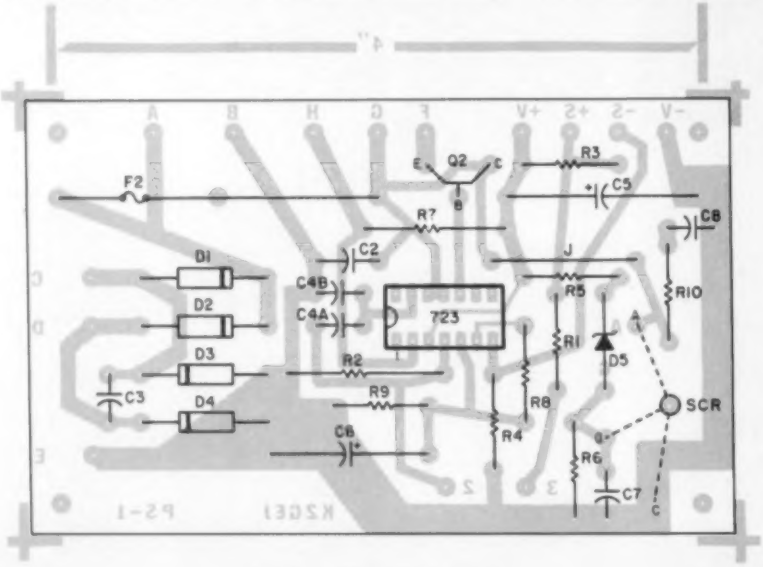

Fig. 4. Component layout.

Let's Regulate

The regulator portion of this supply consists of C2, R8, R9, C6, the 723 IC, C4,

Q2, Q1, R7, C5, R2 and R1 (Fig. 2). The circuit, when constructed with a jumper between pins 5 and 6 of the IC (in place of R8), is for output voltages of between 8 and 24 volts. Do not use R9 and C6 in this case. Remember our reference voltage (V_{ref}) output of 7.15 volts? In this connection, the reference voltage is applied directly to the (+) input of the error amplifier. Therefore, the (−) input of the error amplifier *must* be 7.15 volts in order for the 723 to be in a stable condition at V_{out}, pin 10. Let's go through a simple calculation and see how we can design for an output voltage of 13.5 V dc so that you can run your new 2 meter rig or maybe a mobile unit brought in for the winter. Looking at the schematic, we see that the voltage at pin 4 of the IC, the (−) input of the error amplifier, is derived from a voltage divider R3, R1, pads 2 and 3, and R2 and R4. R3 and R4 are very low value resistors that allow for rvs and, therefore, have no effect on our calculation. Pads 2 and 3 allow for an external voltage adjustment if desired. So now we're down to two resistors, R1 and R2. The value of R2 is not critical (somewhere between 1k and 3k is fine), but must be chosen first. Let's say a 2k resistor is handy for R2. The voltage across R2 must be equal to our reference supply, again 7.15 volts. Our supply is supposed to operate at 13.5 volts, so the voltage across R1 will be 13.5 volts minus the drop across R2 (7.15 volts). A proportion will give us the value for R1. The equation is as follows:

$$\frac{R1}{V\ R1} = \frac{R2}{V\ R2}$$

Solve:

$$\frac{R1}{13.5 - 7.15} = \frac{2k}{7.15}$$

$$7.15 \times R1 = 6.35 \times 2k$$

$$R1 = \frac{6.35 \times 2k}{7.15} =$$

1776 Ohms.
Use 1800 Ohms, 5% tolerance, 1/4- or 1/2-Watt.

This will give you an output voltage very close to 13.5 volts. If you would like to trim V_{out}, use a 1300-Ohm resistor for R1 and wire a 1k variable resistor to pads 2 and 3. This will give you 13.5 volts output at approximately 50% of pot rotation, giving you plenty of trim range. Otherwise, don't forget to jumper pads 2 and 3 if you use a 1.8k resistor for R1. When using the 8-through-24-volt connection, place C4 at C4A, Fig. 4. C4 is the compensation capacitor and provides a high-frequency breakpoint in the error-amplifier circuitry, preventing unwanted oscillations.

In order to use the supply for voltages of less than 7 volts, only minor changes need be made. Resistor R2 will *not* be used. Place a jumper in pads 2 and 3 and also in place of R1. In doing this, the output voltage will be placed directly on the (−) input of the error amplifier. Let's say we want 5 volts output for some TTL circuit we have or maybe that new microcomputer the UPS man just delivered. All that has to be done is to divide the 7.15-volt reference supply down to 5 volts. This calculation will be the same as the previous one. Choose R9 (any value from 1k to 3k). Let R9 = 1k. This time the equation is:

$$\frac{R9}{V\ R9} = \frac{R8}{V\ R8}$$

Solve:

$$\frac{1k}{5} = \frac{R8}{7.15 - 5}$$

$$R8 \times 5 = 1k \times 2.15$$

$$R8 = \frac{1k \times 2.15}{5} =$$

430 Ohms.

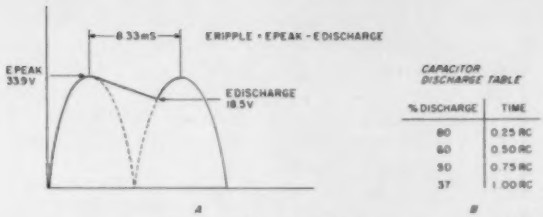

Fig. 5. C1 calculations.

Use a 5% tolerance, 1/4- or 1/2-Watt resistor. Now we have the R8 and R9 values we need for our 5-volt supply. Capacitor C6 is used to filter out any "white noise" present in the V_{ref} output and in R8. Also, place C4 at C4B, Fig. 4.

For output current levels of 6 Amps or less, R7 must also be calculated. R7 is the current-sense resistor and its value will set the maximum output current of the supply. When the R7 voltage reaches 0.6 volts, the 723 will start reducing the output voltage in an attempt to keep the output current constant. This calculation is the Ohm's Law relationship R = E/I, where R is the value of R7, E is 0.6 volts (the specified CL − CS voltage), and I is the supply current limit. The calculation for R7 is as follows: R = 0.6/2 Amps = 0.3 Ohms. Don't forget the power dissipation in R7. That calculation is as follows: P = E × I = 0.6 × 2 = 1.2 Watts. At the risk of not having current limiting, or waiting until you can procure this low value resistor, a jumper may be used in place of R7. As long as R7 is in place, the supply can even stand intermittent short-circuit conditions at the output terminals with no resulting damage.

If you've read this far, it's time to get a cup of coffee or maybe a nice cold 807. We still have a little more to go.

C1 Calculations

There are various ways to find a value to be used for C1; most of them use higher mathematics. To me, that is an exercise in futility. What I will explain here is a simple method that works very well, and can be easily verified if you have access to an oscilloscope. Again, for the sake of numbers, let's work on a 13.5-volt, 2-Amp supply design. I will assume you have found in your junkbox a 24-volt center-tapped transformer. The first step is to add 5 volts to your design output voltage. The reason for this is to make absolutely sure that there is enough voltage to overcome the base-emitter drops (V_{be}) in the regulator transistors, and give the series pass transistors some "operating room." Adding 5 to 13.5 volts gives us 18.5 volts. This value is placed at the point labeled E DISCHARGE, Fig. 5. Now, suppose you would like to use the full-wave, center-tapped connection as previously mentioned. Divide the 24-volt rating by two. The reason this is done is that you are only using half the transformer winding by connecting the center tap to common. This will give you 12 volts, which is an rms value. To find E PEAK, the value C1 will charge to, multiply 12 volts by 1.414 (E PEAK = E RMS × 1.414). This value, 16.97 volts, does not meet the minimum value of 18.5 volts required by the supply design. E PEAK should be a minimum of 5 volts higher than E DISCHARGE, or the filter capacitor (C1) will become very large (ex-

pensive). This dictates the use of the 24-volt transformer in a bridge rectifier configuration. It also means that you have to come up with two more diodes. The value for E PEAK will now be 24 × 1.414 or 33.9 volts. Now we have 15.4 volts before we're down to the E discharge value. The next step is to find out what percent 18.5 volts is of 33.9 volts. Divide E DISCHARGE by E PEAK. 18.5/33.9 = .5457 or 54.57%.

Now go to the capacitor discharge table in Fig. 5 and find a percentage value closest to the above calculation, in this case 50%. Across from this you will find 0.75 RC. What this means is that in the 0.75 time constant, the capacitor will discharge to 50% of its initial value, E PEAK. Now R × C is a formula we can work with to find the value for C1. Remember t = RC? To find a value for t to be used in this formula, solve the equation 8.33 milliseconds = 0.75t. The time value, 8.33 milliseconds, does not change, as it is the period between the pulsating dc peaks that charge C1 (60 Hz line frequency). 0.75 is the table value reached by the E PEAK, E DISCHARGE calculations. Solving the equation, we get: t = 8.33/0.75 = 11.1 milliseconds.

We now need a value for R to complete our C1 calculation. This value can be found from R = E/I where E is the E PEAK value and I is the supply current design value, or 2 Amps. Solving this equation, we get R = 33.9/2 = 17 Ohms.

To find the value of C1, use t = RC. Solving this, we get: 11.1 milliseconds = 17 Ohms × C. C = 11.1/17 = 0.652. To get uF, multiply 0.652 × 1000 = 652 uF for C1. Now 652 uF is the minimum value. Any capacitor of this value or larger is suitable. The voltage rating for C1 has to be greater than E PEAK. In this case, a 50 V dc unit should be used. This method is a bit arduous, but, nonetheless, it's a lot easier than some other methods.

Potpourri

I would like to make some more comments about T1 at this time. Transformers with secondary current ratings of two to three Amperes are very reasonable. If you would like to design a 12-volt, 10-Amp supply, the transformer cost may become quite high. Remember the older tube-type TV sets? The power transformer used in these sets is good for 350 Watts continuous duty. In the *Radio Amateur's Handbook*, in the power supply section, there are excellent instructions on rewinding transformers. Also, in the section on construction practices, you can find a copper wire table that will guide you in selecting the right size wire for your new secondary winding. Rewinding is not difficult and your efforts will be well rewarded. Another advantage is that rewinding enables you to keep the Q1 power dissipation down by reducing the E PEAK (Fig. 5) value to a reasonable level for your supply design.

At no place in this article have I mentioned tying common (−V) to the chassis. Also, on the PC board artwork (Fig. 6) you will not find any mounting holes in the common foil. This is done for two good reasons. The first is safety! Connect that third wire (green) in your power cord to the chassis. All of your equipment should be well grounded. The second reason is for convenience. With a floating supply, the positive and negative connections may be treated just like a battery. Remember that microprocessor the UPS man just delivered? Just found out you needed a negative supply for some PROMs? Build two of these supplies. Tie the positive output of one to the negative output of the other and you have a plus/minus supply. The applications are unending.

In Summary

I believe an outline of the steps you need to go through in designing this supply is in order. First, the regulated output voltage and rated current must be selected. If the voltage is above 8 volts, calculate the values for the R1 and R2 voltage divider. If the voltage is 7 volts or less, calculate the R8 and R9 voltage divider. If R7 is used, calculate that value. Select zener diode D5 in the ovp circuit if used. Select resistors R3 and R4 if rvs is to be used. Decide on the number of transistors to be used at Q1 or Q1 (alt.), and select the correct diodes for D1 through D4. Finally, run through the T1 and C1 calculations.

This sounds like a lot, but many of the above steps are quick and easy. The remainder of the components mounted on the PC board are common to all designs.

The 723 is a great IC. Give this supply your best shot and I'm sure you'll be very happy with the results. For those of you who wish, I can supply a high-quality predrilled circuit board for this article. The cost is $4.50 postpaid. An SASE will bring an answer to any questions you may have.■

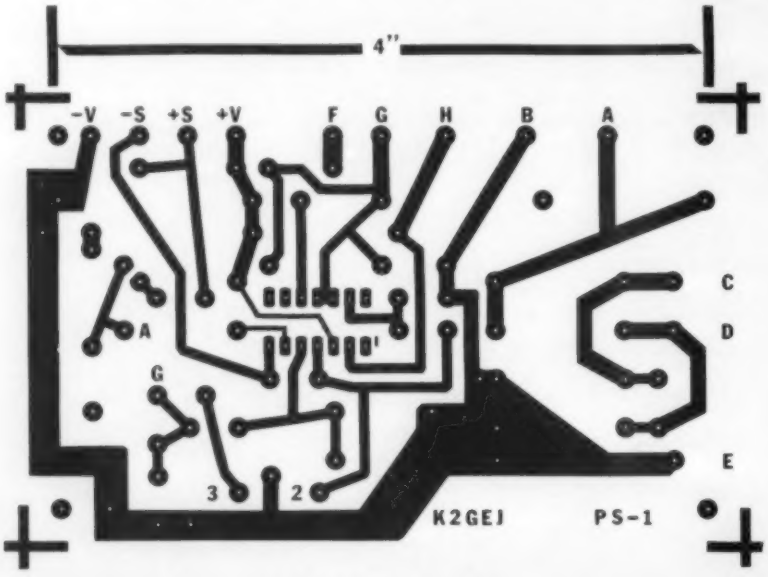

Fig. 6. PC board artwork.

A Touch of Class

—nifty $35 operating console

For comfort and convenience, this bench can't be beat.

Horace M. Lewey, Sr. WA4CUD
2405 Cyprus Street
Greensboro NC 27405

Console design can make a world of difference in your enjoyment of ham radio. Comfort, convenience, and ease of operation were the criteria set for the construction of this operating bench. The finished product provides all that and is very strudy as well.

Figs. 1, 2, and 3 show how everything goes together. The parts list gives all the materials you will need.

You should countersink all holes for the bolts and screws, fill them with plastic wood, and sand them smooth before painting or staining. This will give you an attractive finish. Leave a one-inch overhang on the sides of the top shelf and the desktop, as you can see in the photo. ■

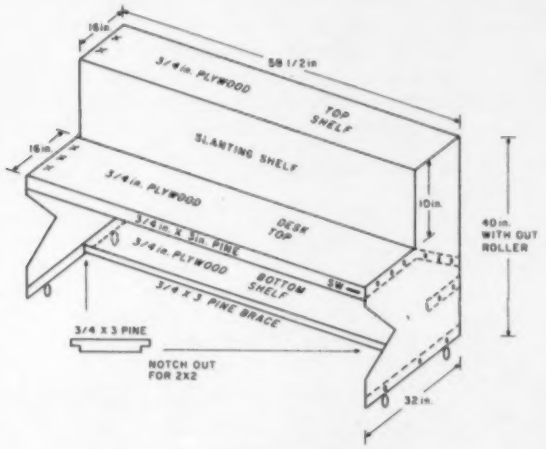

Fig. 1.

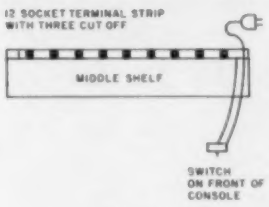

Fig. 2.

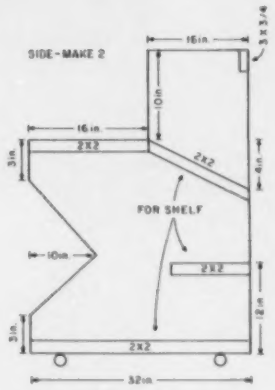

Fig. 3.

Parts List

two	¾" x 4' x 8' plywood
four	2" x 2" x 8' pine or oak
three	¾" x 3" x 6' pine (for front panel and shelf braces)
24	¼" x 2½"-long bolts
24	flat washers
four	roller casters
small can of plastic wood	

How To Bury Coax

— the garden cultivator technique

Ye keep what ye sow.

Max Holland W4MEA
Rt. 3, Rawlings Lane
Madisonville TN 37354

A ground plow is often used to bury coax cable. This special device usually is attached to the rear of a tractor and can put the cable down 8-12 inches in the ground. See *Ham Radio*, May, 1970, page 66, for procedure.

Having no access to a ground plow, I had to use the Armstrong method. It is difficult to bury 100 feet of coax cable in this manner. Using the tip of a chain saw to cut a slot in the ground is dangerous and is hard on the chain.

My neighbor, WA4KJA, has a garden cultivator which has been in his family since the 1930s. By changing to a narrow plowshare which was made from a piece of band iron 1½ inches wide, we were able to make our own ground plow.

The work is still hard, but it is easier than using a shovel. The narrow cut in the lawn disappears after several weeks.

The garden cultivator is a Planet Jr. made about 1935. Over the past 50 years of amateur radio, people have operated mobile from cars, airplanes, boats, bicycles, balloons, lawn mowers, go-carts, and tractors. To the best of my knowledge, this is the first time anyone has operated from a garden cultivator. The rig is a TR-22 with 1-Watt output. The antenna is a 5/8-wave whip. The antenna pattern will change depending on the depth of the cut. ■

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Four or five years ago, there was a terrific bargain at a northern Michigan hamfest. I unloaded a junky Hallicrafters S-38 for fifteen dollars, and spent the money immediately on a cardboard carton labeled "Mobile Stuff." Along with a lot of really useless junk, I found a Hustler mast, a bumper mount, three resonators for 80, 40, and 20, a desk mike, and twenty feet or so of good coax. The mobile antenna was bolted to the rear bumper of my trusty Barracuda right there in the hamfest parking lot, and, with an aging NCX-3 and a borrowed Heath HP-13 supply, I was on the air almost immediately and enjoyed several years of rewarding low-cost mobile operation.

Almost four years later to the day, while visiting some friends at a conference in Lansing, Michigan, I came out of a motel to behold a horrible sight: The mast, mount, and the eighty meter resonator had been ripped off, leaving the chrome bumper itself twisted like a pretzel! Fortunately, the rig itself was safe, still tucked under my pillow in the motel room, and I had purchased a spare resonator for a couple of dollars the year before. For the rest, I headed straight for my (former) auto insurance company, Divestiture & Bombast Mutual.

Following lengthy negotiations, I left the insurance office with ten measly dollars in search of a new antenna and insurance carrier. One look in a catalog, which listed the mast section itself for over twenty dollars, was so discouraging that I shelved the whole project, resolving to limit my mobiling to VHF until another hamfest bargain came along.

Several years more went by, and I replaced the venerable Barracuda with the bent bumper because I could no longer stand 10 miles per gallon on premium gas. A long Thanksgiving vacation trip to a science fiction conference in Champaign, Illinois, was coming, and, while I now had a good 2m FM rig, I would be out of range of repeaters for a good part of the journey. I decided to try and build a replacement for the missing Hustler. I had managed to come up with a spring similar to the one on the original bumper mount for a dollar from a CB friend. This left about nine bucks in the fund, no machine shop facilities at hand, and a few days left before Thanksgiving. Could it be done? Of course!

The Mast

After some thought about aluminum or steel conduit, a helically-wound PVC pipe, and other substitutes, I decided to go with a rigid copper pipe for the mast. It was sturdy, not too expensive, and an excellent conductor. Two sizes were available at the local hardware store, ½" and 3/4". The trick would be to come up with fittings to match the 3/8" × 24 threads on the remaining resonators, using only simple hand tools and hardware available in a small-town corner store the Wednesday before Thanksgiving.

The 3/4" tubing was sturdier, heavier, and required two fittings less than the ½" size. It would also have a slightly lower resistance loss at rf frequencies. On

Changing resonators.

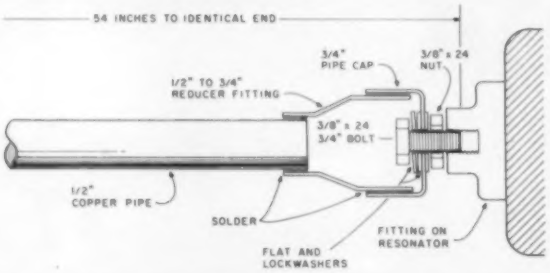


Fig. 1. ½"-pipe version. Mast-to-resonator fitting.

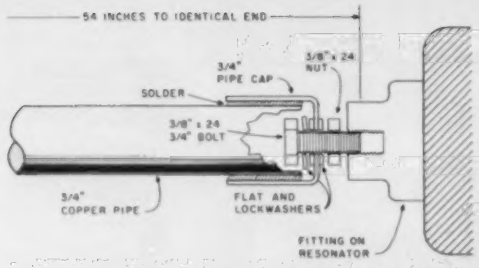


Fig. 2. 3/4"-pipe version. Mast-to-resonator fitting.

the other hand, its larger cross section and wind resistance might make it "whippier" in crosswinds on the freeway.

The ½" tubing was chosen because it was lighter, cheaper, and more closely matched the dimensions of the original Hustler chromed-brass mast. Cost was about 45 cents per foot, or close to $2.50 for a 54-inch length. Had time allowed, used copper pipe could have been obtained for about half this amount, but it would have required extensive cleaning.

Mast-to-resonator and mast-to-spring adapters were made up using store-bought plumbing parts (see Fig. 1). The same design would work for a 3/4" mast, simply by omitting the ½"-to-3/4" reducer fittings (see Fig. 2). The 3/4"-diameter ends are needed for clearance for the hardware.

Making the Adapters

Clean the tubing and fittings carefully with a rag and automotive rubbing compound or some other mild abrasive. Salt and vinegar will also clean the copper chemically, but I found the rubbing compound much faster. Clean the residual abrasive, fingerprints, etc., off the parts with a solvent like alcohol, acetone, or carburetor cleaner. Do this outdoors or in a well-ventilated area, and keep the solvent away from sparks and flames. Handle the parts with gloves or a clean rag, and you'll be able to solder them easily with ordinary rosin-core solder.

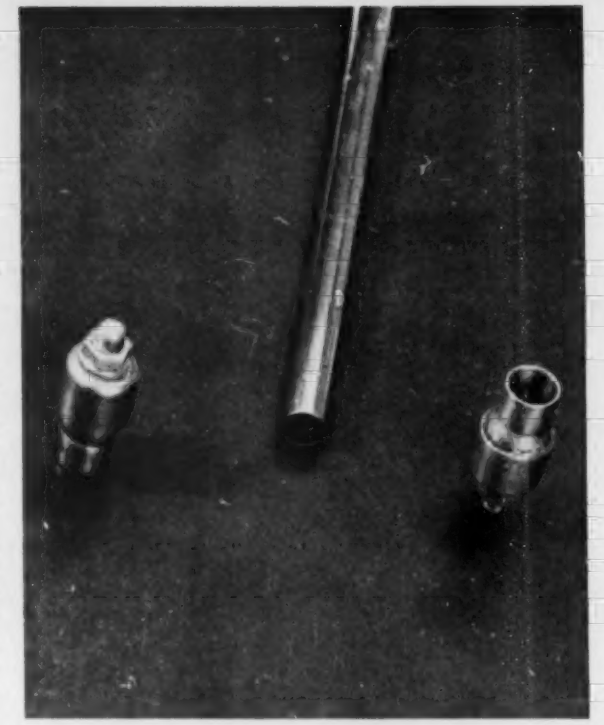
Center-punch the 3/4" end caps and drill them with 3/8" holes to assemble the fittings. Assemble the bolts, nuts, and lockwashers before you do the soldering. Assemble the hardware as per the diagram, and then solder with a small propane torch, gas stove burner, or large (250 W+) iron.

After you have assembled the mast, clean it again with the rubbing compound and the solvent, especially the areas discolored by soldering, and then give it several coats of clear spray lacquer or urethane varnish to protect it from corrosion.

The total cost for the pipe, hardware, and fittings was just under five dollars, well within my cost goal.

The One-Dollar Bumper Mount

Refer to Figs. 3 and 4. The trusty Barracuda had been replaced with a '75 Chevy Monza hatchback which got better gas mileage but featured an odd rubber-covered bumper that made mounting difficult. The base for the mount was made from a piece of ½" marine scrap plywood, but almost anything will do if it's sturdy —sheet metal, Masonite, etc. The brackets were sawed off of the front panel from a TD-2 microwave bay that happened to be lying in the station junk



3/8" × 24 adapters for the ½" copper mast.

box. An aluminum channel from a busted storm door or more scrap plywood would be just as effective. The insulating plastic plate is the only tricky part, as it has to be very strong mechanically. I used a piece of heavy phenolic from the fuse block in a piece of surplus equipment. A scrap of heavy Plexiglas™ or several pieces of scrap circuit board epoxied togeth-

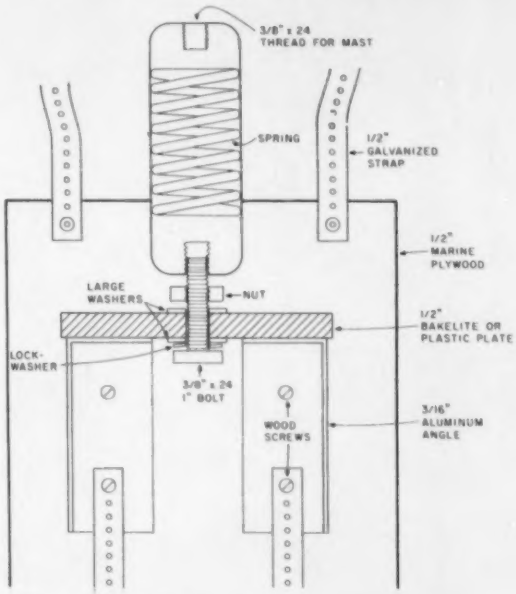
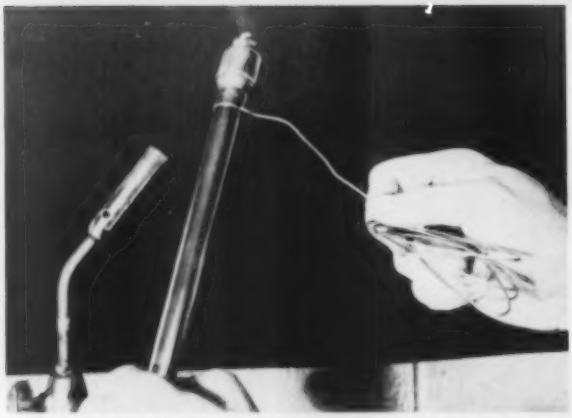


Fig. 3. $1.00 bumper mount—rear view.



Soldering the adapters onto the mast with a propane torch.

The $1.00 bumper mount attached to the Monza's rubber bumper. The coax braid must be securely grounded to the frame underneath.

er with the copper removed would work okay. If you can scrounge up an insulated 3/8" fitting like that used on commercial mounts, then the plate can be metal or wood.

The nails or wood screws that hold the bracket to the plywood base were allowed to extend through the wood for about an eighth of an inch, sticking into the rubber bumper covering and helping to secure the mount. The straps are cheap galvanized pipe hangers that are looped around the frame behind the bumper, pulled tight with pliers, and secured with screws or nails to the plywood. Use large washers on both sides of the insulating plate to ease the strain. This hole takes the full force of the entire antenna and spring. Guys of nylon string from the resonator connection on the mast back to the car will help reduce "whipping" when the car is in motion. Make them light enough to break if the antenna hits an overhead object.

Conclusion: The Hamburglar Strikes Again

The makeshift antenna worked beautifully, with very good signal reports and a good swr across the middle thirty kHz or so of the phone band in each case. Retuning the resonators was a bit touchy, but only required a few minutes with an swr bridge in the line. Results on 40 phone were particularly good. Two meter operation with a Wilson 1402 running barefoot into a home-brew magnet mount was a blast, but, with only six crystal pairs, I was out of range of repeaters more often than not, and being back on the low bands again was a real pleasure.

Arriving at the conference in Champaign, the gear was all taken inside, leaving only the mast and bumper mount on the car. Upon leaving the hotel Sunday morning, it was found that some moron had grabbed the mast and bent it back and forth until it snapped, and then cheerfully pitched the top half into a nearby snowbank.

WB9MQY, also at the conference, was very consoling. "Nyahh, nyahh," he said, "somebody stub-tuned yer copper mast for 5 meters!"

After five minutes work with a hacksaw, removing the bent ends and soldering the two pieces together with a ½" pipe coupling (17¢ at a nearby shopping center), the mast was back together. A slight retuning of the resonator, and I was back on the road!

Moral: Carry a wrench, and remove the mast and hide it inside the car, or use the Hustler quick-disconnect fittings.

Total cost for the project, including the repair, was well under the original goal of ten bucks, and with performance every bit as good as the original. The shiny copper mast looks as nice as the original, although it doesn't have the knurled chrome fittings. Best of all, it's completely compatible with original 3/8" × 24 threads which are also used in a lot of inexpensive CB mounts and hardware. ■

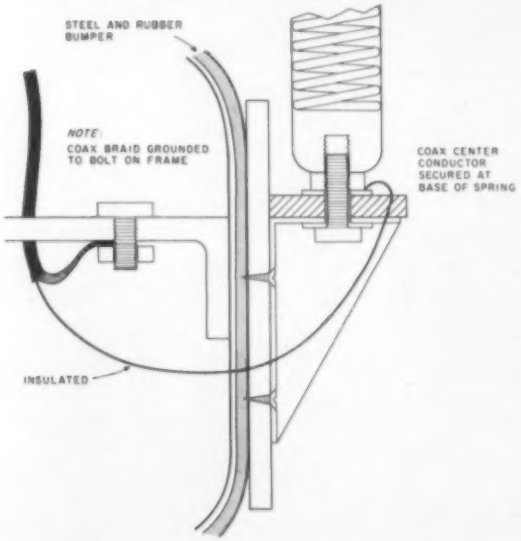

STEEL AND RUBBER BUMPER
NOTE:
COAX BRAID GROUNDED TO BOLT ON FRAME
COAX CENTER CONDUCTOR SECURED AT BASE OF SPRING
INSULATED

Fig. 4. $1.00 bumper mount—side view (straps omitted).

Parts List

two 3/8" × 24 (fine thread) bolts 3/4" long
two lockwashers
four flat washers
two matching hex nuts
*two 3/4" to ½" copper pipe reducers
two 3/4" copper pipe caps, drilled and reamed with 3/8" holes
54 to 60 inches of ½" copper pipe
cleaning compound and solder
*The 3/4" version is the same, except that the two reducers aren't needed, thereby just about making up for the greater cost of the pipe (Fig. 2).

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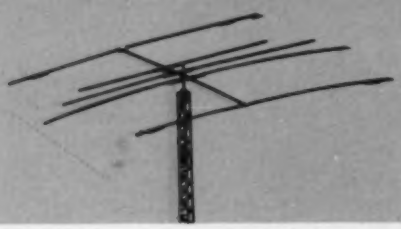

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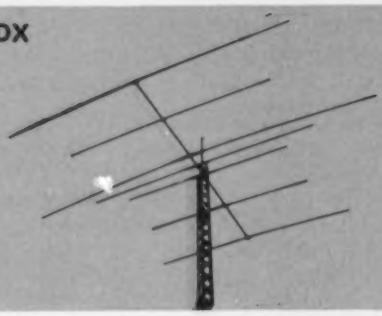

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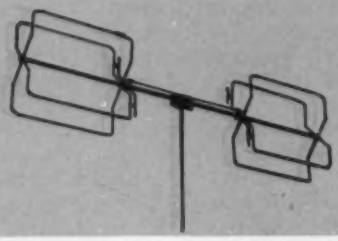

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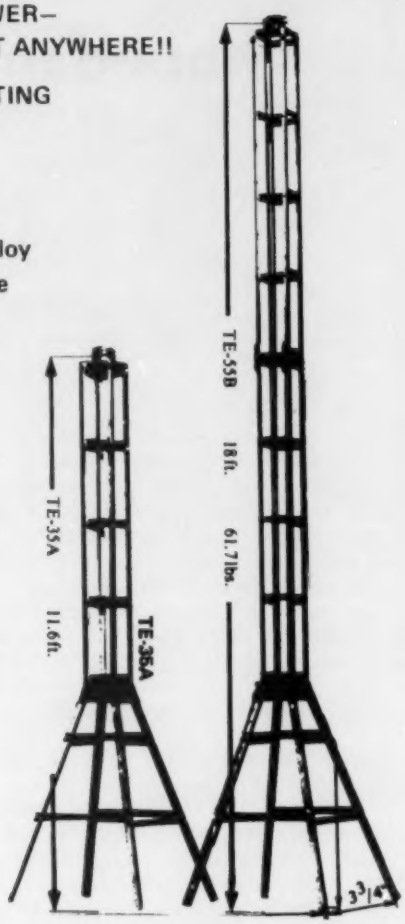

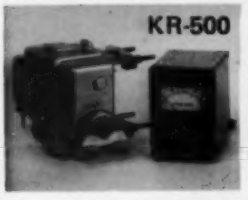

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Reader Service—see page 211

73 Magazine Staff

Impedance and Other Ogres

—another look at swr

You will now understand standing wave ratio.

The subject of understanding the effects of swr (standing wave ratio) has been explained in various articles a dozen times over in recent years. Still, many amateurs look at the "percent power reflected" markings opposite the swr values on an swr meter and are confused. For instance, next to an swr value of 3:1 there is marked "25% power reflected." The usual belief is that 25% of the total power which the transmitter is groaning to put out never makes it to the antenna to be radiated. Instead, it is rejected (reflected at the transmission line/antenna junction) and goes bouncing endlessly back and forth between the transmission line/antenna and transmission line/transmitter junctions. In other words, it is consumed or lost in the transmission line and/or plays all sorts of havoc with the transmitter output stages. This is not the case, of course, but the "percent reflected" scale of an swr meter does produce an image in one's mind that is hard to alter.

Rather than start talking about transmission lines, mismatched loads, etc., there is something much more fundamental than that which one should understand to have swr become clear. It has nothing to do with electronics and just goes back to basic ac electrical circuits. Understanding it (and not just skimming over the idea) will make the whole subject of swr and its effects in radio applications clearer.

Normally one thinks of power as just being the product of voltage times current, and indeed it is, except that one has to put a little "extra" into the formula when speaking of ac circuits. In Fig. 1, a sine wave of voltage and current is shown as it appears across a resistor. The power dissipated at any *instant* is the product of the voltage and current at that *instant*. In the example, the voltage has a peak value of 30 volts, and the current a peak value of 20 Amperes, so the peak power is 600 Watts. When both the voltage and current go into the negative half of their cycles, you have -30×-20 (at the peak negative excursion), so the peak power is still a positive number. By going back to the ac textbooks, one can confirm that by multiplying the rms values of voltage and current, the resultant obtained is average power. But, that is not important at the moment; the only important point is that one multiplies the voltage and current at any instant to get instantaneous power.

In Fig. 2, the voltage and current waves have their same peak values, but because they appear across a reactive load, not a pure resistor, the waves are displaced in time. However, the power formula still holds true at any *instant* (voltage times current). So, if the voltage and current are multiplied at every instant, the dotted peak power line shown will result. The interesting thing about this power wave is that is goes negative. So, the actual overall power

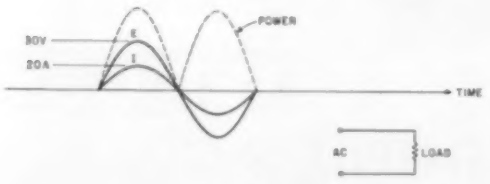

Fig. 1.

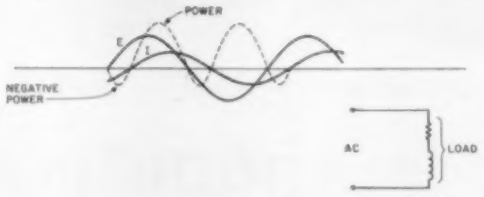

Fig. 2.

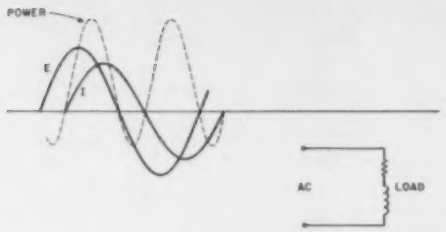

Fig. 3.

absorbed by the circuit is the net "positive" power minus the net "negative" power. This idea of negative power is where our little gremlin comes into play. The concept is that this negative or imaginary power represents power which the load will not accept. Therefore, although the source of power is able to supply power to the load as shown in Fig. 1, when the load is not purely resistive it cannot accept all of the power the source is capable of supplying. Said another way, during the portions of the voltage and current waves when the load is not purely resistive it cannot accept all of the power the source is capable of supplying. Said another way, during the portions of the voltage and current waves when *either* one of them is negative, the load is returning power to the source that it could not absorb. Where is this power in between the time it is "offered" and then "rejected"? It's in the electromagnetic or electrostatic fields associated with reactive elements—inductors or capacitors. It doesn't bounce around like a Ping-Pong™ ball between the source and the load.

To obtain the net average power a load takes, one has to take into consideration not only the voltage and current values, but also the time displacement between the voltage and current waves. In basic ac circuits, the power formula then becomes $P_{AV} = E_{RMS} \times \text{Cos } \emptyset$. Cos $\emptyset$ is, of course, what electrical power people refer to as the "power factor."

There are three simple things one can learn from the simple ac circuit before going on to the radio applications of the idea presented. Note in Fig. 1 that the resistor absorbs a certain amount of power. Remember that only resistors can absorb and dissipate power. Now, if we have the load of Fig. 2 and we want the resistor part of the load to absorb the same amount of power as the resistor in Fig. 1, we have to do something. One thing we can do, so that the net power in Fig. 2 comes out the same as the net power in Fig. 1, is raise the voltage across the load and hence the power "offered" to the load. The load will reject the same proportion of the total power as before, but if we "pump" enough power into the load, we can get the resistive element of the load on Fig. 2 to absorb the same power as the load of Fig. 1. This means increased input power and greater voltages and currents in the circuit as shown in Fig. 3.

The other approach is to "match" the load. That is, if we cancel the inductive reactance in the load of Fig. 2 by a series capacitance reactance of the same value as shown in Fig. 4, the voltage and current wave across the combined resistor/capacitor/inductor load will again become as shown in Fig. 1. Since the reactive elements cannot dissipate power, the circuit becomes the equivalent of Fig. 1, and no extra power need be pumped into the load to have the resistor dissipate the same power as in Fig. 1. This is all true, however, only at one frequency.

The loads in Figs. 1-4 are shown as being connected directly to a source of power. However, what if the load is connected to the power source over a long pair of wires, each side of which has some resistance, as shown in Fig. 5? If the load is a resistor, it doesn't take too much exercise of Ohm's Law to see that the power available from the source will be divided between the resistance of the load and the resistance of the wire pair in a manner depending on the relative value of the resistances. Let's assume that the resistance of the wire pair is a small fraction of the resistance in the load. If the load now becomes a combination of resistance and reactance *and* the power source is increased to maintain the same power in the load resistor, the power lost in the wire resistance will also increase. But, this is only because more current must flow in the entire circuit as per Fig. 3. The wire resistances will absorb *slightly* more power, but they do not absorb the rejected or reflected power because of the combined resistive/reactive load. Again, only resistances can dissipate power. So, even if the load becomes reactive, as long as the resistance in the load is large in value compared to the resistance of the wire pair, the power lost in the wire pair is not going to become significant.

When the foregoing simple circuits are "elevated" to radio frequencies, none

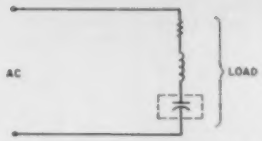

Fig. 4.

of the fundamentals described really changes. Some new elements are introduced, of course. The wire pair is now a transmission line with a characteristic called impedance, and a *time* element is introduced. That is, power cannot instantaneously go from the source (now a transmitter) to the load (the antenna). This time factor, of course, is very short, but, nonetheless, it does exist. That is why transmission lines have, besides impedance, a characteristic called velocity of propagation. So, one has to speak about power traveling along a transmission line. For instance, in Fig. 6(a) we will assume that we have a "matched" system. That is, the transmitter is designed for 50 Ohms output, the transmission line has 50 Ohms impedance, and the line is terminated in a 50-Ohm antenna. The transmitter is turned on only long enough to generate one cycle of sine wave current, which we'll call the incident, or forward, wave. Since everything is matched, the load completely accepts the power. If we leave the transmitter on continuously, we will have a continuous string of current waves traveling down the line and delivering power to the antenna. Note that although the current waves pass current down the line, when there is a continuing series of waves they will appear to stand still along the trans-

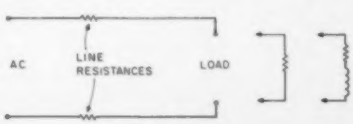

Fig. 5.

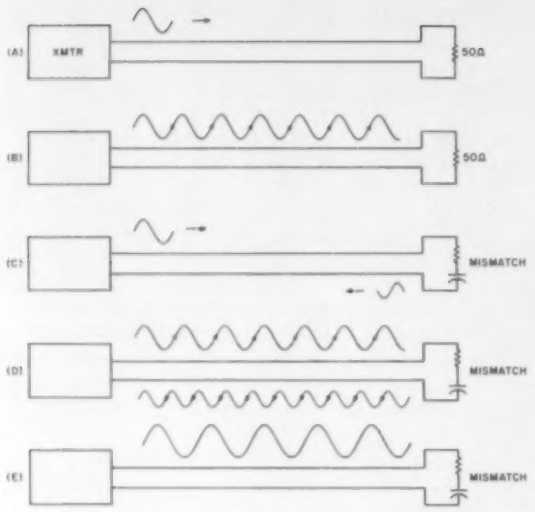

Fig. 6.

mission line.

If in Fig. 6(c) we have a mismatched load and again send a single current wave down the line, we are going to get back from the load a reflected wave. If continuous power is applied to the line, there will be continuous strings of incident and reflected waves. Since the strings are continuous, some incidental waves will always be present at any given point along the line. Therefore, at any given point and at any given instant, the resultant wave will be formed from the combination of the values of the two waves. At some points they will reinforce each other, and at some points they will subtract from each other. One probably thinks of various optical effects where two light sources interact to produce a seemingly stationary light interference pattern. Much the same thing happens on a transmission line. The result of the traveling incident and reflected wave is a resultant stationary wave. Stationary, that is, in respect to its position along the transmission line. Since the resultant stationary wave stands still, it is referred to as a "standing" wave. For example, the resultant of the wave shown in Fig. 6(d) might look something like the standing wave of current shown in Fig. 6(e).

If one can grasp this basic concept of a standing wave, the rest of the ideas surrounding standing waves, what to do about them, how to interpret swr meter readings, etc., will not be difficult. If the ideas presented so far seem a bit unclear, one might go back over them a few times. Particularly, one should understand the simple ac circuit mentioned at the start of the article and be sure that one understands what rms values mean for voltage or current values.

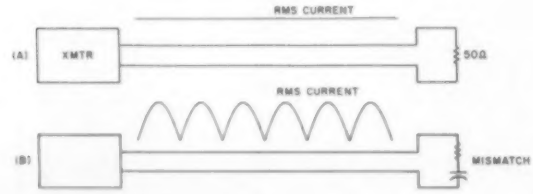

Fig. 7.

If one now feels comfortable about the basic idea of a standing wave, one can accept the information presented in Fig. 7. Instead of dealing with instantaneous values of a current wave, these figures represent the rms current, or the current that one would read along the line with a regular rf ammeter. In the case of Fig. 7(a), the current is the same at any point along the line since the system is matched throughout and there is no reflected current wave. In Fig. 7(b), where a mismatch exists, the current will be found to have different values at different points along the line. Depending on how bad the mismatch is, the current variation will be relatively small or the current variation pattern can approach the half sine wave shown. The swr on the line is defined as the ratio of the maximum current value to the minimum current value. In the case of Fig. 7(a), the ratio is 1:1 and the line is referred to as being "flat." In Fig. 7(b), if the maximum current were 3 Amperes and the minimum current 1 Ampere, the swr on the line would be 3:1.

One can actually measure the current along a line to determine swr. It is done this way in some high-power transmission lines. However, it is usually more convenient to measure voltages proportional to the value of the incident wave and to the value of the reflected wave. A directional coupler is used for this purpose, usually of the type shown in Fig. 8 (for a coaxial line). Two pickup wires are placed near the center conductor. One has a voltage inducted in proportion to the value of the incident wave, and the other a voltage proportional to the value of the reflected wave. The ratio of the two voltages is the swr, the same as the ratio of the currents previously described. As one might imagine, there is no perfect discrimination in the pick-ups between the incident and reflected waves. But, this type of instrument suffices for most needs. In a practical instrument, one usually "sets" the forward or incident voltage reading for full-scale deflection on a meter. Since the attenuation used remains in the circuit when the meter is switched to measure reflected voltage, the *ratio* of the two voltages is not upset. Therefore, the meter scale when reading reflected voltage can be calibrated in swr.

Since an swr greater than 1:1 indicates the load is taking less power than it could if it were matched, there is, as one might imagine, a mathematical relationship between swr and the percentage of power the load cannot accept. This formula is used to derive the "percent reflected power" one often sees marked along the swr scale on a meter.

How bad is it to have an swr of greater than unity on a line? What can one do about it? Part of the answer to the first question can be answered by going back to the simple ac circuit, and part of that answer requires a more careful look at the effects of a transmission line at radio frequencies. If the load is not matched to the line, maximum power will not be transferred to its resistive component, as in the case of the simple ac circuit. We can try to get more power out of the source (transmitter). This, of course, means loading the transmitter more heavily, with consequent heat dissipation problems, etc. But, it can be done if the transmitter can take it and if one is willing to waste input power. So, if the swr meter reads 3:1 (25% reflected power), it means that the

load could accept 25% more power if the system were matched. One could make up, approximately, for the swr by putting 25% more power into the system.

When dealing with a real transmission line, there are also a few other factors to be kept in mind, although their significance is usually a bit overstated for the normal HF installation. Any transmission line has an inherent loss due to its ohmic losses, and also rf losses, because of the dielectric material between the conductors. For instance, RG-58 coax might have a loss of about 1.2 dB for a 100-foot run on 20 meters. So, this means that even if the transmission line system were perfectly matched, a 100-Watt output from the transmitter would end up as about 78 Watts at the antenna. There is nothing that one can do about this except use a cable with a lower inherent loss at the frequency—such as RG-8. If the RG-58 line were now not "flat" but had an swr of 3:1, there would be some additional loss in this line. This is only because the reflected current wave travels along the line as well as the incident current wave. So, one suffers line losses coming and going. These losses can be obtained from a number of graphs in antenna manuals, but they are not as surprising as one might imagine. For instance, in the example given, the swr of 3:1 causes the *total* line loss to increase only to about 1.6 dB. Therefore, if we can still get 100 Watts into the line, the total loss would rise to about 31 Watts instead of the 22 Watts lost under matched conditions. Consequently, the swr has not caused any tremendous increase in the power lost in the transmission line. We are not burning up the transmission line because of the swr, but neither are we getting the available power where we would like to get it dissipated—in the antenna load. But, under some circumstances, one might accept the situation since even if a total of half the transmitter output power were not utilized due to a combination of line losses and inability of the load to accept a portion of the power, the radiated signal would only be 3 dB, or about one half an "S"-unit down. With a view toward doing something to overcome the effects of swr on a line, getting the power into the load may or may not involve doing anything about the swr. The cause of the swr on the line is the mismatch between the load and transmission line impedances. For instance, in Fig. 9(a) we have a 50-Ohm load and a 50-Ohm transmission line. No matter how long the line is, a transmitter is going to see 50 Ohms at the transmitter end of the line. In Fig.9(b), we have a complex load on the transmission line. At the junction of the line and the load there will be a mismatch. One cure for this problem is to do something at this juncture—insert an impedance matching device. This would eliminate the swr on the line, and the line would be "flat," with no more than its inherent losses.

This is usually the preferred solution, but not always a practical one. So, in lieu of this, we can tackle things from the transmitter output terminals. At this end of the transmission line there are two things we can do. One is to experiment with the length of the transmission line. A transmission line when it is not terminated in its characteristic impedance will present a complex impedance at its feed terminals. Depending on the frequency and

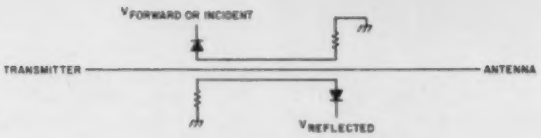

Fig. 8.

length of the line, this complex impedance can be capacitive or inductive. So, by experimenting with the line or by doing some calculations, we can find a line length where a situation similar to Fig. 4 exists. The transmission line/load considered as a *whole* is matched. The only price we pay is the bit of increased loss on the line due to the swr. Of course, this sort of solution is only practical on one frequency. As the frequency changes, the antenna load impedance changes, the electrical length of the transmission line changes, etc. Therefore, the more common solution is to insert a tuning device at the transmitter end of the transmission line. The tuning device can handle the various complex impedances found at the end of the line on various frequencies and match the transmission line/load considered as a *whole*. It presents a constant 50-Ohm impedance to the transmitter output when properly adjusted. We haven't cured the cause of the swr, because the basic mismatch at the antenna terminals still exists. But, we will be able to get more power into the antenna and pay only a small price in terms of increased line loss due to the swr.

The foregoing was concerned with swr, its effects, and what may be done about it. But, to really "close the loop," we might consider if we are really getting anyplace by matching. That is, say we have the setup of Fig. 9(c). Our "super" tuning device is effective enough so that with the same antenna and transmission line on 80 through 10 meters, it presents a 50-Ohm impedance to the transmitter. The transmitter loads easily to produce a 100-Watt output, and an swr meter between the transmitter and tuner reads 1:1. The answer to whether we are getting anyplace depends upon whether we are trying to do something reasonable or not. Remember, in the discussion of the simple ac circuit it was mentioned that only resistances can dissipate power. So, if the resistance part of the antenna load is significantly higher than the rest of the resistive losses in the system (transmission line and tuner), we may be getting someplace. Most of the power will be dissipated in the higher value resistance. The resistance part of the antenna impedance is

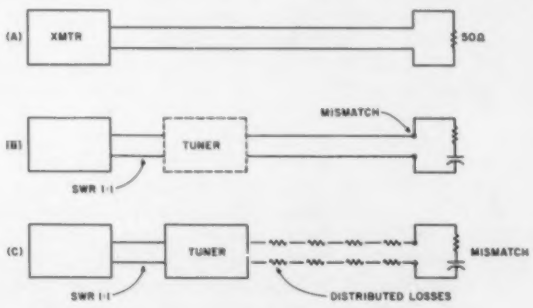

Fig. 9.

referred to as radiation resistance and can be found in antenna manuals for the usual types of antennas. For a ½λ dipole antenna, it might be on the order of 60 Ohms. So if the resistance losses in our matching system are just a few Ohms, essentially all of the power will be dissipated in the radiation resistance. Now, if we take that 10 meter ½λ dipole and try to operate it on 80 or 160 meters, the radiation resistance falls to around one Ohm or less. So, guess where all the power is going even though everything loads fine and the swr meter reading looks great? The use of tuning devices certainly has advantages in many applications. It provides more uniform loading to the transmitter across a band where the actual transmission line/antenna junction swr is changing. They also allow many amateurs to operate on bands they do not have proper antennas for by at least getting some power into the antenna for radiation. But, you can't beat the basics of power distribution in simple ac circuits, even when operating at rf!

This article has not tried to deal with every nuance of the swr question. Math has been completely avoided and a number of propositions have simply been presented without discussion, although they can be verified from antenna manuals. I feel, though, that if you try to relate the transfer of power in an rf application back, within reason, to the transfer of power in simple ac circuits, you will be able to feel more comfortable and understand more when looking at that swr meter. ■

The Active Filter Cookbook

—review of Lancaster's treatise

Canadian confirms composition's class.

Michael Black VE2BVW
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In the September, 1977, issue of *73*, there was an interesting article by Peter Stark using active filters. I was glad to see this because I feel that active filters have been rather neglected. *The Active Filter Cookbook* by Don Lancaster (Howard W. Sams & Co., 240 pp., $14.95) would seem to be the next step if you liked Peter's article and want to know more.

Although not a wide variety of filters are covered in this book, everything that you need to know is here. The sort of stuff which is missing is about the more exotic types, and most people would not have any use for them. Don starts the book off with some filter basics and some definitions of filter terms. He talks about active filter advantages and disadvantages and continues with a description of the rest of the book.

In chapter two, information on op amps, which form the backbone of active filters, is given. Described are integrators, summing blocks, and basic amplifiers. Also, there are some guidelines for selecting which device is useful for your application. Finally, basic information on some of the more widely used op amps is provided.

The next six chapters give theory on how the filters work, selecting which configuration (Bessel, Butterworth, or Chebyshev) to use, and what makes up each of these three types. Information on component tolerance is given here also. Don goes on further to discuss scaling, which is an easy way of taking the normalized filters given in this book from their regular frequency of 1 kHz and placing them at the frequency which you desire.

Chapter 9 is miscellany. It gives information on selecting resistors and capacitors. It talks about manual wide-range tuning along with some thoughts on voltage control. This chapter ends with the description of elliptical filters, which are somewhat unusual.

The tenth and final chapter, like all of Don's other cookbooks, goes into some applications for active filters, such as tone decoding, modems, quadrature art, and color organs. Finally, he hints at some uses which the reader can pursue himself.

Throughout this book, math is kept simple and is used sparingly. Instead, emphasis is placed on graphs and tables, which help the reader to better visualize what is going on. Examples of selecting a filter and putting it to use are given throughout the text. There are numerous pages on active filter theory, complete with math, but this is separate from the main text and can be completely ignored by those not interested.

While some may scoff at the idea of paying so much for a book on audio filters, I would recommend this book to those who have a lot of filtering needs. At audio frequencies, active filters are far better than coil and capacitor combinations and this book will open the door to their use. ■

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Reader Service—see page 211

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After fighting the temperature drift problem with a 555-based audio frequency shift keyer, I decided to try crystal control. The design had three basic requirements: high performance, economy, and digital circuitry.

Making a few quick calculations, I found that I could obtain a 2125 Hz tone from an 8500 kHz military surplus crystal I had on hand by dividing by 4000. Likewise, the 2295 Hz tone would require a 9180 kHz crystal. Frequency tolerance is not critical in this application because a Hertz or two off in frequency is barely noticeable (I wish some of the guys could get within 10 or so), and the crystal would have to be off 8 kHz in order for the tone to be off by 2 Hertz.

The 8500 kHz crystal I used is a small type in an HC18-type holder, which is about 1/8 by 1/2 by 5/8 inches. The 9180 kHz crystal is in an FT-243-type holder and was originally at 8970 kHz. Fortunately, this type of holder is easily opened, and, also, the crystal can be etched rather easily.[1]

Circuit Details

The circuit uses eight inexpensive ICs, all of which can be purchased from several sources for less than four dollars. Each oscillator is free running. The oscillator circuit is the simplest one available,[2] but works well for crystals in the range from about 2 to 15 MHz of almost any type. Some higher frequency crystals of the overtone type will oscillate at the fundamental frequency with this circuit.

The output of each oscillator is fed into separate divide-by-ten counters (SN7490) to ensure isolation. Referring to Fig. 1, the output of each divider, now 850 and 918 kHz, respectively, is fed into a NAND gate, U7A-U7D (SN7400). The four gates in this chip are wired so that only one of the frequencies is passed at a time, depending upon whether the switching input is low or high. The signal is taken from the last section of the 7400 and divided by 10 twice more with U3 and U4 and then divided by 2 twice by U8, the SN7473 dual flip-flop. This results in a total division by 4000, which yields square waves of 2125 and 2295 Hz. The signal must consequently be passed through a low-pass filter in order to change it to a sine wave. I used a circuit similar to that in the AK-1[3] for the filter. Active low-pass filters could be designed for this job, but the main advantage to them is space savings, since no amplification is needed. The passive filter won out in my case for simplicity and eliminated the need for another power supply connection on the board. Some adjustment in the divider network may be necessary to suit individual transmitter requirements. Finally, this sine wave is fed into the microphone input of an SSB transmitter.

The keying circuit shown is designed to operate from the series loop in the printer and keyboard. The keying input is taken from the top of the emitter resistor of the loop switching transistor (27-Ohm resistor in my TU). If plus 5 volts is used for the switching input, resistor Rs should be increased to 15k Ohms. If separate keyboard and printer circuits are used, the input should be modified accordingly. If it's more convenient to have the mark condition low instead of high, the two crystals could be switched or another transistor configuration could

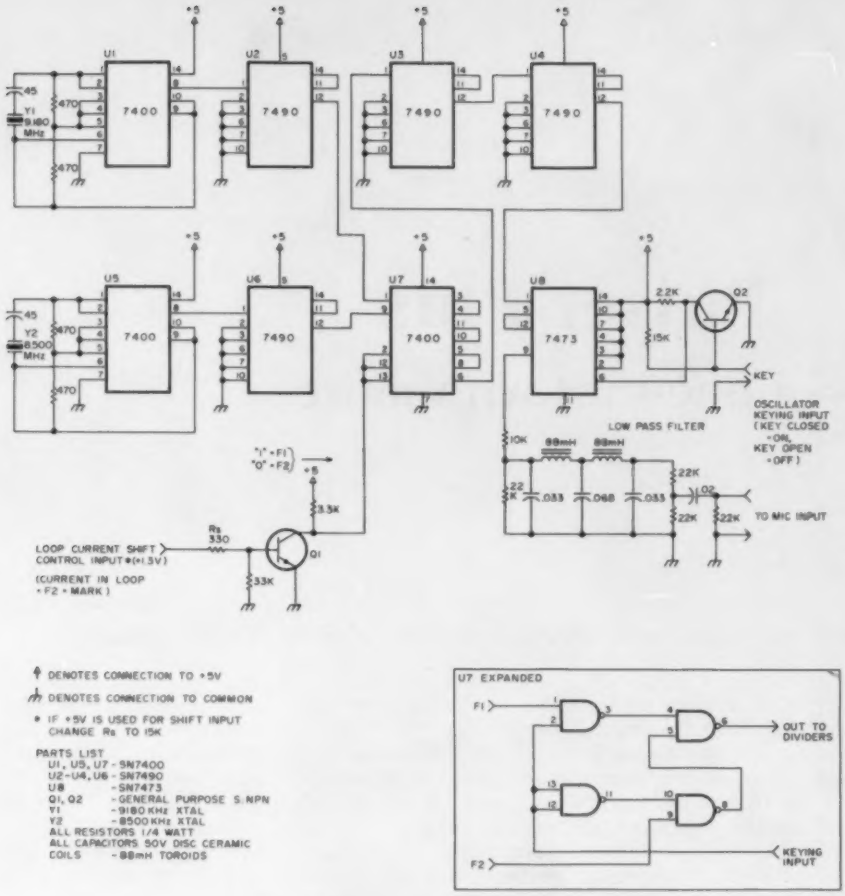

Fig. 1. TTL crystal AFSK oscillator.

be used (see Fig. 2). For CW ID, on-off keying is used instead of narrow shift. The key thus also acts as a transmit-receive switch when using VOX with the transmitter.

Construction Details

The complete circuit, except for the power supply and the 88 mH toroids, is on a 2- by 4-inch circuit board using the layout shown in Fig. 3. Bypassing of all plus 5-volt leads with a .1 uF capacitor is recommended. Leads should be kept as short as possible, and all leads which leave the chassis should be bypassed to ground to prevent rf from activating the switching chip. Good filtering of the power supply is necessary for a clean output from the transmitter. The circuit draws about 180 mA.

Conclusion

While not having the advantages of a single crystal synthesized unit, this one does have rock-solid stability, is relatively inexpensive, and is readily compatible with computer or TTL circuits. Several QSOs were made using this unit, and only favorable comments have been received.

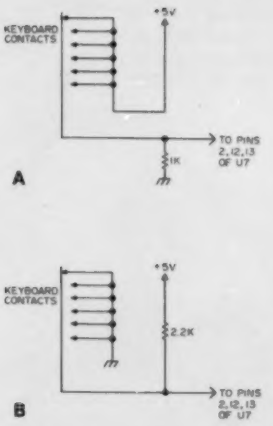

Fig. 2.(a) Separate keyboard normally high; (b) separate keyboard normally low (requires reversing crystals).

Acknowledgements

I wish to express thanks to all the authors mentioned in the references and many others from whom I got ideas and circuit information before deciding to design and build this circuit. Also, I am grateful for much assistance from Jimmie Straughn K4COV who did the layout and helped with making the board.

I will be glad to answer any questions of design, availability, performance, etc., if inquiries are accompanied by an SASE. ■

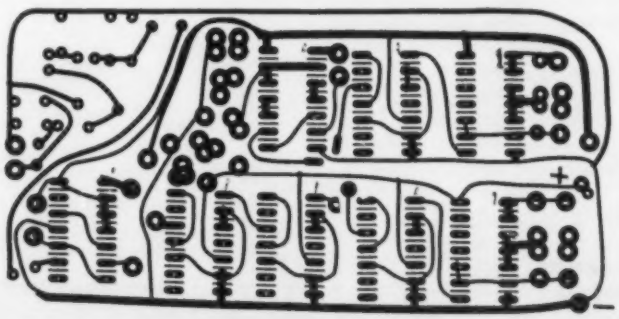

Fig. 3. PC board layout, foil side.

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1. Newland, "A Safe Method for Etching Crystals," *Single Sideband for the Radio Amateur*, ARRL.
2. "A TTL Crystal Oscillator," *QST*, Feb., 1974, p. 34.
3. "Audio Frequency-Shift Keying for RTTY," *Specialized Communications Techniques for the Radio Amateur*, ARRL.

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Montreal, Quebec
Canada H3Y 2E7

Pulser Plus

— a one-shot with more

This circuitry turns your single-shot multivibrator into a useful piece of test equipment.

This gadget is a combination of circuits from two previous articles. The first, in the October, 1974, issue of *73*,[1] described a wide-range repeating pulse generator using three 555s. The second article was in *73* for February, 1975,[2] and described a variable pulse width, single-shot generator using TTL devices. Both of these circuits were interesting and I hope that the circuit discussed here has kept all the good features of both.

The circuit of the pulser is shown in Fig. 1. Here, again, the circuit consists mainly of three 555s. Every time S1 is pressed, there is a pulse at the output, the length of which is variable over a wide range. Both positive- and negative-going pulses are available. The unit operates over a supply voltage range of 4.5 to 16 volts, which makes it usable with both TTL and CMOS, and even linear circuitry under certain conditions.

Here's how it works: U1 is connected as an RS flip-flop. I have not seen much on using the 555 in this way, but it is just right for our application. As long as pin 2 is low, the output is high. When S1 is pressed, pin 2 goes high, pin 4 goes low, and the output (pin 3) goes low. Since a 555 is negative-edge triggered, U2 will be triggered when pin 3 of U1 goes low. As U2 is connected as a single-shot multivibrator, there will be a pulse on pin 3 for a length of time determined by the equation $T = 1.1(R1 + R2)C1$. A positive-going pulse is available from pin 3 of U2. U3, connected as an inverter, provides a negative-going pulse. Note that the output pulse is somewhat less than the supply voltage and the pulse height varies directly with this voltage.

An interesting addition to this circuit is also shown in Fig. 1. This is nothing more than a diode bridge, but, when hooked up as shown, it allows you to get power from the circuit that you are testing without worrying about connecting the polarity wrong. This trick is not new, but it is a great addition to simple pieces of test equipment like this pulser and logic probes.

This circuit can easily be built using a minibox as an enclosure. Have R1, S2, and S1 mounted on the front. Put J1 in the back. Perhaps a rough calibration of R1 would be useful. In some applications, both output polarities may be required, in which case S2, the polarity selector, could be eliminated, and two output jacks used. Be sure to locate S1 so that it can be used without hitting any of the other controls.

This unit can be used anywhere that a variable width, single-pulse multivibrator is needed. While it is not very different from the average one-shot, the little extras make it a valuable addition to your lab.■

References

1. Christer Falkenstrom SM4DZR, "A Simple Pulse Generator Using the Signetics 555 Timer," *73 Magazine*, October, 1974, p. 141.
2. Hank Olson W6GXN, "Further Adventures of the Bounceless Switch," *73 Magazine*, February, 1975, p. 111.

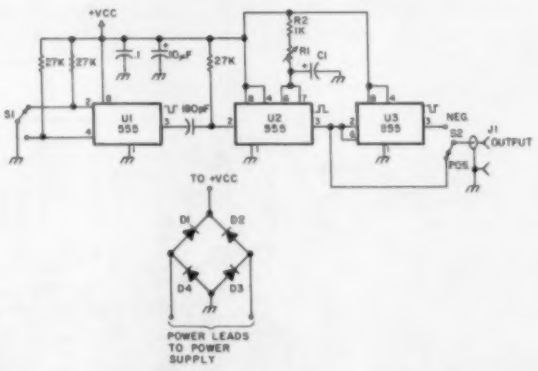

Fig. 1. Versatile single-shot schematic diagram. S1 = SPDT momentary contact. S2 = SPDT toggle switch. D1-D4 = 1N914 silicon diodes. J1 = phone jack or similar.

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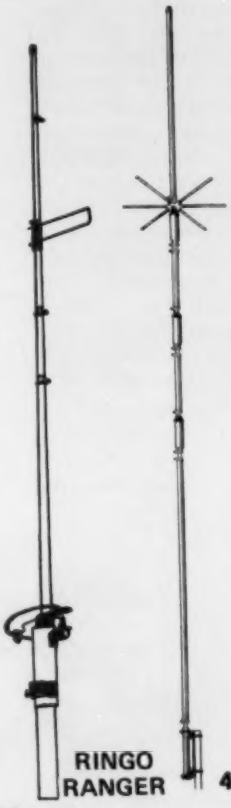

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L'Eggs are the legs.

Several *73 Magazine* articles on anemometers and weather indicating devices by W2AOO[1,2] and W9CGI[3] caught my interest and led to the construction of the anemometer shown in Photo A. I have been casually interested in wind speed and direction, particularly when going fishing or sailing or attempting to outguess the weatherman.

Several early construction attempts were unsuccessful due to the lack of a readily available, low-cost pivot point, and a method of trapping the wind (cutting Ping-Pong™ balls in half just didn't work).

After stacking a three-element 15 meter beam and a three-element 20 meter beam, I became even more interested in wind direction and wind speed. The wind surface area and resultant torque vary considerably depending on whether the wind blows against the elements broadside or against the boom length (element tips facing the observer). In my instance, the antenna surface area is approximately 9.5 square feet when viewed broadside and less than 5 square feet when facing the boom lengths. When you consider the combined antenna torque and wind loading on the antenna and tower, the resultant load on the rotor and tower is considerable.

Pointing the antenna boom lengths into the wind significantly reduces the wind loading and lengthens rotor life. If high winds should develop, an indicating device in a high-traffic area such as the kitchen would indicate wind speed and gusts. A wind vane mounted on the tower would serve to indicate the wind direction.

The major items required to construct the anemometer are a bicycle front axle, three L'Eggs™ stocking containers, a slot-car motor or other permanent magnet dc motor (which will serve as a dc generator), a 0-50 microampere meter, a pipe or length of tubing, and the top from a spray paint can (Photo B).

The problem of finding a low resistance pivot point was solved by cutting in half the front axle of a discarded bicycle and using it as the pivot point. Most bicycle axles may have to be annealed before drilling a hole to accept the motor shaft. This shaft can be held in place with epoxy glue or setscrews (Photo C). I used setscrews to secure the motor shaft to the axle so that the motor could easily be changed, although this hasn't been necessary during two years of operation. Be sure the slot-car motor readily drives the 0-50 microampere meter when spun by hand.

A piece of tubing or pipe is selected so that the lip of the bicycle axle rests on the outside diameter of the tubing as shown in Photo D. An aluminum retainer bracket secures the axle to the tubing, and a piece of Romex insulation taped around the dc generator will prevent it from rotating inside the tubing.

In Photo E, three 1/8-inch diameter aluminum rods are cut into 7¼-inch lengths and threaded. The L'Eggs stocking containers are secured with nuts. Each rod is then threaded into a 1¼-inch diameter by ¼-inch thick aluminum disk. The threaded holes are spaced 120 degrees apart. The center of the disk should be drilled so that it will pass through the bicycle axle.

Locate a plastic aerosol spray can top which will be used as a rain shield. Cut, or burn out with a soldering iron, the internal

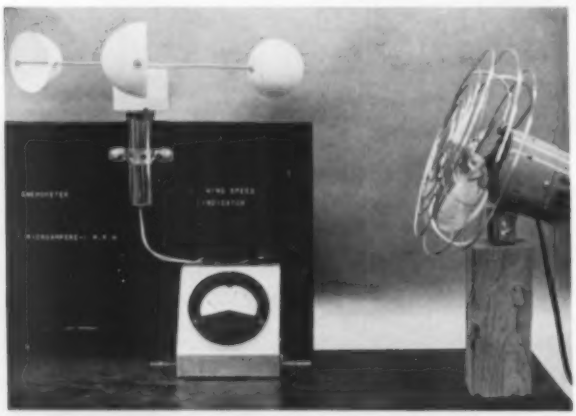

Photo A. Complete anemometer system.

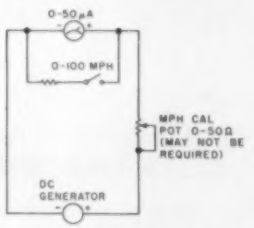

Fig. 1. Anemometer schematic.

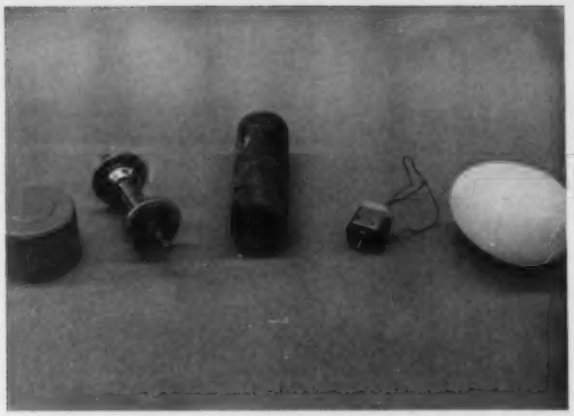

Photo B. Component parts of anemometer.

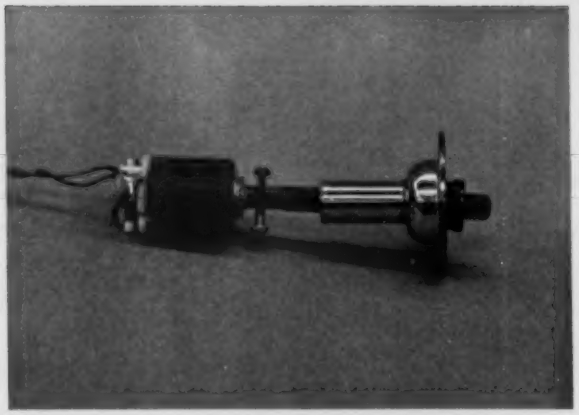

Photo C. Slot-car motor attached to bicycle axle by means of two setscrews.

plastic wall which is used to lock the cap on the can. A hole should be drilled in the center of the cap so that it will fit over the axle. The unit is assembled by placing the cap over the bicycle bearing nut, followed by the cup assembly (which is secured with the remaining axle nut). (Photo E.) A wooden plug may be inserted in the other end where the two wires come through.

It just so happened that three of the constructed anemometers indicated approximately one microampere per mph on the 0-50 microampere meter readout device. Depending on various motor/dc generator outputs, a small value of variable resistance (0-50 Ohms) may have to be inserted in series to calibrate the mph reading. A switchable shunt resistor should be installed across the meter movement. This will enable the meter to read 0-50 mph or 0-100 mph full scale. Refer to Fig. 1.

The internal resistance of the meter and the shunt value can easily be determined by using the formula or circuits found in the *ARRL Handbook*. In most cases, the shunt value will be the same as the meter's internal resistance. A typical shunt value would be 5 Ohms. I used common carbon resistors since extreme accuracy was not as important as the relative readings.

Frequent monitoring of a NOAA weather station indicated that the observed meter measurements were very close to local mph readings. Since I was only concerned with relative readings, no actual calibrating resistance was required.

If you are a purist, the easiest way to calibrate the anemometer is to compare the readings with an anemometer of known accuracy. An alternate method would be to mount the anemometer on the front of a car and adjust the calibration pot. An open field or vacant parking lot should be selected and all safety precautions and speed limits observed. A 10 mph reading should be sufficient for adequate calibration. The air-foiling effect of the car chassis will affect the readings if it is held outside a window. Also, be sure the wind is not blowing.

One word of caution: Provide some means of disconnecting and grounding the lead-in wire from the anemometer to prevent damage from lightning.

Mount the anemometer in a clear, unobstructed area and pay attention to Mother Nature! ■

References

1. "Digital Wind Direction Indicator," Warren MacDowell W2AOO, *73 Magazine*, November, 1974, pg. 40.
2. "Inherit the Wind," Warren MacDowell W2AOO, *73 Magazine*, March, 1976, pg. 72.
3. "The Wind Counter," Dave Brown W9CGI, *73 Magazine*, November, 1976, pg. 84.

Photo D. Bicycle axle held in tubing by use of aluminum retainer.

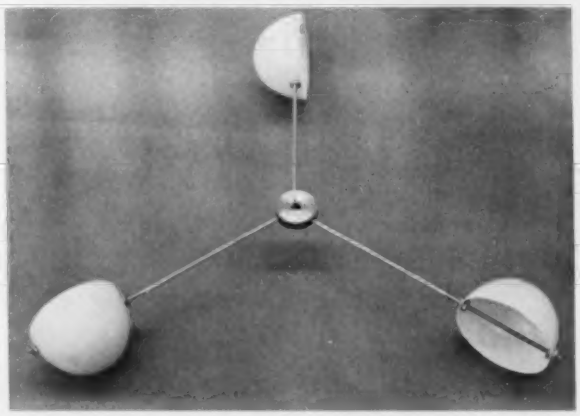

Photo E. Completed wind-catching assembly.

A Self-Contained, Fully-Automated, Transistorized Fuse Tester

—amaze your friends

Take a look at the English answer to the battery and bulb.

C.F.J. Ward G3TAI
50 Lakeside
Bracknell, Berkshire
England RG12 2LE

Here is a simple fuse tester for the shack which is quick and easy to build and use. Although it is only one step better than a battery and bulb, it does have an advantage in that it will test those low-current fuses that appear here and there. (And it is bound to impress your nontechnical friends!)

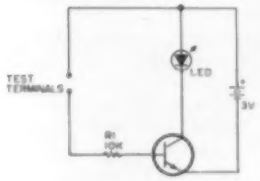

Fig. 1.

The circuit is shown in Fig. 1, and operation is as follows:

1. With no fuse connected, there is no base current and, hence, no collector current; the LED remains dark. Use of a silicon transistor ensures that the leakage current is negligible.

2. When a short circuit (good fuse) is placed across the test terminals, it completes the base drive line, and base current will flow. The resulting collector current will light the LED.

The base current will have a value of approximately 0.24 mA since the supply is 3 volts. The base-emitter drop is about 0.6 volts, and the base drive resistor is 10k Ohms. This will cause a collector current of HFE times 0.24 mA to flow, and, for a typical HFE spread of 50 to 150, this will be 12 to 36 mA, which will easily light the LED. With my unit, I used a low-gain transistor salvaged from a surplus computer board which gives a collector current of 16 mA. With a high-gain transistor, the collector current can be adjusted by increasing the value of the base drive resistor, but it is much better to use a low-gain transistor because leakage current through the fingers when using the tester can cause the LED to light even if the fuse is blown! This effect is much worse with high-gain transistors.

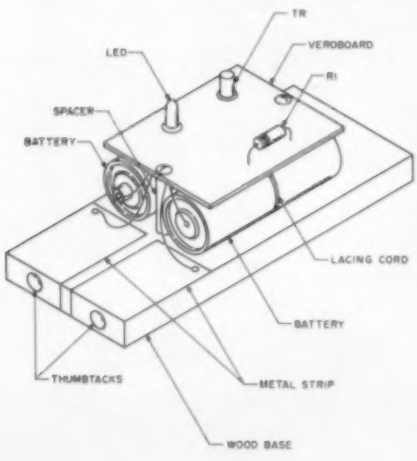

Fig. 2.

Construction

The tester can be made up as shown in Fig. 2. The components are mounted on a small piece of Veroboard. This is fixed to the wooden base plate with screws and spacers made from ball-point pen cases cut into ¼-inch-long tubes. The two AA-size batteries are tied together with lacing cord, which holds them against the spacers. The test terminals are made from some brass strip that I had in the junk box, but bits cut from an old can would do as well. The batteries are soldered into the circuit since no current flows unless a good fuse is tested. They should last a long time with the intermittent use expected of a fuse tester.

I have drilled a hole in the base of my tester so that it can be hung up when not in use. ■

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Reader Service—see page 211

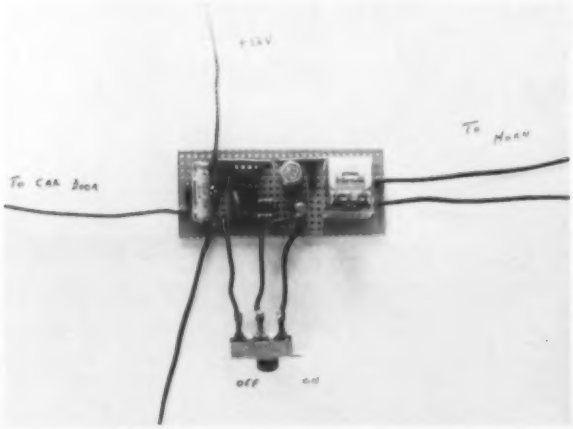
Don't Get Burgled!

—build this simple alarm

Isn't security worth $10 or less?

William R. Fletcher, Jr.
2810 Riverview Drive
Fairbanks AK 99701

Here is a simple burglar alarm that makes an excellent one-evening project and can result in a safe car or shack. It is based on the fact that some thieves will not stop for anything except a good reliable alarm such as this one. There are no critical parts to find or adjustments to make with this alarm as with others I've seen (Jeffrey Pawlan WA6KBL, "The Smart Alarm," *73 Magazine*, June, 1975). The circuit allows safe exit and entry using a minimum of components. Most ham operators with a small junk box could probably build it for almost nothing. Even if you had to buy all the parts new, it should cost less than $10. Shopping in the back of *73 Magazine* could put it closer to $5. Not much for such a reliable source of protection.



Operational Description

All you have to do is park your car, open the door, set the alarm, and exit. Unlike other alarms I have read about, there is no minimum exit time on this one. For example, you can take as long as you want to unload groceries, kids, etc. This alarm is only activated and starts timing out the next time your door is opened, such as when you return or when a thief decides your car is next. You then have ten seconds to switch off the alarm. Once switched off, it will not sound the car horn.

Circuit Description

The circuit is inexpensive, reliable, and very easy to build. For active com-

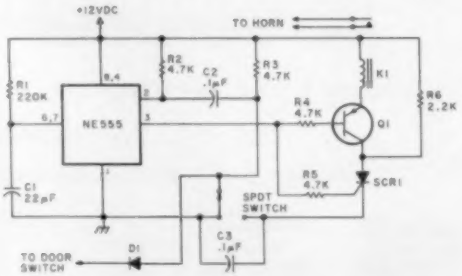


Fig. 1. Burglar alarm schematic diagram.

ponents, it uses a very common integrated circuit (NE555), one PNP transistor, and one SCR. See Fig. 1.

The timer circuit is designed to have 12 V dc applied at all times. If the circuit used a power switch, it would cause false triggering of the timer, and this would cause the horn to sound after time-out. It does, however, use a switch in the relay circuit. With the switch in the off position, it holds the input to pin 2 at ground, which also prevents false triggering of the timer. With the switch in the on position, it puts ground to the relay circuit so it can be switched in or out, to shut off the alarm, and removes the ground from the trigger input (pin 2). When pin 2 goes high (12 V dc), this arms the alarm.

When you open the door, the switch is in the off position and ground is applied to the trigger input (pin 2). If the door opens, the door switch puts ground on the trigger input wire. Now you can switch to the on position. This arms the circuit and the trigger input still sees ground (via the door switch). You can now close the door and lock it if you wish. This puts pin 2 at 12 V dc. The next time the door is opened, pin 2 receives a negative-going pulse which starts the time-out. When pin 2 goes low, pin 3 (output) goes high (12 V dc) and turns on the SCR. After the circuit times out, pin 3 drops back low again, which turns on Q1, and K1 energizes which sounds the alarm. Relay K1 can be connected to a horn, bell, lights, or any combination thereof. The alarm will continue to sound until you shut off the switch and, by then, the would-be thief should be long gone.

If for any reason you need to alter the entry time, it is easily accomplished by changing R1 or C1. Increasing either will lengthen entry time and decreasing either will decrease entry time. With the components shown, entry time is about 10 seconds. I find this to be just about right to comfortably enter and shut the alarm off.

If this alarm is to be used for shack protection, you must build an additional input circuit which is nothing more than a switch and resistor combination (Fig. 2). Also, if house current is preferred over a battery, Fig. 3 shows a power supply circuit that will work.

This alarm has already proven itself once for me! Since that one attempt on my car by a thief, I consider it to have paid for itself. If you value your possessions as I do, this alarm will give you peace of mind while away from your car or shack. ■

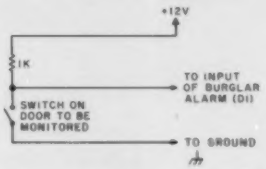


Fig. 2. Input circuit switch schematic diagram.

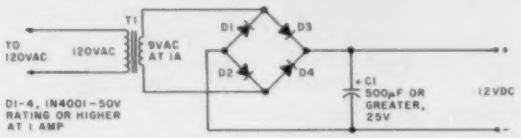


Fig. 3. Power supply schematic for burglar alarm.

Power x 2

—dual auto batteries

Your car will always start, and you can operate all you like.

Harry J. Miller
991 42nd Street
Sarasota FL 33580

If you'd like to install a second battery in your car to operate your radio, CB unit, ham setup, etc., and not worry about having enough current to operate your starter, use the device shown in Fig. 1.

Your car's alternator will charge both batteries, but operating your radio gear too long will only discharge one, leaving the regular vehicle battery fully charged for instant use.

D1 through D4 are stud-mounted silicon diodes rated at 60 piv and 25 Amps or more. Mount with the usual insulating washers on a heat sink. ■

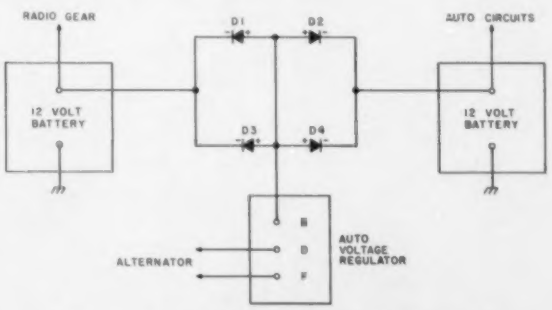


Fig. 1. Battery isolator schematic diagram.

George R. Allen W2FPP
161 Rosedale Dr.
Binghamton NY 13905

Experimenting with Tones

— fun with functions

Tone generation the foolproof way.

Tone generators, or audio oscillators as they are commonly called, are frequently used in amateur and commercial radio systems. They are used in touchtone™ pads, toneburst generators, subaudible generators, AFSK oscillators, and in remote station control systems. They have also been widely used for years in test generators for testing AM, SSB, and telephone equipment. While there are many ways to generate tones for these and other uses, most of the traditional methods have drawbacks of one sort or another. LC circuit oscillators, for example, are difficult to tune up, twin-T oscillators sometimes are reluctant to oscillate, and multivibrators aren't always as stable as required. The above problems are compounded when attempting to adapt these oscillators to frequency shift keying. While these drawbacks aren't too serious to an experienced experimenter or engineer, they sometimes prove to be major frustrations and obstacles to the average experimenter who needs a good audio oscillator quickly.

An easy and almost foolproof way to generate audio tones for a large variety of purposes is to use one of the IC function generators, readily available from most electronic supply houses. These function generators and a minimum number of external components will provide stable, low-distortion sine wave audio outputs. This article describes the operation and application of these IC function generators, and gives simple examples and circuits using an EXAR XR2206 function generator IC. The experiments require no test equipment other than a pair of earphones and a VOM. The total cost of these experiments should be under $10, provided that a source of 12V dc is available.

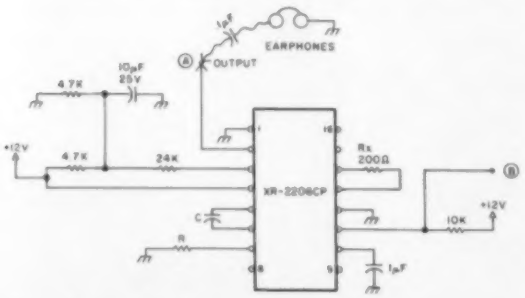


Fig. 1. Basic audio oscillator. All resistors are 1/4- or 1/8-Watt. For a frequency of 1 kHz, C = .1 uF, R = 10k.

The EXAR XR2206 IC Function Generator

Fig. 1 shows a basic audio oscillator using an XR2206 IC. None of the components is critical, and the circuit should work the first time it is turned on. R and C are the frequency determining components. With the values given for R and C, the function generator will produce an audio output of 1 kHz. Connect the earphones to point A through a .1-uF capacitor as shown. A clean sine wave of about 1 kHz will be heard. The output impedance is 600 Ohms, and the IC will drive earphones of 600 Ohms or higher impedance. It will not drive a 4- or 8-Ohm speaker. The rms audio output is about 1-2 V, which is more than enough for most purposes. For ease of construction, the circuit may be breadboarded on a Continental Specialties or similar breadboard.

With the earphones still connected to point A, remove Rx from the circuit. The output should become slightly richer in harmonics as the sine wave is changed to a triangle wave. If an oscilloscope is available, the waveforms should appear as shown in Fig. 2.

Connect the earphones to point B, the square wave output, through a .1-uF capacitor. A 1-kHz tone, rich in harmonics (square waves), should be heard. If an oscilloscope is available, the waveform should appear as shown in Fig. 3.

The output frequency of the function generator is determined by R and C, by the expression:

$$f = 1/RC.$$

Thus, in this case,

$$f = 1/[(1\times10^{4})(1\times10^{-7})] = 1/10^{-3} = 10^{3}/1 = 1000 \text{ Hz}$$

Component tolerances are an important consideration if a precise frequency is desired. With average, run-of-the-mill

capacitors and resistors (20% tolerances), you can get near the desired frequency, but you won't get exactly on frequency. If a precise frequency is desired, then a trimming resistor should be inserted in the circuit as shown in Fig. 4.

Temperature Stability

The temperature stability of the XR2206 is about 15 parts per million per degree centigrade, or about .15% over the temperature range of 0 to 75 degrees C. This is very good temperature stability and probably better than needed for most purposes. Unfortunately, in practice, it is difficult to achieve this stability due to temperature tolerances of R and C, the frequency determining components. In the circuit given in Fig. 1, it is assumed that normal run-of-the-mill carbon composition resistors and disk ceramic capacitors will be used. Components of this variety exhibit very poor temperature stability, and will change in value from 10 to 20% from room temperature to freezing. This phenomenon can be verified by connecting the output of the tone generator to a counter, and then placing the tone generator in the refrigerator. A significant change in frequency will be noted.

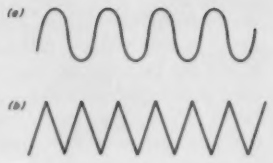


Fig. 2. (a) Waveform with Rx in circuit; (b) Waveform with Rx removed from circuit.

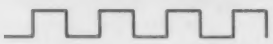


Fig. 3. Waveform at square wave output.

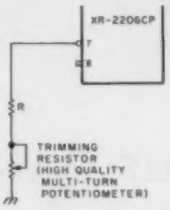


Fig. 4. Adding a trimming resistor to adjust frequency.

The temperature stability of the tone generator circuit can be improved considerably by using temperature-stable components for R and C. For C, mylar™ or silver mica capacitors should be used; for R, 1% resistors of the variety RN55 (an industry designation) should be used. These components exhibit good temperature stability, and are readily available from the supply houses listed at the end of the article. Fig. 5 shows a stable oscillator with a table of components for various frequency ranges.

The XR2206 IC is a unique chip in that it is designed for two-frequency or AFSK operation. If the circuit in Fig. 6 is used, the frequency will change from 1000 to 1170 by grounding pin 9. By adding a relay, as shown in Fig. 6, this circuit may be used for AFSK keying. The output of the oscillator is continuous when changing frequency, as shown in Fig. 7, and thus the oscillator may be used to modulate an SSB transmitter to produce FSK.

Tone-Burst Oscillator

Fig. 8 shows a simple tone-burst oscillator. Point C is connected to the push-to-talk line in the transmitter. When the transmitter is keyed, a short tone burst is generated and fed to the audio circuit of the transmitter. R_T adjusts the time duration of the tone burst, and R_A controls the output tone level. Choose C and R according to the formula shown for the desired frequency.

Subaudible Oscillator

A simple subaudible tone oscillator may be constructed by using the circuit in Fig. 8. In this case, omit the NE555V and its associated components, and connect pin 4 of the XR2206 to +12 V. The output of the subaudible generator should be connected to the high side of the modulation or deviation control in order to bypass audio speech filters that pass speech in the 300-3000-Hz range. This type of oscillator is called

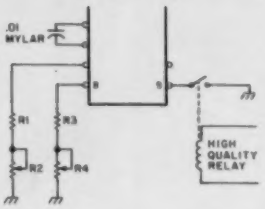


Fig. 6. AFSK oscillator. R1 = 90,900 RN55, 1%; R3 = 75,000 RN55, 1%; R2, R4 = multiturn miniature 20k pot, such as Beckman or Spectrol, which are used to trim the frequencies to 1000 Hz and 1170. Hz, respectively.

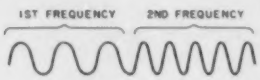
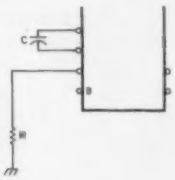


Fig. 7. Oscillator output when changing frequency.



Frequency	C	R
100 Hz	.01 mylar	1 meg
500 Hz	100 W V dc	200,000
1000 Hz		100,000
1500 Hz		66,500
2000 Hz		49,900
3000 Hz		33,200
5000 Hz		20,000

Fig. 5. Stable oscillator. Resistors are 1% tolerance MIL style, RN55D, RN55C, or RN55E. f = 1/RC.

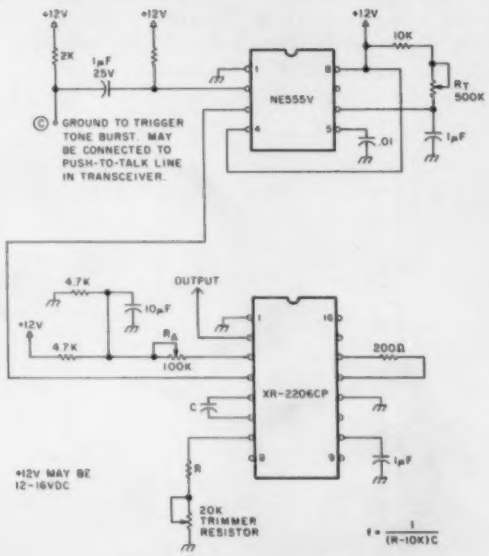


Fig. 8. Tone-burst oscillator.

subaudible since FM receivers with private line or tone squelch capability filter out frequencies below 300 Hz, and are not passed to the audio stages. Subaudible frequencies (frequencies below 300 Hz) are used to activate a private-access repeater or station.

Audio Test Generator/ Code-Practice Oscillator

A simple audio test generator may be constructed by using the circuit in Fig. 4. If R is 10k and the potentiometer is a 500k pot, the frequency may be varied over the range of about 200 Hz to 10 kHz. This simple generator may also be used as a code-practice oscillator by placing a key between +12 V and pin 4 of the XR2206.

Other Function Generators

The circuits given in this article were based on the XR2206, which was chosen because of its ease of use and availability. Other function generators, such as the XR2207 and the Intersil 8038, may also be used to generate audio frequencies. However, they are not the same as the XR2206 and lack some of its capabilities. If these other chips are to be used, a set of application notes should be obtained from your distributor. ■

Sources for Parts

XR2206CP, NE555V, .01 mylar (mylar film), nonprecision resistors and other parts—James Electronics.
Resistors, capacitors, and multiturn trimming pots—Poly Paks.
Precision 1% resistors—Harvy Electronics, Vestal Parkway E., Vestal NY 13850, or Cramer, Summitt, and other large distributors.

Synthesize Your Ashtray

—article for non-smokers

Let your dashboard do it for the 22S.

Hugh S. Pearl WB9VWM
2502 Oak Lane
Rolling Meadows IL 60008

Being a non-smoker and the owner of an Icom IC-22S provided me with a simple way to have a programmer built permanently into my car. The cup in the front ashtray is removable and has enough room in it for 8 miniature toggle switches and 8 diodes needed to program the 22S for any of its frequencies.

An aluminum plate was cut to fit the ashtray opening and drilled out for the switches and mounting holes. The back of the ashtray has a hole and rubber grommet in it to protect the connecting cable. A 9-conductor ribbon cable (10 conductor with one wire removed) was used with the accessory plug connected to one end. The photo shows a 24-pin Molex plug which my rig uses, but the 9-pin plug Icom provided works just as well. The switches, diodes, and ribbon cable were obtained from James Electronics.

I made a listing of the frequency conversion code and mounted it to my visor. When the ashtray cover is closed, the programmer is hidden in the dashboard. Best of all, now no one leaves old butts in my ashtray.

The connector in the radio is connected by the ribbon cable to the channel 22 switch position on the matrix board. The other 21 positions can be permanently programmed as you desire. ■

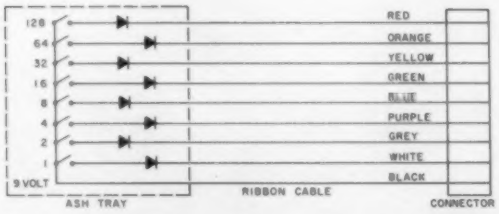


Fig. 1.

Midland's 13-510 Is One Great 2-Meter Mobile.

Our 13-510A Is Even Better!

NEW! The 13-510A P.L.L. synthesizer delivers 1,200 frequencies between 143.00 and 149.00 MHz . . . the full 2-meter band, plus MARS.

NEW! The 13-510A will operate with up to a 6 MHz split between TX and RX frequencies.

NEW! The 13-510A microphone connector is pre-wired for your Touch-Tone® encoding microphone.

NEW! The 13-510A has a 7-pin accessory connector for your Touch-Tone® dial, tone-burst generator or discriminator meter. *Touch-Tone is a registered trademark of AT&T.

NEW! The 13-510A is compatible with available popular CTCSS continuous tone-coded squelch system accessories.

NEW! The 13-510A has 3 transmitter outputs: 1, 10 and 25 watts.

Midland's 13-510, with its commercial-type modular construction, earned its reputation as one tough 2-meter FM mobile. Now Midland has made the 13-510A an even more versatile performer!

The 13-510A P.L.L. synthesizer splits the 6 MHz spread between 143.00 and 149.00 into 600 discrete frequencies, and a 5 KHz up-shift delivers 600 more for a total of 1,200 . . . shown directly on the digital display. In addition, there's access to 4 available offsets for repeater operation on ± 600 Hz with crystals supplied or up to 6 MHz spread with your crystals installed.

Inside the 13-510A, there's a highly sensitive (0.3 uV), highly selective (-70 dB at ± 15 KHz) dual conversion receiver with dual gate MOSFET RF and mixer stages, crystal filter in the 1st IF, ceramic filter in the 2nd IF, and helical resonators in the RF amplifier.

The transmitter is conservatively rated for 25 watts output, switchable to 1 or 10 watts for repeaters, and uses direct FM modulation to deliver natural sounding audio.

Other features making Midland's 13-510A the one to look at include automatic protection circuit for the output transistor, internal DC filtering and polarity protection, a deep-finned heat sink for the power transistors, and electronic switching that needs no mechanical maintenance. Mobile mounting bracket, base stand and push-to-talk microphone are included.

CHECK OUR SPECS:

RECEIVER. Type: dual conversion superheterodyne. 1st IF frequency: 16.9 MHz. 2nd IF frequency: 455 KHz. Sensitivity: Less than 0.5 uV for 20 dB quieting (0.3 uV for 12 dB SINAD). Spurious response: -60 dB. Squelch threshold: Less than 0.3 uV. Modulation Acceptance: ± 7.5 KHz. Selectivity: -70 dB at ± 15 KHz. Audio output power: 1.5 watts at 8 ohms.

TRANSMITTER. Outputs: 1, 10, 25 watts. Frequency deviation: Adjustable 3 - 16 KHz (normal 5 KHz). Audio Input: 600 ohms. Modulation system: Direct FM. Spurious Radiation: Less than -60 dB below carrier.

GENERAL. Power: 13.8 volts DC, negative ground. Current drain: Transmit, 2 - 7 amps.; receive, 0.8 amps. average. Antenna impedance: 50 ohms. Unit size: 2-5/8" x 6-13/16" x 9-5/8". Unit weight: 6.6 lbs.

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Dr. Ralph E. Taggart WB8DQT
602 S. Jefferson
Mason MI 48854

Attention, Satellite Watchers!

—a solid-state monitor for GOES

The satellite doctor strikes again.

In a previous article in *73* (November, 1978), I described various approaches for reception of GOES (geostationary operational meteorological satellite) picture signals on S-band (1691 MHz). For the experienced satellite fanatic, the S-band conversion is the big snag to implementing GOES operations, since most have adequate display equipment to handle the APT mode pictures. For newcomers, however, the problem is more complex, particularly since many new converts to weather satellites have little experience in electronic construction. All things considered, the easiest approach for most is an integrated display monitor which permits photographs to be obtained from a TV-like display.

Photo A. The remote display terminal in the author's prototype. This used the cabinet, bezel, CRT, HV module, and yoke from a Robot fast-scan viewfinder. The cabinet contains these components and the relevant CRT circuits.

The *73 Weather Satellite Handbook* contains one such display unit that will do a fine job. This monitor is a multimode unit, however, and is designed to handle both geostationary and polar orbiting satellites. If geostationary spacecraft such as GOES are the major objective, there are several design simplifications which are possible. In addition, since designing the original unit, several new circuit ideas have been tried with good results. It seemed a good idea to present a circuit incorporating many of these ideas while, at the same time, getting at a unit that was designed strictly with GOES service in mind.

Before getting into a discussion of the unit, a short digression on design philosophy is in order. There is no single-circuit solution to any given problem. Some approaches are more complex than others, and each has its own unique trade-off between simplicity and performance. As is always the case in my published circuits, I have taken the simplest approach that will yield quality results. If you think you have a better solution at one point or the other, feel free to modify the beast. If worse comes to worst, you can always put it back in its original state with assurance that it will do a good job.

The second problem facing the home constructor these days is the matter of obtaining parts. It gets hard enough to obtain garden-variety components at times, without trying to duplicate a circuit where the author had access to a one-of-a-kind part left over from the construction of the last lunar module! In that regard,

you can rest assured that all of the parts specified are widely available and a wide margin for substitution exists. In each case where this is possible, I will try to outline what you should look for in substitute parts. Virtually all of the specified components are available from local distributors, off the pegboard at your local Radio Shack, or from mail-order supply firms.

Finally, as an aid to those who are terrified of what looks like a complex project, virtually all of the active circuits for this monitor have been boiled down to single large plug-in circuit boards with only 14 connections to the outside world. For those without facilities for making PC boards, the boards are available, as I will note later.

Circuit Functions

In the broadest sense, the monitor has to take the satellite video signal and turn it into a meaningful image. To understand how it does this, we must first understand the satellite video format which is summarized in Fig. 1. GOES pictures are transmitted in the APT (automatic picture transmission) mode, and, for the sake of discussion, the overall circuit can be broken down into a number of fundamental subunits, each with its own function.

(1) Video circuits—These circuits must filter the signal to remove any components outside of the video passband and must demodulate it in such a way that maximum subcarrier amplitude (white) results in a bright trace on the screen, while minimal amplitude (black) causes the trace to be extinguished.

(2) Sync Circuits—Here we must maintain a precise 4 Hz trigger rate in order to display the picture properly. Since it is possible to record the satellite pictures on standard audio tape, it is most useful if the sync circuits will function even with the speed variations resulting from the recording and playback process, in addition to handling satellite signals in real time.

(3) Phase circuits—Although the sync circuits maintain the proper trigger rate, they cannot assure that the line trigger pulse that starts each display line corresponds precisely with the start of each line of satellite video. Without special provisions for phasing the picture, you are likely to get a display where the left edge of the actual picture falls somewhere inside the display frame, forcing you to cut and paste the picture to get the proper display.

(4) Horizontal deflection circuits—In this case, we want to generate a linear, 250 ms line each time a line trigger pulse is produced by the sync circuits.

(5) Vertical deflection circuits—Here we want to produce a linear vertical scan which requires 200 seconds for the trace to move from the top to the bottom of the screen. If 8-second frames in slow scan (SSTV) are actually slow scan, then APT pictures with their 200-second frame intervals are very slow scan indeed!

The remaining functional description will center around Fig. 2 (a system block diagram) and the schematics in Figs. 3-8.

Video circuits (Fig. 3). The video signal from the receiver or tape recorder enters the unit at J1 across the 10k CONTRAST control (Fig. 7). Since the gain of all circuits after the CONTRAST control is fixed, it is this control that determines the amplitude of the final processed signal and, hence, the contrast of the displayed pictures. From the CONTRAST control, the signal enters the main circuit board on pin 12 (Fig. 3) where it passes through an active filter (U1) set up for a center frequency of 2400 Hz, a bandwidth of 1600 Hz, and unity gain. The 2840-Ohm resistor in the input circuit sets the center frequency, and can be approximated closely enough by paralleling two 5600-Ohm resistors. From the filter, the signal is routed to U2, which is the video power amplifier. Here the signal gets a significant power boost. A part of the subcarrier signal is tapped off at "A" for the sync circuits which will be described shortly. The signal is also routed off the board at pin 15, where it goes to T1 to be stepped up in voltage in the high impedance secondary windings. Here it is detected by a bridge rectifier network. The output of the detector is a 4800 Hz waveform (positive going) whose amplitude is proportional to the instantaneous amplitude of the satellite subcarrier. This signal is applied to the CRT grid across a 10k load resistor (Fig. 7).

The CRT is biased by the BRIGHTNESS control in the cathode circuit so that the tube is just cut off (the trace is just extinguished when viewed in a dark room). Any positive excursions at the grid will cause the trace to brighten proportionally to the applied voltage which is precisely what APT display requires. About 5 V swing on the grid is all that is required for useful display. To prevent transients or other inputs from blooming the trace, a conventional silicon diode and zener are used across the grid resistor to provide peak white limiting by holding voltage at the grid to a maximum of a little over 5 V. Q1, the blanking transistor, is driven by the line trigger pulse, pulling the grid to near ground potential and blanking the trace during horizontal retrace.

Sync circuits (Fig. 4). The operation of the sync circuits is based on the fact that the 2400 Hz satellite subcarrier is locked to the same master frequency source as the 4 Hz line trigger generator. If we can lock a stable frequency source to the subcarrier signal, it is possible to derive the 4 Hz line trigger rate by digital frequency division. Our reference source in this case is a 565 phase locked loop. The internal voltage controlled oscillator (vco) of the loop is adjusted to free run very close to 2400 Hz by the 1k vco pot. When a sample of the subcarrier signal from "A" is applied to one input of the phase comparator, the vco is pulled onto the subcarrier frequency with the vco output providing a stable source for frequency division. The loop will follow any reasonable frequency changes caused by speed changes in the tape recorder, thus providing

Subcarrier frequency	2400 Hz
Subcarrier modulation	FM
White level	maximum amplitude (@ 96%)
Black level	minimum amplitude (@ 4%)
Dynamic range	@ 14 dB
Line rate	4 Hz (240 lines/min.)
Direction of horizontal scan	left to right
Frame rate	200 seconds
Direction of vertical scan	top to bottom
Number of scanning lines/frame	800
Aspect ratio	1:1 (square)
Baseband video bandwidth	1600 Hz

Fig. 1. Characteristics of the APT satellite video format.

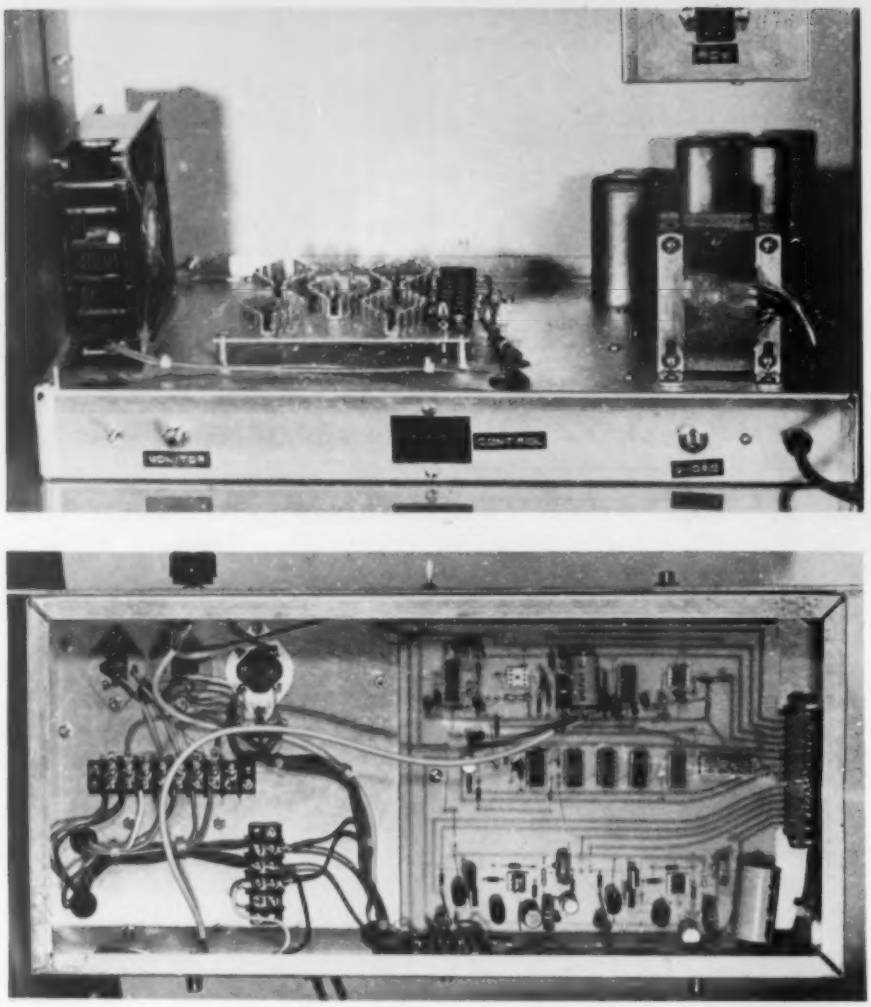

Photo B. Above chassis (top) and below chassis (bottom) views of the electronics assembly of the author's prototype. This unit contains the power supply and the main circuit board. A fan was required to compensate for inadequate heat sinking of the regulators (see text).

for display of recorded video as well. The vco signal from the PLL (U3) is routed through a series of gates in U4 to provide phasing, a function I will discuss shortly. The 2400 Hz output from U4 is then routed to a frequency divider chain composed of U5, U6, and U7, providing a total frequency division of 600. Since 2400/600 = 4, we have derived the proper line trigger rate. This 4 Hz signal is routed to a 12 ms single-shot (U8) which generates the required trigger pulse. A sample of this pulse is routed to board pin 10 for blanking, while another sample, "B", is used to actually trigger the horizontal deflection system.

Phase circuits (Fig. 4). Although the phase locked sync system does maintain the proper line rate, it cannot assure that the line triggering in the display coincides with the start of a line of video data. When it does not, which is likely to be the case most of the time, you get a situation where the left edge of the satellite picture is actually inside the frame. This condition is corrected by the phase circuits. To understand their function, it is necessary to redraw a portion of Fig. 4 to show the connections of the various gates. This is done in Fig. 4(a).

The PHASE switch, a normally-closed pushbutton, has one side grounded and the other connected to the phasing bus on the main board at pin 8. Since the phase bus is normally grounded, this low is inverted to a high by gate D, and this high is applied to one input of gate B with the other input to the 2400 Hz PLL signal that is buffered by gate A. The 2400 Hz signal is thus gated through gate B and then through C without interruption on its way to the sync divider chain. When a phase error exists, however, the switch is pressed (opened), and the status of the phase bus is now determined by the state of the collector of the phasing transistor (Q2). This transistor is driven by the $\overline{Q}$ output of U8, which is high except during the 12 ms trigger interval when it goes low. This results in the collector of Q2 remaining low except for a 12 ms high that is coincident with the trigger pulse. This high is inverted to a low by gate D, and this low at one input of gate B stops the 2400 Hz signal for 12 ms. This interruption, occurring once each line, represents a 12 ms counting error in the sync chain so that the next trigger pulse is delayed for 12 ms, causing the beginning of the next satellite video line to appear closer to the left edge of the display. The PHASE switch is held down until the edge of the satellite video signal moves over to the left edge, at which point the switch is released. This restores proper sync, but, this time, the picture is properly phased.

A worst-case phase error, where the left edge of the picture was all the way at the right end of the 250 ms line, would require 20 line pulses to correct (250/12). Since the line pulses occur 4 times each second, the phase switch would have to be held closed for only 5 seconds (20/4). This is entirely ample since about 20 seconds is actually available for phasing at the start of each APT frame. The action of the phase circuits in stepping the picture into place is shown in Fig. 11.

Horizontal deflection (Fig. 5). The 12 ms trigger pulse at "B" turns on Q3 for the duration of the pulse,

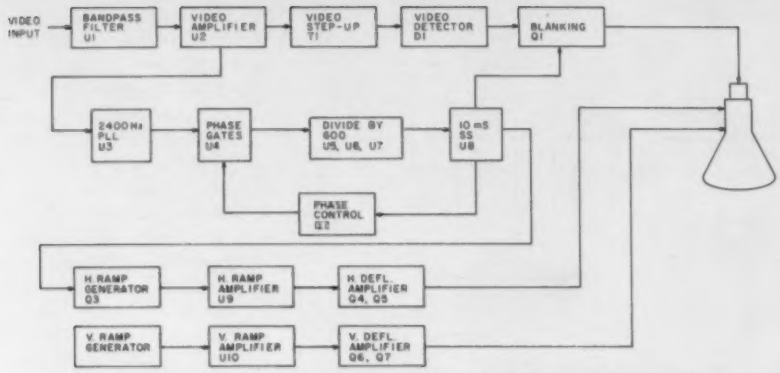

Fig. 2. A block diagram of the monitor signal processing circuits.

discharging the 4.7 uF capacitor in the collector circuit. When the trigger pulse is finished, this capacitor begins to charge through the HORIZONTAL SIZE control, producing a voltage ramp that is amplified by U9. The output of U9 drives the complementary output transistors (Q4 and Q5), which have the deflection windings in their emitter circuit (pins 5 and 6 of the main board). Feedback to the inverting input of U9 via the 100k resistors helps to linearize the deflection waveform. The HORIZONTAL CENTERING control feeds a voltage to the inverting input which provides centering of the trace.

Vertical deflection (Fig. 6). The vertical circuits, with a few exceptions, function much like the horizontal circuits, with the vertical deflection windings connected to pins 3 and 4 of the main board. The differences involve the use of a much larger discharge capacitor (2200 uF) to accommodate the 200-second sweep interval and the fact that the capacitor is cycled by a switch (the sweep switch) rather than a transistor. In the RUN position of the DPDT center-off sweep switch, a reed relay (K1) on the main board is pulled in, causing its contact (K1A) to short out the capacitor and reset the sweep at the top of the screen. When cycled to the center-off position (RUN), the contacts of K1 open, permitting the capacitor to charge and initiating the sweep down the screen. The other position of the switch (FOCUS) grounds the bases of Q6 and Q7, centering the trace on the screen. This position is used to focus the CRT or the film camera and also serves as a standby position when the monitor is not displaying pictures. The low-resistance vertical windings would cause one or the other of the deflection transistors to draw excessive current if left for long periods in the RESET or RUN positions. In the FOCUS position, neither transistor is drawing current, and they will sit indefinitely without overheating.

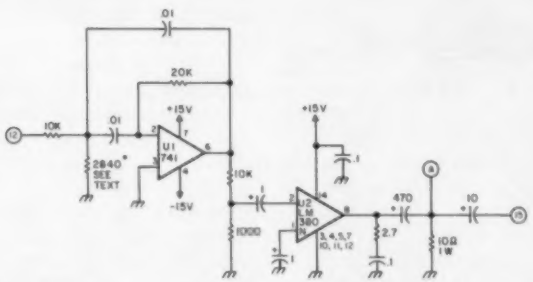

Fig. 3. Monitor video circuits. Unless otherwise noted in this and other schematics, all resistors are ¼ W, 5% carbon film, all decimal value capacitors are 50 or 100 V dipped mylar, all capacitors between 1 and 10 uF are 16 to 35 V tantalums, and all higher value capacitors are aluminum electrolytics rated at 16 V. All unmarked diodes are general-purpose switching types (1N457, 1N914, etc.). Circled numbers refer to board pinouts, while circled letters refer to interface points on other schematics.

Mainframe wiring (Fig. 7). Much of the mainframe wiring has been covered in previous circuit descriptions. In order to eliminate the chance that power transformers would cause unwanted deflection of the scanning beam, it is suggested that the power supply be remoted from the main cabinet. The mainframe does contain the +5, +15, and -15 V regulator ICs, driven from the unregulated voltage buses from the remote supply. If the regulators were mounted on the supply itself, you would get unwanted voltage drop in the connecting cable. In addition, the mainframe contains the high-voltage module for generating the +7-10 kV required for the CRT external anode. The high voltage module will be discussed in detail in the construction section. Regardless of the approach taken, however, it is desirable to power the module from its own regulators to minimize interaction with other circuit components.

Power supply (Fig. 8). This supply is one possibility for generating the required voltages. A low-voltage transformer (T3) provides the unregulated voltages via a bridge rectifier and filter capacitor network. The +350 volts required for the internal anode and focus grid of the CRT as well as the BRIGHTNESS network is obtained via a conventional power transformer (T2) and a full-wave rectifier assembly. T2 also provides the 6.3 V ac required by the CRT filament. The mainframe and power supply circuits are shown with Cinch Jones P-808-AB and S-308-AB connectors, respectively. An 8-conductor cable with an S-308-CCT on one end and a P-308-CCT on the other is used to interconnect the monitor and its supply. The power supply is turned on via an ac lead actuated by an SPST switch (S3) on the mainframe.

Construction

Main Circuit Board

Fig. 9 shows the land layout for the main circuit board which carries most of the active circuits. If you do not have facilities for making boards, this particular board is available—a point that will be covered at the end of the article. The component layout is shown in Fig. 10 as viewed from the component side of the board. The main puzzle in wiring the board is the cluster of unused holes between the LM380 and the LM565. These holes mark the demise of an idea that was better on paper than it was in prac-

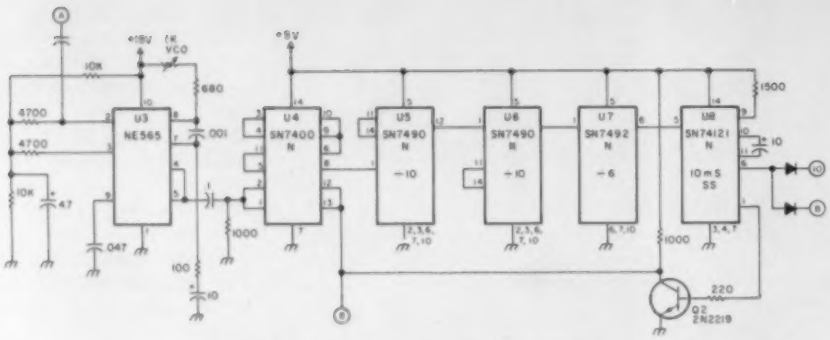

Fig. 4. Monitor sync and phasing circuits.

Photo C. An IR frame from GOES E displayed on the prototype monitor. Despite the small screen size, the picture is relatively clear, showing a major tropical storm off the west coast of Mexico. The IR format displays cold objects as white (space and high cloud tops), while warmer areas are darker. Note the warm surface temperatures in the southwestern US and northern Mexico in this frame. The use of a somewhat larger CRT would assure the full 800-line resolution in the APT pictures.

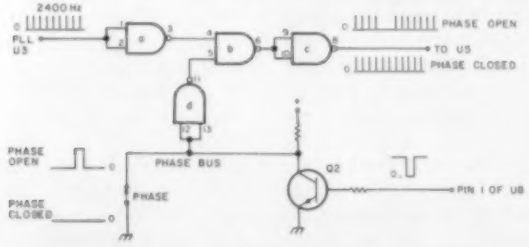

Fig. 4(a).

tice. The idea was to place a limiter in front of the PLL to remove any AM variations in the signal, thus improving the ability of the loop to lock on the subcarrier. That part worked, but the unforseen difficulty was that the limiter was quite sensitive to any noise, and, should it begin to limit on noise, much of the advantage of the PLL was lost. Out went the limiter notion!

In wiring the main board, sockets are suggested for all ICs. They do increase the cost of the project, but they suddenly seem worth it when you discover that you have a bad chip to replace! If you watch the polarity of tantalum and aluminum electrolytics and remember that all the ICs have the same orientation, you will not get into much trouble.

Mainframe

Once the board is finished, the remaining decisions revolve around the packaging style you want to use. The schematics of Figs. 7 and 8 assume that the monitor will go in one box with the power supply remoted on its own chassis. In terms of simplicity, this is probably the best approach to take. In the case of the prototype unit, I opted for a different scheme which got just a bit more complicated. I happened to have a Robot Research fast-scan viewfinder unit which had a suitable CRT, yoke, and HV module, so this was stripped and used as a remote display terminal. The power supplies and main circuit board assembly were mounted on a chassis behind a standard rack panel. Photo A shows the display terminal, and Photo B shows the rack-mounted electronics package. If I were doing the job over again, I would certainly follow the first route I suggested. No matter what scheme you employ, the power supply should be remote from the CRT circuits. It is virtually impossible to package everything in one cabinet and avoid unwanted deflection of the CRT trace by transformer fields. You can try if you want, but plan it so you can pull the transformers with minimal difficulty! When

you actually start to build the mainframe and power supply, you will run into situations where you may want to substitute, so let's look at some of those options.

CRT. The CRT used in the prototype was the original tube that came with the fast-scan viewfinder. It is a type 5M140P7M manufactured by Thomas Electronics, 100 Riverview Drive, Wayne NJ 07470. They made a larger tube for the Robot Model 70 SSTV monitor which is ideal for satellite display and has the same pinouts as the smaller tube used in the prototype. The latter measures only 4.25" × 3.25" (5 inches diagonally) and is really quite small for the display of an 800-line picture. Although the pictures are acceptable, you really can't get the full resolution unless you have a somewhat larger tube.

The one used in the Robot Model 70 is just about ideal. Both of these tubes have a P7 phosphor. This long-persistence phosphor is sufficient to let you see some aspects of the picture in real time in a dark room and therefore has some advantages. P4 phosphors of the type used in black and white TV sets will also work fine, although they do not have the long-persistence feature. If you have a Model 70 SSTV monitor on hand that is doing little these days with the advent of digital SSTV scan converters, you can use this as the basis for a conversion, as it will provide a cabinet, yoke, HV module, and a suitable power transformer. If you are building from scratch, I would suggest contacting Thomas and seeing what is available along the lines of the tubes they supplied to Robot. Their prices are quite reasonable compared to other sources. Failing this, you can check out various small black and white TV picture tubes at your local distributor. Many of these will work fine if you change the socket wiring to accommodate the pinouts. Many of these will have a 12 V filament which can be powered from another LM340T-12 regulator tied to the +LV bus.

HV Module. As mentioned above, the HV module for the prototype came from the Robot fast-scan viewfinder. Other Robot display equipment will furnish similar units. There are many designs available for such modules, and several alternatives are shown in references 1 and 2 and the SSTV section of reference 3. All of these are similar in that a power transistor is hooked up as an oscillator operating into the primary of a standard TV flyback transformer with the HV rectifiers and capacitors in the secondary circuit. The main difficulty with most is that the suggested feedback circuits to run the oscillator are highly dependent on the specific flyback which is specified in each case. Another approach worth checking, if you like to play on the bench, is to use a 555 timer chip as an oscillator at about 20-25 kHz and use this to drive the power transistor as a switch in the flyback primary circuit as shown in Fig. 11. This approach should work with just about any flyback, and you simply choose your primary taps to achieve the desired output voltage.

Transformers. T1 in the video circuits (Fig. 7) is a standard audio output transformer with an 8-Ohm secondary winding (actually used as the primary in this application), and primary windings can be anything from about 1k to 16k. Calectro and others make quite a few that will work just fine—simply look for a "universal" output transformer if you can find one that seems to be custom made for the application. Power transformers are comparatively noncritical as well. If you convert a Robot Model 70 monitor, the power transformer in that unit has all the proper windings in one package. If you go the route of separate transformers, as shown in Fig. 8, you can use the following guidelines in making substitutions.

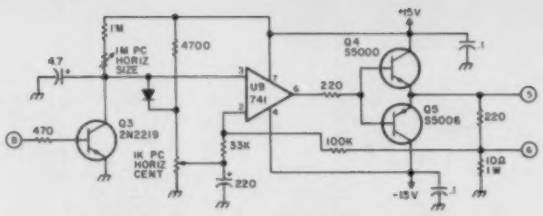

Fig. 5. Horizontal deflection circuits.

The LV circuit requires that the voltage on both the + and − buses be at least 17-18 V for the 15 V regulators to operate properly. The regulators themselves will take up to 30 V when properly heat sinked, so any transformer that will deliver between those dc limits will work fine. It should be capable of supplying at least 1 Amp, and 2 Amps is better yet. The HV supply is low current, and there are a variety of power transformers with 225 and 250 V c-t secondaries in the 25-50 mA range which will work fine. All of these have the required 6.3 V ac filament winding.

Deflection yokes. Any deflection yoke designed for a small solid-state black and white TV set will do the job here. If you have a choice, pick a yoke with higher resistance windings in preference to one with very low resistance.

Cabling. You can do anything you want in this area, from hardwiring the two units together to the use of exotic cable assemblies. Figs. 7 and 8 specify the use of a Cinch-Jones P-308-AB

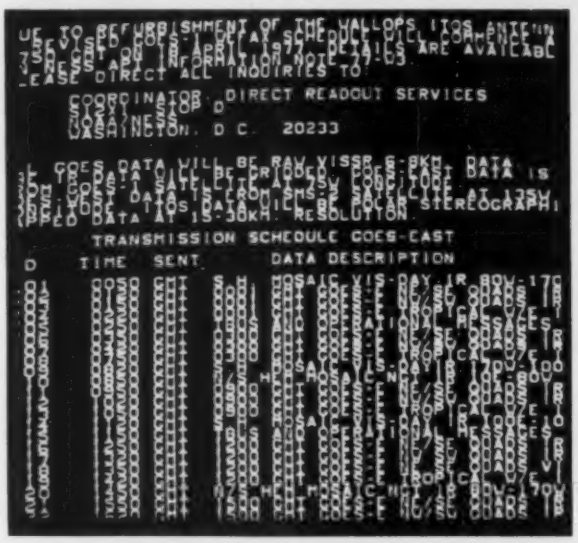

Photo D. An example of an operational message. In this case, it is a system status announcement and part of the transmission schedule for GOES E. This example shows the old format with white letters on a black background. The current format uses black letters on white.

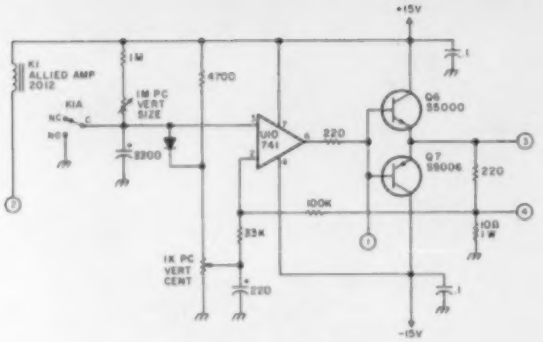

Fig. 6. Vertical deflection circuits.

on the mainframe and an S-308-AB on the power supply. An 8-conductor cable terminated with an S-308-CCT on one end and a P-308-CCT on the other connects the two units. These plugs and sockets are available from almost any distributor and are inexpensive compared to other options. Of course, octal plugs and sockets could be used if you can tolerate wiring the former —I can't! Just be sure to use a socket on the supply and a plug on the mainframe lest you electrocute yourself some evening while wrestling with cables!

General Notes

Only a few general guidelines are necessary in actually wiring up the mainframe and power supply. The first is to adequately heat sink the IC regulators. Dinky sheet aluminum sinks were used in the prototype, and this required the use of a cooling fan to stop them from shutting down when they got too hot. Generous extruded aluminum units are a good investment and will keep the regulators cool. Note that the positive regulators (LM340T series) have their cases at ground potential, so no insulation is required in mounting them to a grounded heat sink. The negative regulators are a different story (the LM320T series). Either use mica washers to isolate the cases from a grounded heat sink or mount them individually on smaller heat sinks, each of which is isolated from ground.

In hooking up the deflection yoke, first measure the resistance of the two windings. One is almost always higher than the other. Use the high resistance member of the pair for Y2 (vertical deflection) and the low resistance one for Y1 (horizontal deflection), and orient the yoke accordingly.

Ordinary hookup wire can be used in most interconnections, but you should use shielded wire in the CRT grid circuit and in the video input circuit to and from the CONTRAST control.

S3, the SPST POWER switch, is best incorporated on the BRIGHTNESS control, so choose a pot with a switch assembly. Wire the BRIGHTNESS pot so that, when the switch is off, the center arm of the pot is at ground potential. This will assure that CRT brightness is always minimum when the unit is first turned on.

The HV module should be mounted quite close to the external anode of the CRT so that only a short length of HV cable is required for the anode connection. The HV module should operate off its own regulators (as in Fig. 7) to minimize its effect on other circuits.

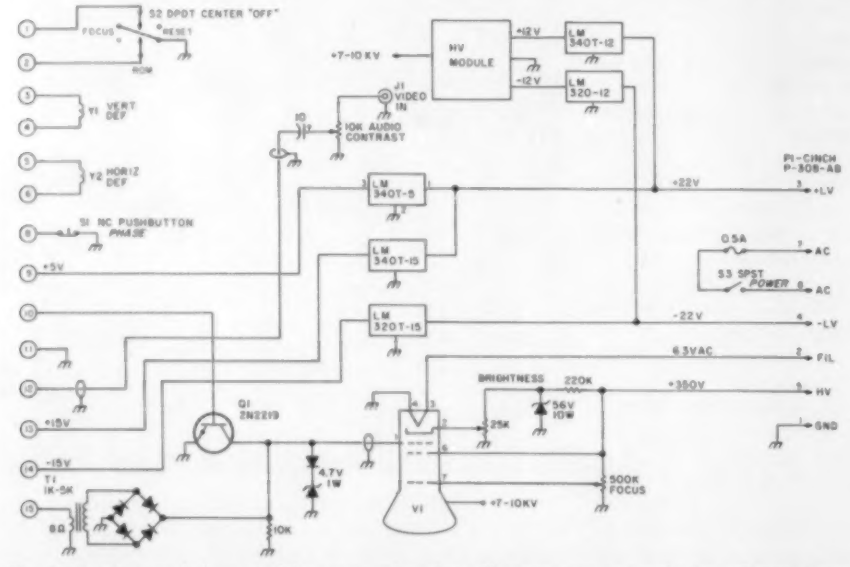

Fig. 7. Monitor mainframe wiring, assuming that all components, exclusive of power supplies, are in one cabinet.

Setup and Operation

Preliminary Setup

By all means, check and recheck all connections prior to powering up. In particular, the +15, +5, and −15 V lines should be checked for proper voltages. To start with, remove U9 and U10 from their sockets and connect the board to the ground, +15, and +5 V lines with the board on the bench.

(1) Connect a frequency counter to the junction of the .1 uF capacitor and 1k resistor at the output of the 565 circuit. Adjust the vco control for a reading of 2400 Hz.

(2) A counter or logic probe should show a 4 Hz signal on pin 8 of U8. A short pulse should be observable on pin 6 of U9 using a logic probe or scope. This pulse should occur at the 4 Hz line rate.

(3) Connect a scope or logic probe to pin 8 of U4. Gaps in the output of 12 ms at the 4 Hz rate should be noted. Use a test lead to ground pin 8 of the main board, and the gaps should disappear.

You can now plug the main board into the powered down monitor. Preset all controls as follows:

CONTRAST (panel)	minimum (max. CCW)
H SIZE (board)	midrange
H CENTERING (board)	midrange
V SIZE (board)	midrange
V CENTERING (board)	midrange
SWEEP (panel)	FOCUS
FOCUS (panel)	midrange

(1) Advance the BRIGHTNESS control to

engage the power switch but no further. Allow 5 minutes for the unit to warm up.

(2) Slowly advance the BRIGHTNESS control in a dimly-lit room until a trace is just visible. If the trace is not horizontal, loosen and rotate the yoke until it is. Sharpen the trace with the FOCUS control.

(3) Mask off the largest possible square area on your CRT. This will be referred to as the "viewing area."

(4) Adjust the HORIZONTAL SIZE and CENTERING controls on the main board so the trace extends from one side of the viewing area to the other. Momentarily ground the collector of Q3. The trace should jump to the left edge of the viewing area. If it jumps to the right, you should power down and reverse the connections to Y1 and then reapply power and repeat the size and centering adjustments.

(5) Cycle the SWEEP switch to RESET. The trace should move upward. If it goes down, you should power down and reverse the connections to Y2 and power up again.

(6) With the SWEEP switch in the RESET position, adjust the VERTICAL CENTERING so the trace is even with the upper margin of the viewing area.

(7) Cycle the SWEEP switch to RUN and adjust the VERTICAL SIZE control so that it requires 200 seconds for the trace to move from the top to the bottom of the viewing area. You will probably have to cycle between RESET and RUN several times to get this right, but it is critical if the pictures are to have the proper aspect ratio.

(8) Back the BRIGHTNESS down to the point where the trace is just extinguished in a dark room.

(9) Play a tape-recorded satellite signal into J1 starting somewhere in the middle of a frame transmission. Slowly advance the CONTRAST control to achieve the best swing between black and white. If you go too far, the screen will be completely white due to the action of the white limiting, and, if you don't go far enough, you will lose some information at the black end of the picture signal. At this point, you should see a picture, but it will probably be out of phase. Press the PHASE switch until the edge of the picture lines up with the left edge of the viewing area.

At this point, you have tested all of the elements of the monitor and are ready to display a picture. Generally, you will not have to alter the CONTRAST control settings unless you change the input level to the monitor.

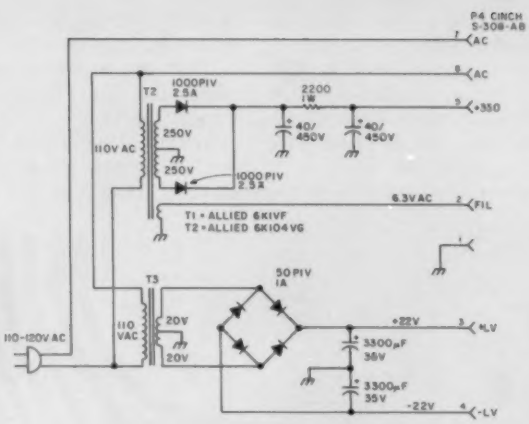

Fig. 8. Power supply circuits.

Operation

Either a Polaroid™ camera with a closeup lens or a conventional roll-film camera can be used to take pictures from the monitor. It should be firmly mounted at the proper distance from the monitor and ideally should employ a cable release to actuate the shutter. Reference 2

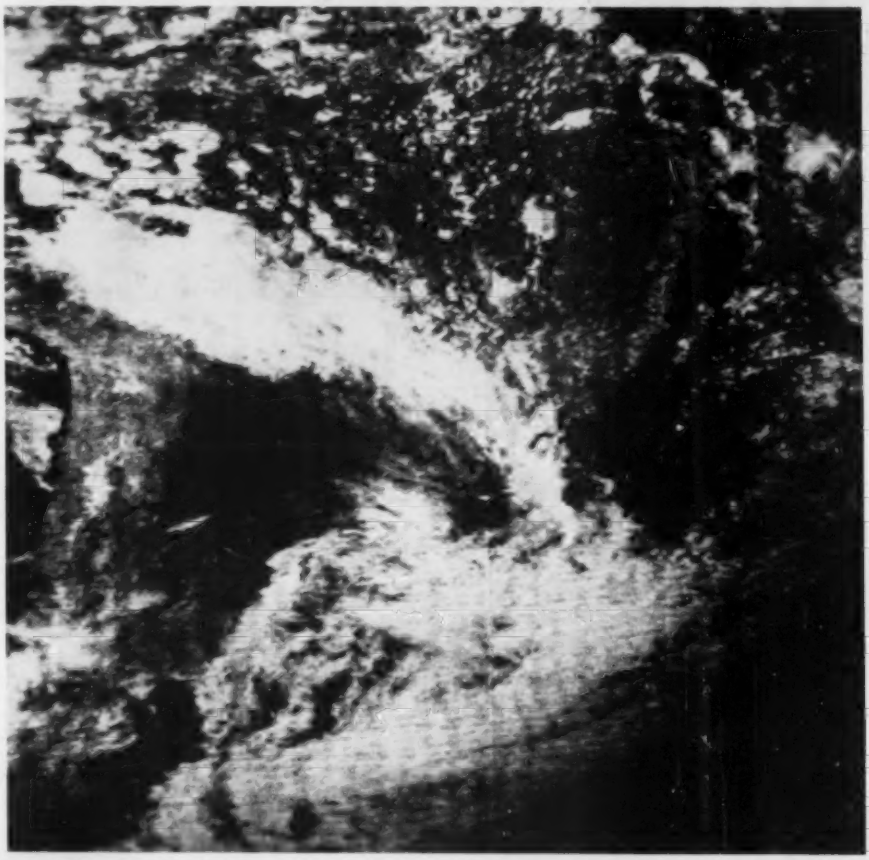

Photo E. A visible light frame of the SE quarter of the earth disk as seen by GOES E showing almost all of South America. This is an afternoon frame, so the eastern limb of the disk is already darkening as the terminator appears, marking local sunset in the South Atlantic.

contains a great deal of useful information about photography from CRT displays, and I won't repeat it here. In each case where the monitor is used, you should allow at least 5 minutes for warmup to get reproducible results. Whenever the monitor is on but not displaying pictures, the SWEEP switch should be in the FOCUS position. When you are ready to display a frame, it can be cycled to RESET.

The picture will begin with a few seconds of start tone—300 Hz modulation of the subcarrier which results in a distinct bar pattern on the trace. When the tone terminates, you should observe a black area somewhere along the trace. Press the PHASE switch to move this to the left edge of the viewing area. 20 seconds after the end of the start tone, cycle the SWEEP switch to RUN and the frame will begin to

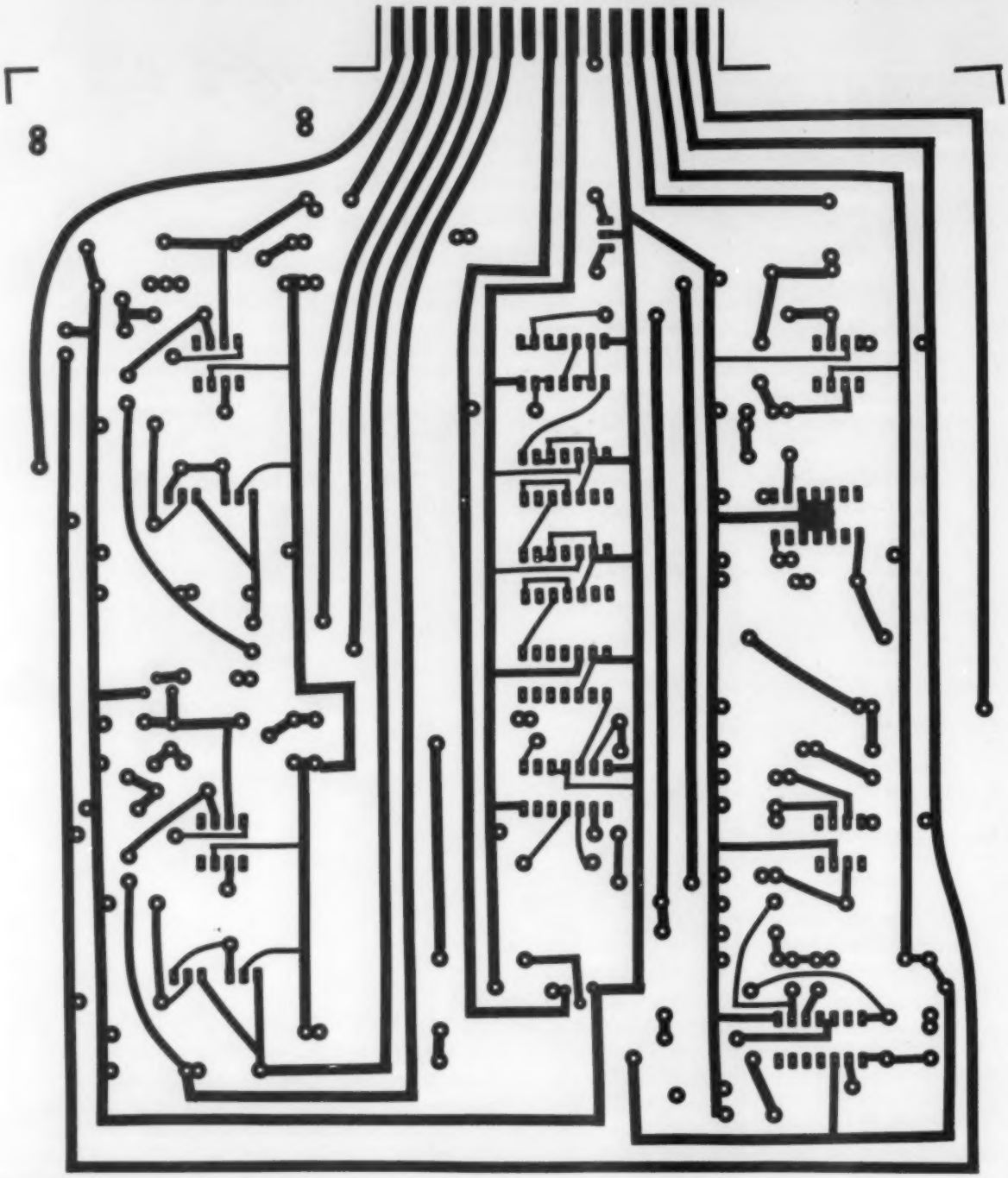

Fig. 9. PC board layout (foil side) for the main circuit board.

read out, beginning with the ID header, followed by the actual frame. About the time the scan reaches the bottom of the viewing area, you will hear a 450 Hz stop tone which tells you the picture is finished. In photographing the display, you should use a completely dark room unless you have a light hood assembly for the camera. The shutter should be opened as you cycle the SWEEP switch to RUN, and it should be closed when you hear the stop tone. If you want to copy another picture immediately, simply cycle to RESET and await the next start tone, otherwise set the switch to FOCUS until you are ready for the

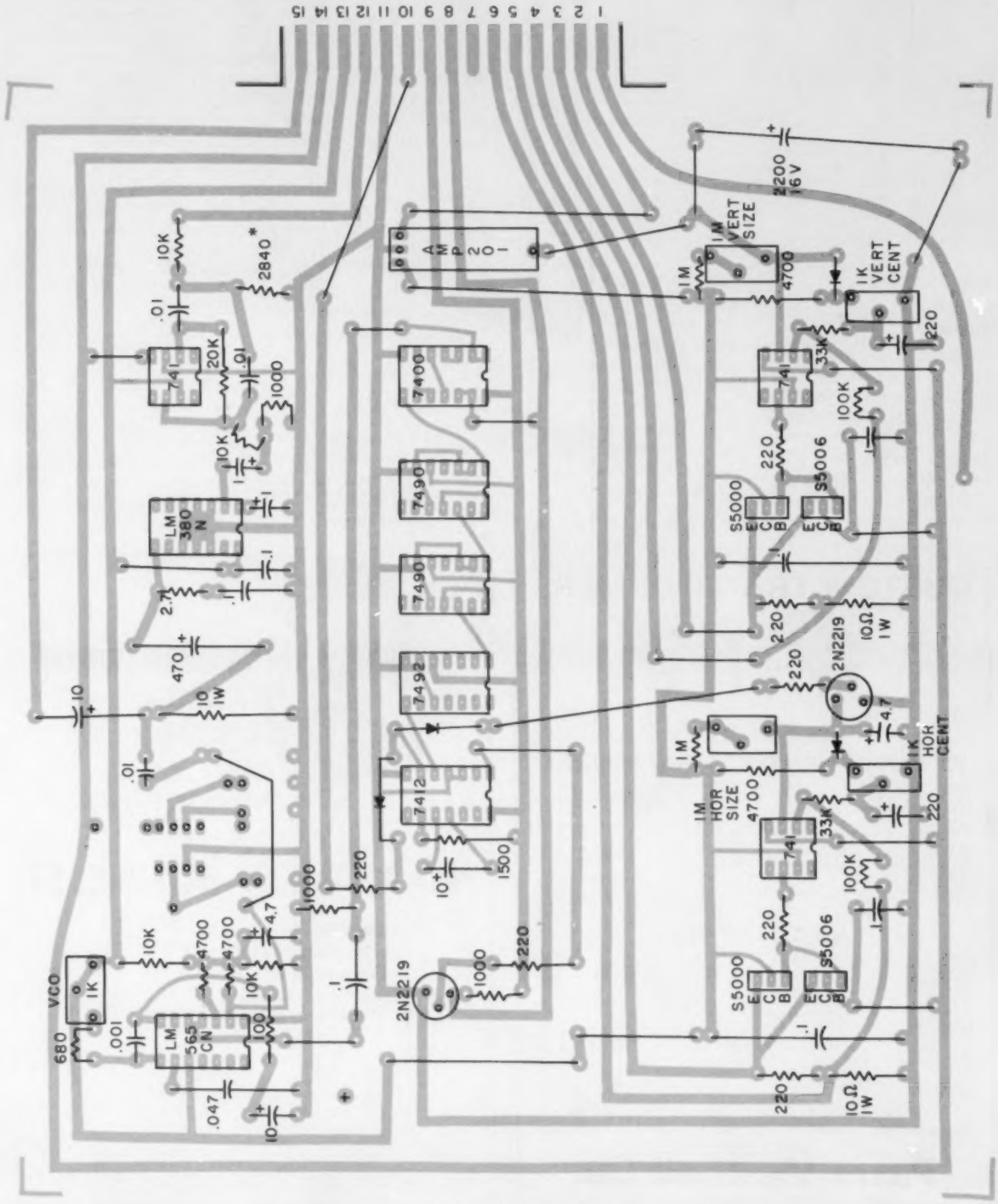

Fig. 10. Component side layout for the main circuit board.

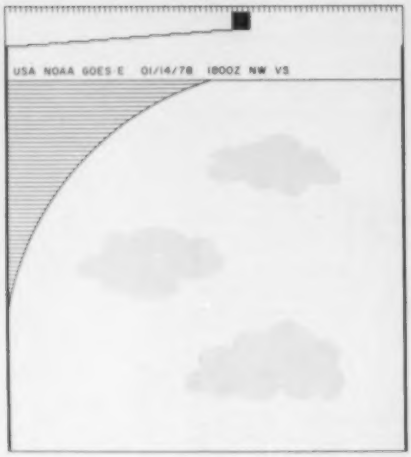

Fig. 11. Operation of the phasing circuits. The top of this segment is the start tone (300 Hz modulation of the subcarrier) where the PLL first locks on the signal. This is followed by a 25-second phasing interval. Note that the edge of the picture, marked by the black bar, is inside the viewing area. When the PHASE switch is pressed, the bar begins to move toward the left edge of the picture where it belongs. When it reaches the edge, the PHASE switch is released and the picture drops back into sync. Note that the last 5 seconds of the phasing interval is devoted to an ID header for the picture. Normally, phasing is done with the sweep switch in the RESET position and the switch is cycled to RUN about 20 seconds after the end of the start tone, permitting the ID header to be displayed.

next frame.

Summary

Photos C, D, and E show typical GOES APT frames displayed on the prototype monitor. Despite the small CRT size, the pictures are quite acceptable. The use of a larger CRT would sharpen them noticeably, however. With a larger CRT, the display can come quite close to the results achieved with a good photographic fax system with considerably less fuss. Polaroid film will give you almost instant prints with little bother, or the use of roll film will let you prepare enlargements at any size you desire.

This is actually an easy unit to build and operate and probably represents one of the easiest ways to get into GOES picture display. With a few modifications, the unit can also be used to display VHF pictures from the new series of polar orbiting satellites that became operational with the launch of TIROS N.

Circuit boards are available for this project from METSAT Products, Box 142, Mason MI 48854. The main circuit board, G-10 epoxy, drilled and plated, and a documentation pack costs $50. If you want to go this route, ask for minikit GM-1. ■

References

1. Taggart, R.E., *The Weather Satellite Handbook*, 73, Inc., Peterborough N.H

2. Miller, D. and R.E. Taggart, *The Slow-Scan Television Handbook*. 73, Inc., Peterborough NH.

3. ARRL, *Specialized Communications Techniques*, American Radio Relay League, Newington CT.

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73 Magazine *Staff*

Batteries Dead?

— take preventative measures

Your worries are over if you use battery status indicators.

One of the problems associated with battery-operated equipment is knowing that the battery supply has been turned on and/or that the battery voltage is still within suitable limits. Suitable limits might mean the voltage range necessary for a circuit to perform properly, or the upper voltage limit that a rechargeable battery pack should have when it is properly charged and the lower voltage limit when discharged to the point where its usage should be discontinued before the battery pack is damaged by too deep a discharge.

Depending on the capacity of the battery used, one can "afford" only certain types of battery status indicating circuits. Obviously, for a small piece of test gear operated from a 9-volt transistor radio-type battery, even the use of an LED or the smallest incandescent lamp available will take too much current (15 to 20 mA) compared to the milliampere hours (mAh) rating of the battery (62 mAh for an inexpensive 9-volt type). On the other end of the scale, using a higher capacity battery source, one can "afford" even elaborate battery status circuits that provide detailed information regarding battery condition.

This article explores several interesting battery status circuits including ones that will work with even the lowest capacity battery source to more elaborate alphabetic indicators. Some of the circuits use discrete devices although ICs are available to do the job. Discrete device circuits don't take significantly more current and use commonly available components, whereas the ICs may not be readily available.

Before getting to the circuits, one might mention meters as battery status indicators. The availability of inexpensive, imported microampere meters might appear attractive to use because of the very low current drain. But, if one calculates the current change indicated by the meter as the battery voltage changes, it might not be very significant. The current change indicated depends on the internal resistance of the meter and any added series resistance. As an example, if a typical, inexpensive 500-microampere meter in series with a suitable resistor is placed across a 9-volt battery, the meter indication might only decrease by about 1/3 scale as the battery voltage sinks to 6 volts. This is not a very obvious indication that the battery voltage has fallen to the point where it will significantly affect the performance of many 9-volt circuits. Of course, there are often small battery status meters available during parts sales, but a true indication is obtained only when the meter is used for its designed purpose.

After having left many 9-volt-powered transistor checkers, bridges, and even portable receivers turned "on" instead of "off" after usage, with resultant battery loss, the circuit of Fig. 1 was finally discovered. It uses an LED as a battery "on" indicator, but the LED is flashed at a low duty cycle so the average current drain is only about 1 mA. The 2N4870 unijunction transistor forms a simple pulsed oscillator circuit which in turn drives a 2N2222

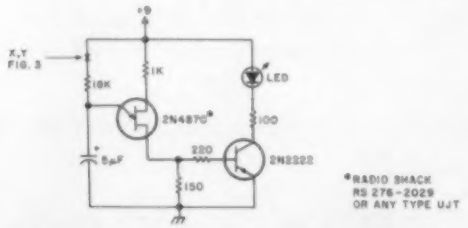


Fig. 1. Due to the low duty cycle of this flashing LED circuit, the average current drain is 1 mA or less.

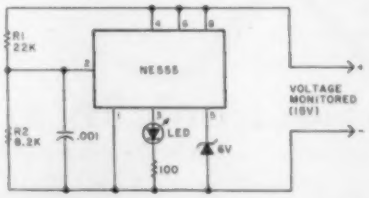


Fig. 2. The NE555 will trigger the LED on when the monitored voltage falls to 12 volts. The ratio of R1 to R2 only needs to be changed if it is desired to change the voltage point at which the LED is triggered.

switch that turns on the LED. The LED flashing rate and the battery voltage range which may be accommodated can vary over a wide range by the suitable choice of R1, R2, and C1. Flashing rates from 2 to 20 per second are the most attention-getting, while still keeping the average current consumption low. The battery voltage can be anything from 3 volts on up. The values in the circuit of Fig. 1 will produce a flashing rate of about 5 times a second from a 9-volt battery. A small amount of experimenting is necessary, particularly with R1 and R2, for other battery voltages. They should be raised in value for higher battery voltages and lowered in value for voltages below 9 volts, although their value is not at all critical. The cost of the batteries saved will rapidly repay the cost of the components for this circuit if you have any tendency at all to forget to turn off battery-powered equipment.

The circuit of Fig. 2 is an undervoltage indicator. It is particularly valuable when using nicad battery supplies since such batteries can be damaged if they are too deeply discharged. This circuit is useful only if there already is some sort of indicator on a piece of equipment informing the operator when it is turned "on," since this circuit will tell the operator when it is time to turn the equipment "off." As shown, the circuit is used to monitor a 15-volt battery source. The ratio of R1 to R2 is such that the LED will illuminate when the battery voltage falls to 12 volts, which is approximately 80 percent of the fully-charged voltage of the 15-volt nicad supply. The voltage value at which the circuit switches on can be controlled by changing the ratio of R1 to R2. The circuit can also be used on other supply voltages in approximately the 9- to 18-volt range. The circuit is quite sensitive and the turn-on of the LED when a low voltage condition is reached is distinct and sharp. If one wanted absolute protection, pin 3 of the IC can also be used to drive a small relay which would automatically turn off a piece of equipment. This might not be a bad idea for some operators who insist on a last transmission although their nicad battery packs are about to be damaged.

The circuit of Fig. 3 does not indicate when a supply is on, but it can indicate both an undervoltage and an overvoltage condition. This may be useful when charging certain types of battery packs where a fully-charged condition is indicated by a specific voltage level. The circuit can also be a warning device to indicate that the output of some device, such as a portable generator, is not within acceptable lower and upper voltage limits. The circuit can be set up for completely independent lower and upper voltage limits and the limits can be as far apart or as close together as desired. The critical components are the two zener

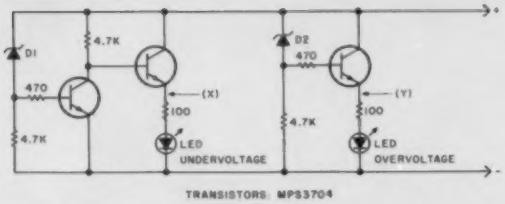


Fig. 3. This circuit will ignite the appropriate LED if the monitored voltage goes below or above the value determined by zener diodes D1 and D2.

diodes: D1 to set the undervoltage indication value and D2 to set the overvoltage indication value. These diodes have to be fairly exact in value. For instance, if one wanted to set the upper voltage indication at 15 volts, one would have to use a 15-volt, 5% tolerance zener or test a bunch of 10 or 20% tolerance zeners until a suitable diode is found.

The circuit of Fig. 3 provides a steady LED display for low and high voltage. A more attention-getting display can be obtained by combining the circuits of Figs. 1 and 3 so a flashing LED display is obtained. In this case, the LEDs shown in Fig. 3 are not used and the points marked X and Y are connected to the similarly-noted points in Fig. 1. Note that two circuits of the type shown in Fig. 1 are necessary.

The circuit of Fig. 4 provides a battery status display using a 7-segment LED readout. A low voltage state is indicated by display of "L", a high voltage state by display of "H", and when any in-between voltage is sensed, the display is a constant "F". One can arrange the connections to the readout to display differently depending upon one's fancy. For instance, one could have the display read "1" for high, "2" for in-between voltages, and "3" for low voltage. Another idea might be to have all segments on the readout active for a high voltage state and then progressively switch off segments for lower voltage states. By studying the diagram and the logic states to get the L, F, and H display, one can arrange other displays on the readout. The zener diodes are, again, critical in value if the circuit is to react when specific voltage levels are sensed.■

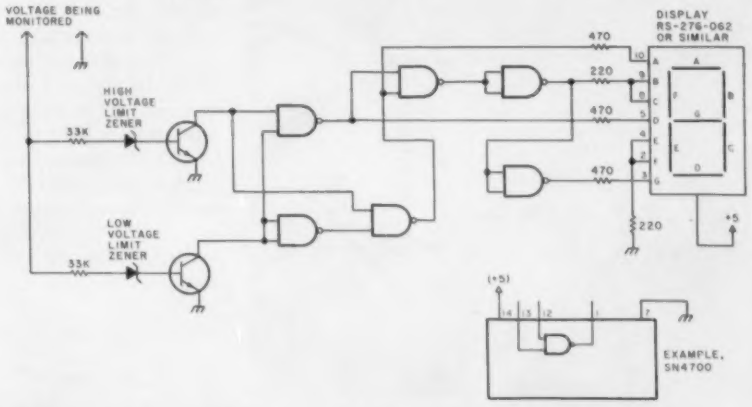
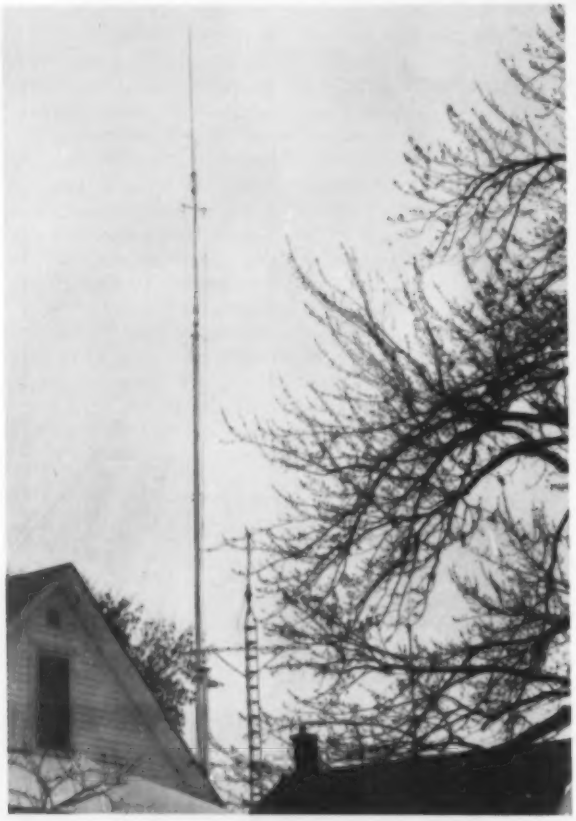


Fig. 4. This circuit uses an LED readout and displays an "L" when the monitored voltage is low, an "H" when the voltage is high, and an "F" when the voltage is between the low and high limits.

How to Nab a Jammer

—another use for 220

It's the Omaha VHF posse vs. the Red Rider.



This shows the 146.40/147 antenna with a 100' tip and, more difficult to see, the 222.34/223,44 repeater antenna with an 85' tip.

John Gebuhr WBØCMC
2340 N. 64th St.
Omaha NE 68104

It all started about a year ago when Omaha VHF was plagued by a character who went by the handle of "Red Rider." Every Saturday night without fail, for several weeks, he would come up on the 34-94 repeater: "Breaker one nine, this here's the Red Rider." Usually, no one would answer him (which was the best policy in the long run), and the first few weeks he shouted obscenities until he found out the repeater got shut off when he did. We would get fixes on him and close in "for the kill," and suddenly he would QRT for 15 minutes to a half hour and show up again on the other side of town.

After the 3rd week of this, it became obvious that he was listening to us on other 2m frequencies as we would track him. We used some very uncommon ones, but he obviously had a synthesized receiver. His transmitters were identified as a PLL type of moderate power (10-30 W) and also a low-power crystal, probably handheld, unit. (This was later verified.) The two transmitter fingerprints were watched for on legal transmissions, but never appeared until several months later.

One night, we used 5 or 6 ten meter mobiles and spotted his car, but he saw us about the same time and we didn't get a license number. We saw that evening that 10 meters would work, but to get enough 10 meter mobiles to do a good job proved a hassle, as did propagation.

A couple of days before, I had received a flyer from Clegg which offered ten 220 MHz radios for the price of eight. I asked the rest of the guys if they

would be interested in going together on this, and there seemed to be some interest. I took a chance and ordered ten. About ten days later they came, and, by nightfall, six had gone out the door. That was on Thursday night. By Saturday, the rest of them were in service and crystals were ordered for two repeater pairs and another simplex frequency. The following Monday, ten more Cleggs were on order, and two weeks later, there was a 220 repeater in Omaha with 19 users.

If one wonders what happened to the 20th radio, it is now the upper 34-94 repeater in north Omaha. The entire receiver lifted out of the case by loosening four screws and was put in a shielded box. The COR is a reed relay driven from the squelch circuit. R_{61} is removed from B+ and reconnected to the base of a PNP transistor, the emitter is connected to B+, and the collector goes through a relay coil to ground. A diode was hooked across the relay coil to reduce spikes (hysteresis diode). A 25 uF capacitor was later added to provide a short squelch tail. The LED was added as a cosmetic device.

Cavities were later made out of some 3" transmission line donated for the cause. A handful of "SMA" series connectors was used in the duplexer (because they were free) and a half pound of solder.

The repeater finished, we got permission from Motorola to put the thing up on the Woodmen Tower (300'+ above average terrain) for the weekend. The top of this building is a protected site and has what looks like a crewcut of top-quality commercial antennas — ATS, paging, business, railroad, and many others. I had managed to pack the entire repeater into a suitcase, duplexer and all, and we carried it up to the top, climbed out on the roof 425 feet above the street, and clamped a Ringo Ranger to a lightning rod. We took the repeater out of the suitcase, set it up, and put it on the air in about 15 minutes. The duplexer didn't need any retuning, and we were off to hunt Red Rider.

We had some success that night, but, unfortunately, Red didn't stay on too long and we didn't get him. For about four months, 220 was probably the best-kept secret in Omaha. And in those four months, we compiled a nice fat file including names, addresses, vehicle descriptions, footprints, and real dog smelling prints, and sent it to the FCC in Kansas City. The night that we got a positive ID on the Red Rider, the comments heard on the 2m 34-94 were, "This is the first Saturday night I'm gonna sleep soundly for a long time," and "Bad guys 31, good guys 1; that kind of evens up the score, doesn't it?"

The only thing that got on people's nerves after that was that it took the FCC about three months to do anything about it. Since the FCC came to town, though, there has been almost no deliberate interference or other flagrant rule violation.

By this time, it was obvious that 220 was here to stay, and there is now a second repeater here cross-linked with the 2m 40-00 machine, making possible, for many people, full duplex operation.

The second repeater is a Midland 13-509, which turned out to be the exact same radio as the Clegg, except for the case and name, right down to the Japanese fingerprints on the PC board. As it turns out, the Cobra 200 is also identical to the above two radios and is the cheapest one on the market.

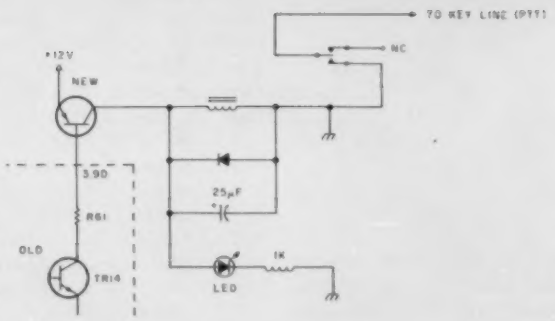


Fig. 1.

As with most ham gear, all three of these radios are imperfect and it is a lot of fun modifying them for various reasons.

Modification #1 eliminates the somewhat long squelch recovery time or reduces it to insignificance (with the squelch set near the edge of operation, it may take up to a full second for it to recover). By changing C89 and C91 from 4.7 uF each to 1 uF each, the recovery time is very fast without significantly impairing the operation.

Modification #2 removes the lamp behind the channel selector and replaces it with an LED. The LED is connected in series with R60 on the receiver board, and R60 is changed from 100 Ω, 1 W to 47 or 56 Ω, ½ Watt. The entire operation reduces receiver current from over 200 mA to about 140 mA. Modification #2(a) removes the meter lamp or puts a switch on it, reducing receiver current to around 60 mA, easily in the portable range.

Modification #3 removes the TX lamp and replaces it with an LED in series with the relay coil, reducing the low-power transmit current from 800 to 700 mA. The only degradation in performance this entails is that the transmitter must have 10.5 V minimum instead of 9.1 V to key properly. So, total low-power current drain is 1.1 A stock minus meter lamp minus channel lamp minus key lamps = 700 mA, clearly a significant saving. A 12 V gel cell will run the radio for a couple of days and still have power to spare (1.5 Ah).

Modifications #4 and #5 change the SO-239 to a BNC for quick disconnect, lower loss at this frequency, and the capability to use a rubber ducky. The power leads are removed and a quick disconnect plug and socket are installed.

Modification #6: The zener, D6, next to the 56 Ω resistor (in Mod. #2) is disconnected from the 9 V line as is the 9 V side of the LED/56 Ω network. An NPN 1 W resistor is put in as a series regulator, and a 1k resistor is added as shown in Fig. 2. This modification further reduces receiver current by 5 to 10 mA, and, as the zener is a ±5% device, the performance of the receiver is completely unchanged. The 9.1 V line should now be about 8.5 to 8.7 V.

I might at this point say that the part numbers above mentioned are the same for all three makes of radio. The instruction book that comes with the Cobra is far more complete than that with either the Clegg or Midland. It is a service manual, whereas the other two have only a schematic and block diagram.

I don't know when I've seen a radio that is more

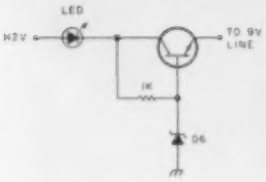


Fig. 2.

fun to play around with and tinker in and modify than these. They are very easy to work on, are laid out well, and come apart quickly.

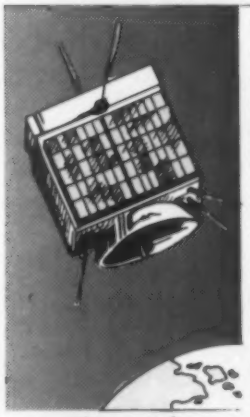
The first two batches of Cleggs probably sparked the biggest antenna building boom Omaha has ever seen. The two amateur stores had nothing and the only antennas available for 220 were from the local Larsen rep, and they were for mobile only. For the base antennas, most built 5/8-wave or ¼-wave antennas, and a few cut down Ringo Rangers to the proper dimensions.

There are only two minor problems I have seen with these radios that are really in the problem category and they are: First, the mike hanger button on the back of the mike is riveted too tightly, and, if it is dropped, frequently a crack appears between the button and the PTT switch. The second is the tuning on the output of TR 21. If one is not careful in tuning it, it can create spurs due to oscillation of the stage. A simple verification can be made of this by keying the transmitter and pulling the crystal while keyed. If the power meter shows output, it's oscillating. If the meter goes instantly to zero, it's probably not and is set alright.

One might notice a much greater difference in antenna position compared to 2m; because of the shorter wavelength, moving the antenna 5 or 6 inches one way or the other may make as much difference as a 2/3-scale reading on the S-meter. Objects which only partially reflect and partially absorb on 2m become good reflectors on 220, and, consequently, the interference fringes are much more pronounced (see optical behavior in any general physics book).

Looking to the future, I see 220 as a band that will grow by leaps and bounds in the next 2 or 3 years. The 220 class E is dead, there is a vast empty space there now in most parts of the country, and, as 2 meters becomes more congested, 220 and 440 are the next logical places to go. I also think one of the reasons 440 is so much more popular than 220 is the availability of used VHF gear retired from commercial service at very low prices. But, as people are finding out, 220 seems to take the best of both 2m and 440 plus a few points all its own and offers the individual a new playground to do as he wishes on VHF.

As a footnote to this, one of the 220 repeaters has become an administrative frequency for ARES and other such activities because of the large and ever-growing number of people who have 2m crystals in their scanners. 146.94 is a hot-selling rock in Omaha Radio Shack stores. People are finding out that, for weather watch information, 146.94 is where it's at. Inasmuch as we have stations at NWS and a 3rd weather wing at Offut AFB during severe weather and tornado watches, there are a number of bits of information which should not be passed over 2m, so, rather than tie up telephones or take a chance on upsetting the nonamateur public on 2m, they go via 220 as there are no scanners made which will pick it up.■



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This Station Plays Beautiful CW

—with a Morse keyboard

Roll over, Beethoven!

The international Morse code (CW) is a digital musical language. If you happen to be a straight-key master, such as K9ZTH, you can make music to rival that of Mantovani. If you happen to be blind, a talented pianist, composer, piano tuner, and a ham, you can even write a concerto using this musical language. Ol' Rip Snorter John (W9ORS) is such a person and is presently writing *The CQ Concerto*. The first few bars are great and I can hardly wait for the finished work, because it will include a CW message hidden within beautiful music.

Because timing is tricky, it is a challenge for a composer to work the unique rhythm of CW into conventional music. The dot is the basic unit of time in precise code. The syllable space between dots and dashes also requires one time unit. A dash is exactly three time units long and matches the letter space. The interword space is the mystical number 7.

Photo A. Diode matrix (front) forms 8-bit binary code. The 13 ICs (back) provide logic to convert binary code to Morse code. Keying and VOX relays at lower right.

The digital aspect of CW makes ICs ideally suited for application in keyers, keyboards, and readers. In the CW language, spaces are as important as the dots and dashes. Often hams forget that spaces are important. At times, a ham will send, "my nag is . . ." It is easy to run the "m" and the "e" together so that instead of having a *name*, the ham is a *nag*. Even old-timers with bugs and weighted keyers have problems. With dots set for 40 words per minute and dashes at 20 words per minute, the sender speaks with an accent. He can communicate with his own kind who have the same accent, but others who prefer the musical rhythm of good code have difficulty copying 20 words per minute even though they are capable of handling 30 words per minute of perfect code.

The importance of spaces and the application of ICs has been recognized by others and many fine articles have been published (see references). The electronic keyer with its supervised dots and dashes has improved CW communications in recent years. However, proper operation of a keyer takes a certain amount of musical skill which many of us do not have. As a result, the average CW QSO is still well below 20 words per minute.

The keyboard encoder offers additional improvement in communications with the CW language. Good commercial equipment is available, but high prices discourage many potential users. Articles on home-brew projects are being published, and any ham who likes to solder (or wire-wrap) can have a keyboard.

My prototype keyboard used TTL and a 9-bit code. I

used a diode matrix to generate a binary code and digital logic to convert it into dots and dashes. The TTL scheme worked fine, but as I was putting on the finishing touches, a regulator in the power supply failed and fried a $17.50 40 x 9 first-in, first-out (FIFO) memory chip. About the same time, K2BLA published a circuit that could be constructed using about $30 worth of parts. Also, WB5IRY wrote about the possibility of TTL becoming obsolete. Both of these writers were generous in their praise for CMOS and emphasized how easy it is to construct a power supply for CMOS. With this motivation, I switched to CMOS and an 8-bit code.

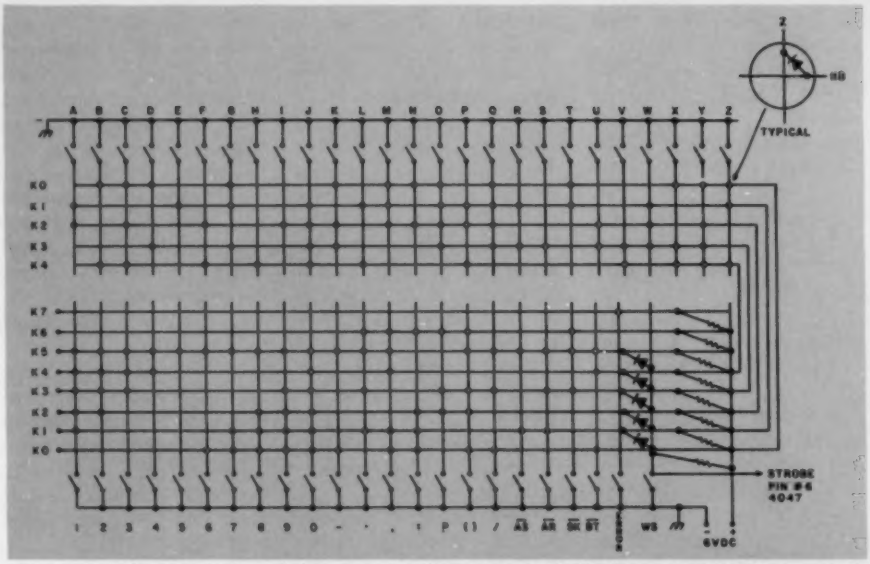

Fig. 1. Diode matrix for alphanumeric characters. All diodes are 1N4814 or equal. Resistors are 10k, ¼ Watt. Switches—typewriter keyboard.

After trying high-frequency keyboard scanning, such as is used by K2BLA and in calculator keyboards, I have decided that diodes are still beautiful (Photo A). They are rugged, cheap ($2.84 for this circuit), and even though 142 diodes have 284 leads, the hookup is so simple that it can be made while the XYL is talking. There are no glitches, and troubleshooting is so easy that it can be done with a VOM.

Considering the possibility that some hams may not be any more advanced in the art of applying ICs than I am, some basic fundamentals about logic devices used in this circuit will be included for convenience. Being an electrical engineer specializing in power, I am more familiar with 500 MCM cables and 10,000 kV-A transformers than I am with the 14- and 16-legged bedbugs normally called ICs. If you happen to be a digital pro, skip a few paragraphs and go directly to the schematics. Before going into the details of how the circuit works, let's review a few basics concerning solid-state devices that are used in the system. Use Fig. 2 for reference.

Flip-flops can be considered remotely controlled switches which have several input control lines. Two 4013 ICs are used. The 4013 is a dual type D flip-flop. Each section has 6 terminals: a data terminal marked D, a clock input marked C, an output marked Q, the complement of the output marked $\overline{Q}$ (pronounced not Q), and set and reset terminals. Data is transferred from the input D to output Q on the positive transition of the clock, provided that both the set and reset pins are low. With a high on the reset pin, the Q output is zero, and the $\overline{Q}$ output is high regardless of clock status.

Those of you who have constructed the "contest keyer" by WA4KUO will recognize the dot-dash generator used in this keyboard. The CMOS 4027 is a dual J-K flip-flop equivalent to the TTL 7473. The J-K flip-flop is similar to the type D flip-flop, except that it has two input terminals labeled J and K. The 4027 also flip-flops on the positive transition of the clock. The J-K flip-flop is useful in this application because, with relatively simple connections, it can be made to toggle with clock transitions.

Logic gates OR, AND, NOR, and NAND behave just as their names would suggest. OR gates and AND gates have two or more inputs and normally have only one output. In the case of an OR gate, a high on any input terminal will produce a high at the output terminal. With the AND gate, all of the input terminals must be high in order to obtain an output. Then, with the NOR and the NAND, the operation is simply reversed.

The inverter is another useful logical device. It has one output and one input, and they always complement each other. The 4049 has six inverters in one chip.

Two 40105 4-bit chips are used to make up an 8-bit first-in, first-out (FIFO) memory. This provides 8 input data terminals and 8 output terminals. A binary code word of 8 digits is loaded into the FIFO each time that the strobe pin receives a positive pulse. The array will hold 16 words. Within a few nanoseconds after loading, code words bubble through the memory and queue up in order at the output terminals. When the output data is stable, a *data out ready* (DOR) flag goes high. Binary words can be clocked out of the memory by applying a negative-going pulse to the shift-out (SO) terminals. Loading is completely independent of the output. By using the FIFO as a buffer between the input keyboard and the reading logic, the operator is free to type at any speed. If he types below the output clock speed, the output will follow the hesitating typing strokes. If the operator types faster then the clock speed, output will be a smooth continuous stream. Of course, since the memory will only hold 16 binary words, the operator cannot go more than 16 letters ahead of the reading logic or some of the characters will be lost.

Two 4035 chips are used to make an 8-bit shift register which also has 8 input and 8 output terminals. The shift register operates in the parallel mode as well

as in the serial mode. With the parallel/series (P/S) control high, 8-bit words are parallel loaded into the register clock. Data at inputs are transferred to the outputs each time the clock is pulsed. With the P/S control low, digits are shifted serially toward the right with each positive-going clock transition. The shift register is also equipped with a truth/complement (T/C) control so that an inverted output can be obtained. That is, all of the outputs will be exactly opposite to the corresponding inputs. Thus, if the serial input terminals (J-K) are made permanently high, zeros will be clocked into the shift-register output. These zeros migrate toward the final output terminal with each positive-going clock pulse.

Binary-coded words are generated for each letter in the alphabet and special characters by a diode matrix in the keyboard. The circuit is simple, and examination of Fig. 1 will show that it is only the Morse code with a marker bit added to mark the end of the character. Once you recognize the pattern, assuming that you know the Morse code, you can wire up the matrix without referring to a diagram.

The buses K0-K7 are energized through 10k, ¼-Watt resistors from the positive terminal of the power supply. Keyboard keys ground out selected bits of the K0-K7 buses through diodes to form the 8-bit code words required for each character. As an example, the letter "A" would have the code word 00000110. Recall that the shift register inverts all digits. The inverted digits correspond to K7, K6, K5, K4, K3, K2, K1, K0, respectively.

In the Morse code, there are more dots than there are dashes; therefore, in order to minimize the number of diodes, one diode is used to generate each dash. Read the code word from right to left: "Dit, dah, marker." Meaningful digits are followed by a string of filler zeros.

For a closer look at the system, refer to Figs. 2 and 3 which show the general schematic and its companion timing diagram. The diagram assumes that the operator has turned on power and set the master clock to operate at a selected speed. At some random time later, he has typed the letters "AE" followed by a word space, then the letter "T" at a speed greater than the corresponding clock speed. After power has been turned on, the master clock runs at a frequency set by the operator. The instant that a key is struck is a random event with respect to the clock output. The FIFO is very fast and responds within nanoseconds after the operator strikes a key on the keyboard. The code words (one 8-bit word for each character) bubble through to the output terminals of the FIFO, queuing up in order. As soon as data is stable, the data out ready (DOR) goes high. Since there are two FIFO chips involved, the two DOR signals are combined by AND gate U8D into a single signal. This high passes through OR gate U7C and on the next positive transition of the master clock output causes U12B to flip, thereby starting the dot generator in synchronism with the master clock. (I learned the hard way that this flip-flop 12B was needed. Without it, sometimes the first syllable of a letter would be cut short or missed completely. The addition of the 12th IC had a bonus. The "Q" of 12B gives a signal to provide automatic receive/transmit switching.)

The dot generator, U6A, is clocked by divide-by-2 flip-flop U12A, which runs at one-half clock frequency. The combination of U12A and U12B ensures that the dots will have the

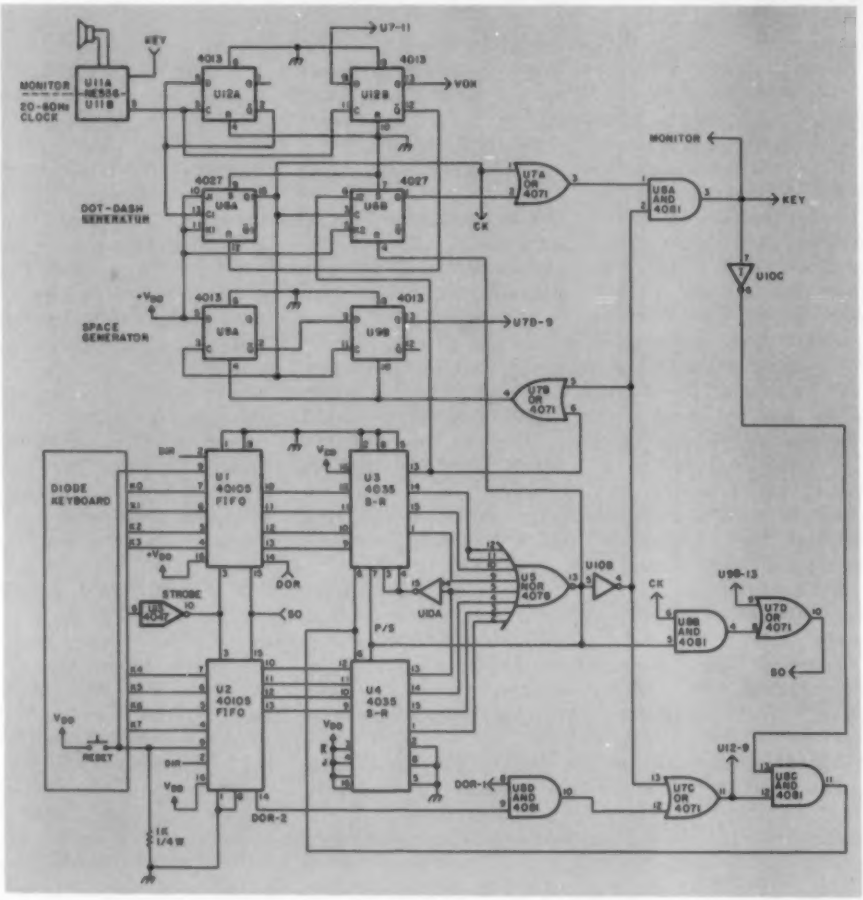

Fig. 2. CMOS Morse encoder schematic. U1, U2—40105 FIFO. U3, U4—4035 shift register. U5—4078 8-input NOR gate. U6—4027 dual J-K flip-flop. U7—4017 quad OR gate. U8—4081 quad AND gate. U9, U12—4013 dual type D flip-flop. U10—hex inverter. U11—NE556 dual timer. U13—4047 one-shot. Refer to spec sheets for power connections.

proper phase relationship with respect to the random loading of the FIFO.

Observe that the positive transition from DOR is passed through AND gate U8C to provide a positive-going clock pulse to clock the shift registers via pins 6-6. This causes the parallel-load feature to function because terminals 7-7 of the shift registers are already high (parallel mode) since at the time of starting, the outputs of the shift registers were all zero. Therefore, NOR gate U5 would have a high output.

Remember that the dot generator runs continuously once it is turned on by the synchronizer flip-flop. Each dot represents one time unit. This is also the fundamental time unit for dashes and spaces. The "CK" clock signal is generated by U6A, which is shown as line 6 of the timing diagram, Fig. 3. When required, U5 and U10B will silence the key by controlling pin 2 of AND gate U8A. Flip-flop U6B goes into operation any time that a dash is required. Examination of the timing diagram will show that both the dot generator and the dash generator are divide-by-2 counters. The OR gate, U7A, combines these outputs to produce a dash whenever U6B is active. Flip-flop U6B is turned off and on by commands from pin 13 of U3.

In the case of the letter "A", the first digit presented to terminal 13 is a zero. Consequently, the dash generator is restrained because there is a zero on the "J" input of U6B. Pin 2 of AND gate U8A is high because the signal from inverter U10B is the complement of NOR gate U5 output and all characters (except the word space) will have at least one "high" at the inputs of U5. The dot generated by U6A will be passed on to the keying circuit through gates U7A and U8A. On the falling edge of the dot, the shift registers see a positive-going pulse on terminals 6-6 through AND gate U8C after it is inverted by U10C. This clocks the shift register one position to the right. Note that the shift register is in the serial mode because of the low on P/S. The next digit at terminal 13 of U3 is a one, representing the dash of the "A". This activates dash generator U6B, causing a dash to be dispatched. (See lines 6, 7, and 8 of Fig. 3.) On the falling edge of the dash, the shift register is pulsed again and another high moves to terminal 13 of U3. At this instant, all of the inputs to NOR gate 5 are low. This makes U5 output high and silences the key by causing pin 2 at U8A to be low. U5 output also resets dash generator U6B, changes the signal on P/S from high to low in preparation for a new character, and, at the same time, AND gate U8B is set up so that it will pass the next pulse from the dot generator.

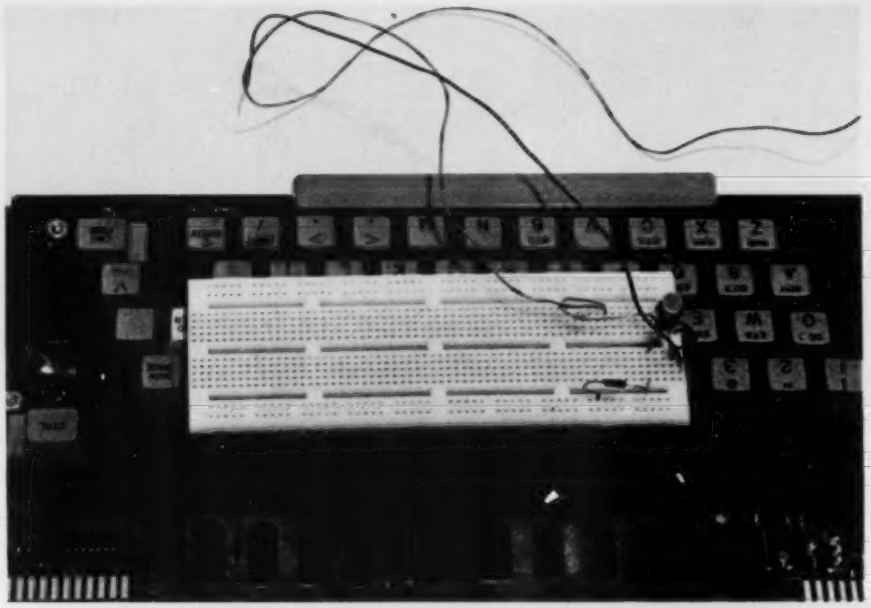

Photo B. A surplus NPN transistor, two current-limiting resistors, and an LED make a breadboard logic probe to debug circuit. Discrete components (lower right) are used for the clock and sidetone monitor.

The key is silent because of the low on pin 2 of U8A. The next pulse from the dot generator (see line 6, Fig. 3) is passed through U7D to shift out the next character. On the falling edge of the SO pulse, the FIFO dumps the old character and replaces it with a new one. During the dumping process, the DOR flag dips momentarily. This logic function is internal to the FIFO and the pulse is of only a few nanoseconds duration. (This is the only pulse in the system that is too short to be seen with a simple LED logic probe.) The short pulse is used to clock the shift register and parallel load the new character via gates U7C and U8C. This is more easily understood by referring to lines 13-15 of Fig. 3. This pulse is not to scale but illustrates the phase relationships. The process of dumping the old character and loading a new letter into the shift register has had the effect of silencing one dot. The dot requires one time unit; this, with the intervening spaces on either side, makes a total of 3, as is required by exact code for the inter-letter space. Some keyboards silence a "T", but this is not precise code because the "T" is 3 time units long, which, when added to the two intervening space units, totals 5 time units.

To continue the example, the letter "E" is dispatched next. Action would be similar to that described for the "A". The main difference is that following the "E" there is a word space. The code word for a word space is 00000000. With this code word loaded into the shift register, the key is silenced, as was the case with the inter-letter space, but pin 13 of U3 is also zero and this drops the reset signal of the space generator on U9. This is a mini shift register which counts the word space. Refer to the timing diagram and note that it has the effect of silencing a total of three dots. These dots plus the four intervening spaces total 7, as Mr. Morse specified for the word space.

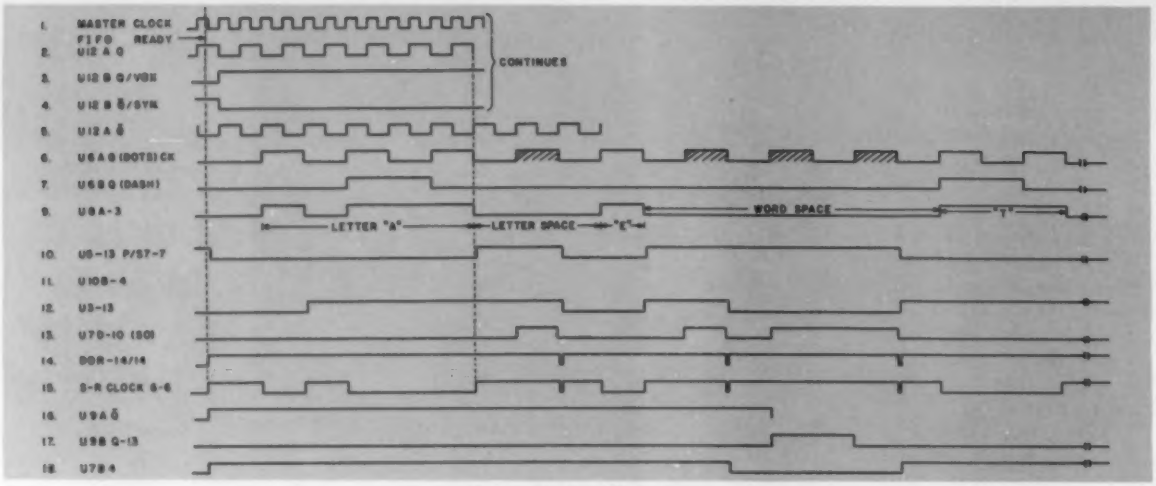

Fig. 3. Timing diagram.

The timing diagram shows the remaining letter "T" of the example. This is for illustration only and will not be described.

Circuit details for the sidetone oscillator, master clock, and the strobe have not been shown on the schematic because these are readily available from a number of existing publications. Manufacturers will supply chip specification sheets with this information.

The master clock and the sidetone oscillator (U11) are made from an NE556, which is simply two 555 timers in a single DIP package. A variety of capacitors and resistors are suitable. Just follow the graphs in the specification sheets. The master clock should have its frequency adjustable between 20 and 60 Hz for a speed range of about 5 to 50 wpm.

The sidetone oscillator can be made variable if desired. I used a fixed tone of about 440 Hz, which is the musical note "A". My rig has a sidetone oscillator, so I installed a switch to silence the monitor speaker while on the air. When not used for communications, the keyboard makes an excellent code teaching aid.

An additional switch can be installed to have a "send-store" feature. By stopping the master clock, the FIFO can be preloaded. A storage of sixteen characters is too short for anything more than a CQ. However, for those who would choose to have a longer message, the Fairchild FIFO 3351 is an excellent choice and holds 40 characters. One 3351 can be substituted for the two 40105 4-bit chips. Additional 40105 chips can also be cascaded to provide more storage.

A master reset button is needed for the FIFOs. Just after power up, random noise is loaded into the FIFOs, and, unless the M-R button is used, you will have a hard time recognizing the language that will be dispatched.

The choice of power supplies is almost unlimited. The CMOS and the NE556 can use anything between 5 and 15 volts. On my keyboard, I used a 50¢ surplus 6-volt, 200 mA calculator adapter. In order to improve the tone of the monitor, I did add a 25¢ electrolytic capacitor and a couple of resistors to provide filtering. To my surprise, even unfiltered full-wave dc can be used for the CMOS and still work. It must be that some of the claims about noise immunity by CMOS are valid.

As the numbering might suggest, U13 is an afterthought. At first I was determined to make a one-shot from the spare inverter gates in U10. According to RCA's ICAN 6267, three inverter gates will make a one-shot. The circuit worked most of the time, but occasionally a double pulse would be triggered, causing two letters to be loaded for one key stroke. I took the easy way out and cook-booked a 4047 one-shot and selected a capacitor/resistor combination to make a 2 millisecond pulse. This is a very versatile chip and does a good job of debouncing; it interlocks the keys so that only one letter will be dispatched even though two keys are struck simultaneously. This circuit will ignore all other strokes until keys are completely released.

The one-shot strobe (4047) is triggered by "wire-ORing" through diodes. The lower right of Fig. 1 shows this circuit. Note tht only buses K1, K2, K3, K4, and K5 are monitored. This is sufficient to cover all characters except the word space. A separate switch is used for the word space. The 4047 is connected to fire on a negative-going pulse which is obtained through 2 diodes in series for the normal characters and through a switch for the word space.

Experience with my Swan 700 CX has taught me that it eats expensive PNP transistors like a feathered swan eats corn. I took the coward's approach and used relays for both the VOX and key functions. This works very well except that if someday I am to give the "bionic brass pounder," WB2ZDF, his 1000 wpm, I may be forced to use a transistor. Is he kidding about 1000 wpm? Maybe not, or at least something that will approach that figure. Although no one can type 1000 wpm, a RAM can be interfaced in between the keyboard and the FIFOs to provide burst sending. Then, with the video readers, very high speed should be possible. This raises an interesting question. If TTL is on the verge of obsolescence, how about the RTTY bandwidth hog?

Parts for the final circuit cost about $40 (this does not include parts invested in the prototype which have been returned to the junk box). It does include

$10 for a surplus computer keyboard. This keyboard had good quality reed switches and a fiberglass PC board. None of the circuits on the PC board were salvaged but were removed from the old fiberglass board by using a wide-flame burner on a propane torch and a wood chisel. Holes for the diodes and the ICs were quickly drilled by using a standard piece of perforated board as a template and a Dremel tool. Interconnections were made with point-to-point wiring using standard wire-wrap wire. I use solder-tail sockets rather than conventional wire-wrap sockets because the long pins give my bifocals fits. A wire-wrap tool conveniently fastens connections to the solder-tail pins of the sockets and these can be quickly secured with a small dab of solder. This approach was used for all chips except No. 13. I ran out of sockets, so I simply wired this rascal in place. It worked so well that on the next circuit I build, I will not waste time with the sockets except for the two FIFOs. These are needed to provide a quick disconnect to simplify wire checking.

With 13 ICs, one can expect to make a few wiring errors. These can be readily detected by using a simple homemade logic probe that will cost less than $1.00. My breadboard probe is shown in Photo B parked on top of the keyboard. It is simply an LED driven by a small surplus NPN transistor with a length of No. 22 wire as a probe. By setting the clock at 5 wpm, the waveforms shown in Fig. 3 can be observed by simply watching the LED and counting flashes.

Should you decide to build a keyboard, be sure you understand the timing diagram. It is the key to troubleshooting. Also, recheck pin numbers against the IC manufacturer's specification sheet. Standardization is good, but there are some variations and it is possible that a typographical error exists. However, the diagram has been checked and rechecked to prevent the latter possibility.

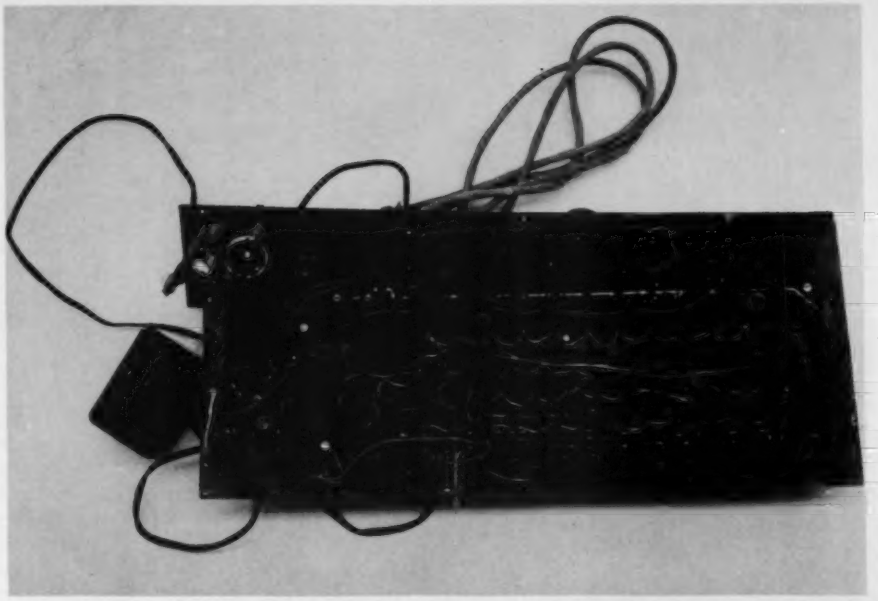

Photo C. This photo shows point-to-point wiring using wire-wrap wire for ICs and #22 telephone wire for keys and diode matrix buses.

The error signal has 8 time units; thus, it can be used as an aid in calibration: wpm = 192/T, where T = seconds (stopwatch) required to send 10 error signals.

A case was constructed from standard heating and ventilating sheet metal. While this is not as beautiful as some store-bought equipment, it is adequate.

If you are still not convinced that diodes are beautiful, you can use an ASCII keyboard, or, for that matter, any keyboard with an oddball code, as long as it does not exceed 8 bits. You can even use your home computer. An EPROM

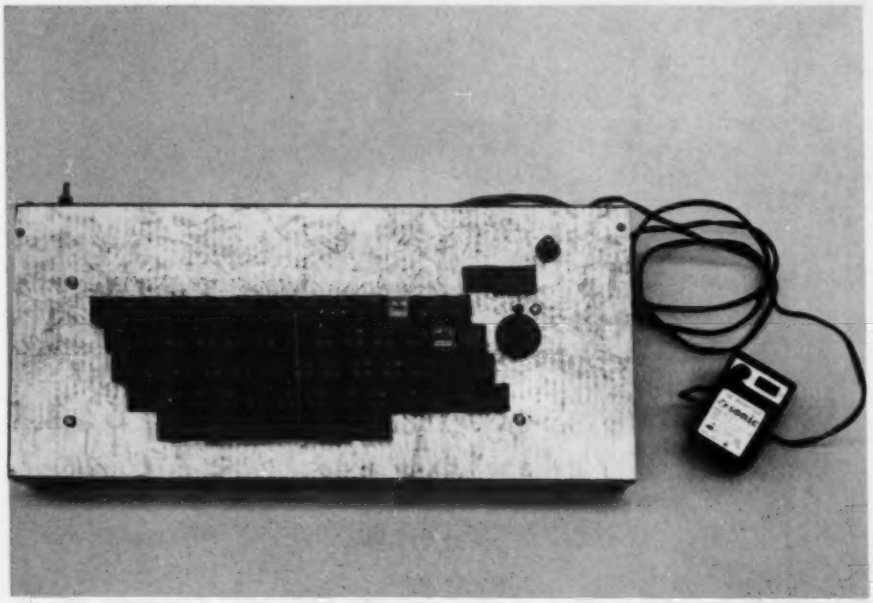

Photo D. Finished keyboard with surplus calculator power supply at right.

can be used to interface between the keyboard and the FIFOs.

In addition to all of the hams mentioned in the text and the references, I am indebted to the sales reps and tech-service engineers of both RCA and Fairchild. They patiently answered my numerous and sometimes frivolous questions. They not only made it possible for me to build a keyboard, but also helped me in my job as a power engineer to apply integrated circuits to industrial applications.

After a 30-year recess in radio, my straight-key sending was even worse than it was during World War II when I frequently would be interrogated with "INT LF" (modern translation, QLF?). Now, with my keyboard, I, too, can make good CW music and the high-speed boys will talk to me. Perhaps after a few more keyboards are on the air, the average QSO can be raised to 30 wpm. ■

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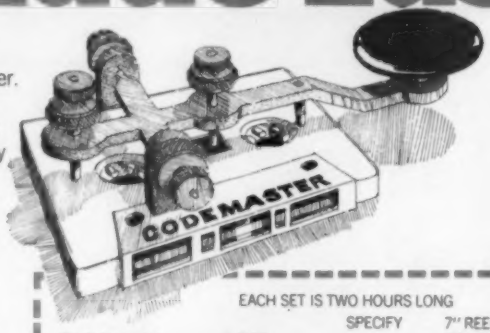

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In most receivers, the groundwork has already been laid.

Many hams copy CW by using an SSB receiver with an outboard CW filter consisting of 88-mH toroids or active filters, to obtain very narrow bandwidths and a beat note of about 1000 Hertz. Some have found that a couple of hours of this type of operating will bring on something resembling a migraine headache and a strong desire to go work SSB up the band.

A lower beat note and a bandwidth of a few hundred Hertz appear to alleviate CW fatigue. The lower tone is softer to the ear and a somewhat wider bandwidth allows the signal to be moved around slightly in the passband, which helps to avoid monotony.

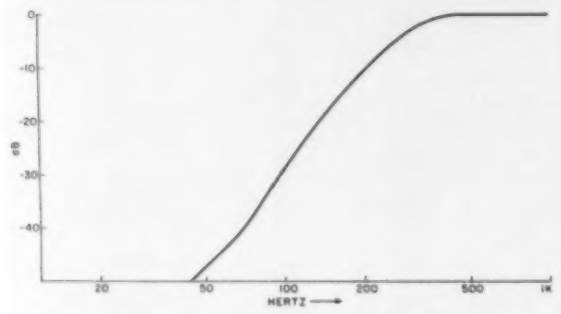

Fig. 1. Low frequency response of typical receiver.

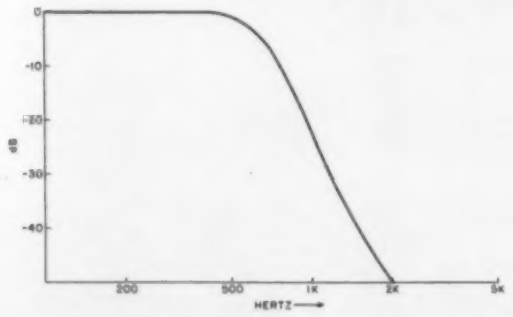

Fig. 3. Low-pass filter frequency response.

One advantage of this approach is that one side of the needed filter response is already there in most receivers. The low frequency side of a typical communications receiver might appear as in Fig. 1. The audio section is designed to attenuate the very low audio frequencies, usually with the 3-dB point around 300 Hertz.

This allows you to build a simple, low-pass filter to get the desired attenuation on the high-frequency side. The filter is shown in Fig. 2. The .176-H inductors are made from two 88-mH toroids connected in series. It plugs into the speaker output, requires no power, uses common components, and will fit easily inside a small minibox. Its response is shown in Fig. 3.

Combined response is shown in Fig. 4. Bandwidth is about 300 Hertz at the 3-dB points, allowing for some variation of tone (and drift). There appears to be less ringing with this approach, as compared with one narrow filter.

This filter may solve your headache. See you on the low end, OM.■

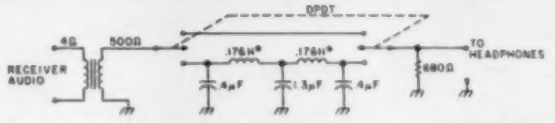

*Fig. 2. Low-pass filter schematic diagram. * = 2 88 mH in series.*

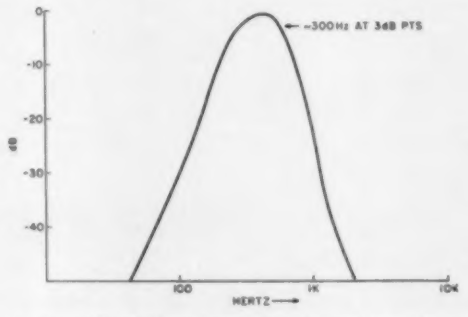

Fig. 4. Combined low-pass filter/receiver frequency response.

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An 8080 Repeater Control System

— part I: an overview

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When told I was going to install a microprocessor on our repeater as the controlling element, some felt, "A microprocessor on the repeater—what for?" After explaining that I would not add anything as complex as a microcomputer to the repeater unless there was good reason to do so, there was no vocal opposition. I suspect that it was not until the control system was placed into operation that everyone became in favor of it. The reason I mention these facts immediately is that a quick first impression of the control system could very well be that the system is too complicated for the resultant benefits. In fact, the opposite is true. The system is indeed much more complicated than what is normally encountered in similar applications. However, the operations it can perform are much greater than would be found were the benefits only proportionate to the system complexity. With an intelligent controller, functions can be done which could not possibly be done otherwise with a reasonable amount of hardware.

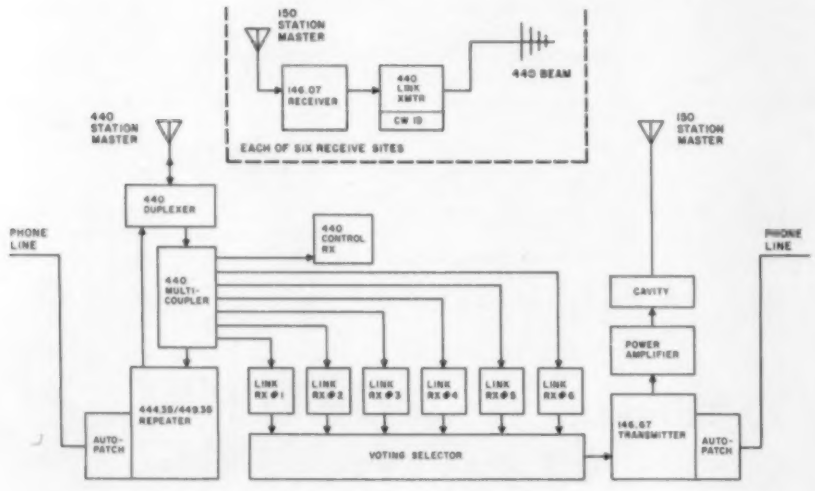
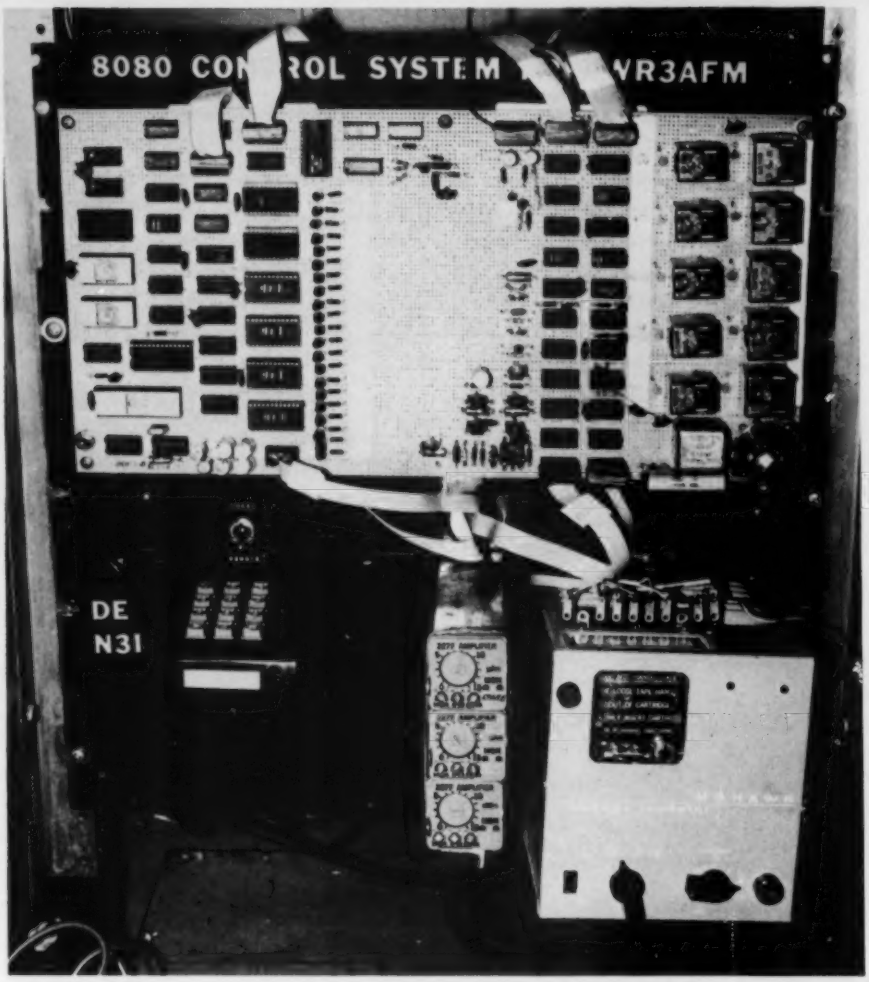


Fig. 1. WR3AFM equipment.

Originally, the major function of the control system, and the reason for implementation with a microprocessor, was to provide many on/off output lines controllable through multiple digit decoding of touchtone™ signals. The existing system, consisting mostly of relays, was capable of at

most six functions. We required several dozen functions, and simple expansion of the relay system would have made the repeater look and sound like a telephone company central office. After the new system was finished, the simple output functions took a back seat to the innovations which were not possible before.

In order to understand what the 8080 control system does, a brief description of the Baltimore Amateur Radio Club's repeater (WR3AFM) is necessary. Fig. 1 shows a block diagram of the repeater. There are actually two repeaters: a two meter repeater and a 440 MHz repeater. The 440 repeater is a simple duplexed one. It has an autopatch independent of the rest of the system. The two meter repeater is a multiple split site repeater. The two meter transmitter is located at the site of the 440 repeater. Spread around the city are up to six receive sites. Each receive site receives signals on the two meter input frequency and retransmits them on a 440 link frequency to the transmitter site. At the transmit site, signals are received from each of the links. Each link receiver feeds a voting selector, which continuously evaluates the signal-to-noise ratio of each signal and passes the best one on to the transmitter. The two meter repeater also has an autopatch. The repeaters can be controlled via the two meter repeater autopatch telephone line or a 440 receiver reserved for control. All told, there are eight 440 receivers; off the receive port of the 440 duplexer is a 440 multicoupler which splits and boosts the signals received from the 440 repeater antenna. As can be seen, we obtain maximum utilization (eight receivers and one transmitter) from the 440 antenna on the top of the tower (400 feet high)!



Control system connected to repeater.

The voting selector can be directed to pass only one of its inputs to the transmitter, or to ignore some of its input receivers. This is a major function of the control system. As our repeater gradually expanded, it became more difficult to diagnose problems. A week would go by before we even realized that one of the receive sites was inoperative. With the new system, it is easy to check all sites by commanding the voter to pass each receiver one at a time. During the summer months, we are plagued with skip signals from users of the two nearest repeaters on the same frequency: Hazelton PA and Trenton NJ. At times, our repeater is unusable due to constantly timing out from the extraneous signals. We can now command the voter to ignore our northeastern receiver, from which most of the interference arrives. These two basic functions provided the impetus for the construction of the 8080 system.

The system has other important functions. It allows the two meter and 440 repeaters to be linked when needed. A prerecorded tape loop can be activated on request, giving information about the repeater and the club. A feature is provided to test touchtone pads—the repeater tells the user in Morse code what it received. The processor controls the autopatch. Instead of the normal system, it gets the requested telephone number from the user and redials the number into the telephone system. If the proper number of digits is not received, it will not even access the telephone line. Single-digit codes permit dialing of emergency numbers. Non-collect toll calls are impossible. There

Using the System

The following text, after suitable modifications, is intended to be distributed to users of repeater systems using the 8080 control system. Use of the processor functions and the autopatch are described.

WR3AFM is now controlled by an 8080 microprocessor. The processor permits flexibility in the system as well as many functions which could not reasonably be implemented without a processor. There are five CW IDs; four are permanently stored, and one is remotely programmable via a touchtone pad. Any of the five IDs may be selected, or, as is often the case, the different IDs may be made to cycle. The programmable ID allows meeting announcements and anything else that could be useful to be placed on the repeater.

For testing and diagnosis, each of the individual receive sites on 07/67 may be either disabled or forced on through the voting selector. There are several modes of accessing the control system, so it is possible for control stations to work on the system without interfering with repeater users. For most functions, the 8080 responds to correct commands with an "R" in CW, so when "R"s are heard on 67 this means that someone is commanding it. Under such circumstances, be slow to pick up transmissions in case the control operator has any requests; if none are made, feel free to continue using the repeater and ignore the "R"s.

For those interested in the size of the 8080 system, it currently has about 2K of program in ROM, 256 bytes of RAM, seven eight-bit output ports, and three eight-bit input ports. The control program is about 1300 lines long, and the hardware consists of 57 integrated circuits.

The processor makes possible the redialing of telephone numbers, the virtual elimination of incorrect dialing for autopatches, and the prevention of toll-charge telephone calls. In addition to the control functions and the autopatch, the processor has five codes available for general use which are accessible via 146.07. Any ideas for additional functions will certainly be entertained. For each of the codes, it is necessary for the first digit to be held at least one full second. It doesn't hurt to hold any tone longer than required. With this in mind, here are the various codes:

1#1—Links the 146.07/146.67 repeater with the 444.35/449.35 repeater. The repeater answers with an "R" if the function is accepted. The linkup will remain up indefinitely until knocked down with a *. Signals on 146.07 will come out on both repeaters, and signals on 444.35 will come out on both repeaters. When disconnected, the repeater responds with an "R" as well. The intention of this function is for calling someone on the other repeater, not for extended rag chewing on both repeaters simultaneously. When transmitting on 444.35, 1#1 will also link up the repeaters. This function on the 440 end is not controlled by the microprocessor, and it does not acknowledge with an "R". The * on 444.35 will kill the linkup if it was initiated on 444.35; alternatively, on the 440 end the linkup will time out after three minutes. This is only true for linkups made from the 440 repeater. The two linkups are separate; if linked on 146.07 they must be killed on that frequency, and if linked on 444.35 they must be killed on that frequency.

2#2—Initiates a prerecorded tape message giving information about the repeater. The tape will disable itself upon completion.

3#3—Disables the blocking of touchtones. Any tones sent after the 3#3 before the carrier is dropped will not be blocked. Normally, upon recognition of valid tones, the repeater mutes them. This is done to protect the ears of those of us who monitor often. It is done on a tone-by-tone basis to facilitate diagnosing problems, since you can hear a short blip for every digit and can tell how many tones were sent. For those hams with selective call decoders, it is necessary for the tones to pass unimpeded, which is the reason for this function. If only short tones are required, the selective call function need not be used, as the repeater does not initiate tone blocking until a valid tone of about one second is received. This is to prevent blocking of voices.

4#4—Touchtone test. Any digits sent after the 4#4 before the carrier is dropped will be sent in Morse to tell the user what the repeater decoded the digits as. Any sequence up to 24 digits can be accommodated.

5#5—If preceded by a 4#4 test, will repeat what the 4#4 sent. If preceded by an autopatch, the telephone number entered will be sent in Morse. If an autopatch attempt fails, 5#5 will show what the number requested was (if the autopatch code was accepted). If, after making an autopatch, you wish to clear your telephone number from the machine, simply do a 4#4.

NOTE: The functions 1#1 through 5#5 are intended for use by anyone, club member or not. The autopatch is restricted to club members and transients. When performing any of these commands, be certain to identify your station first. The functions are there to be used, but not abused. This is somewhat of an experiment in the hope that our repeater users will use these functions wisely. We hope to be able to continue this free access. Should it become necessary, any of the functions may be disabled by remote control. Please do not force us to deactivate them.

are several different CW identifications which may be selected, and special IDs can be loaded in minutes remotely. For a number of years, we have had a reprogrammable CW identifier (*73 Magazine*, April, 1976). It was a great success, and the ability to program an ID remotely makes it more useful. Any of the functions can be disabled, and, of course, the repeaters can be turned off if necessary. A complete explanation of the user codes appears elsewhere in this article. A sample of what can be placed on the tape message loop is given. A complete description of the control functions, "Controlling the System," also appears elsewhere. It is more difficult to control the system than with a simple arrangement, but many times it is not even necessary to enter the control mode and forcefully disable functions. Merely by transmitting on the control frequency, everyone else loses access to the touchtone decoder. This is of great use when some user decides that he will execute some function without identifying himself, as required by FCC regulations. A simple transmission on the control frequency removes his access to the system, and it is not even obvious to those listening. With any amount of luck, these individuals adjust their touchtone pads attempting to bring up a function and throw their pads away in disgust after being unsuccessful.

We have been quite pleased with the overall operation of the control system. The user codes have given the repeater users some involvement with the repeater, and, after the initial adaptation period, general user sentiment has been quite positive. Although the control system is fairly complex, the reliability so far has been good. In the first two months of operation, the system crashed twice. In the software world, a computer "crash" refers to the occurrence of some error which causes a computer to ignore operator commands, necessitating a hardware restart. I added an error detection/recovery routine to the system, and there have been no crashes since. There have been no hardware failures.

In the following sections, I will show how you can duplicate the system, how the hardware and software functions are distributed, what the hardware components are, and provide explanations of how to use and control the

Autopatch Access Procedure

The following procedure is recommended for accessing the autopatch.

1) "N3ABC autopatch"
2) Send the autopatch code and the telephone number in one transmission. Remember to hold the first tone one second. It is imperative that the carrier continue throughout the entire operation of all ten digits. Upon the release of carrier, the repeater will determine if your number is valid. The number is valid if any one of the following conditions is met: exactly one digit which corresponds to a single digit emergency number; exactly seven digits, the first digit not a 1; exactly eight digits, the first number a 0; exactly eleven digits, the first number a 0. If the number is invalid, nothing will happen. It will act as though no autopatch code had been entered, and it is not necessary to send the knockdown digit. If the number is valid, the repeater will bring up the telephone line and redial your number.
3) After the number has been dialed, and the line has clicked over, "N3ABC".
4) Conversation
5) "N3ABC clear with John Doe at 12:37 PM on August 12."
6) Knockdown code. If the "beep" is heard, the patch has been killed.
7) "WR3AFM this is N3ABC clear."

If you have problems, remember the 5#5 code.

The repeater now has several single-digit special numbers. Make a note of these special codes:

2—Baltimore City Police
3—Baltimore City Transit and Traffic
4—Maryland State Police
5—Harbor Tunnel Information
6—Anne Arundel County Police
7—Coast Guard Search and Rescue
8—Baltimore County Police
9—Howard County Police

To use the single digit codes, send the autopatch code followed immediately by the single digit. The repeater will dial the proper number for you.

Half Duplex

The autopatch is half-duplex. This means that the audio from the telephone line is switched off when you push the PTT. This feature can be used to block obscene language, business communication, or whatever, if the called party gets carried away. However, "skip" or interfering signals also have the same effect. Therefore, it is not wise to initiate an autopatch under such conditions. If this problem occurs, remember that the party on the telephone can hear you perfectly—it is just that you cannot hear him whenever any signal is present on 146.07, be it yours or something else.

Autopatch Timer

The autopatch is to be used for short traffic only. A timer will automatically terminate the patch after three minutes. Once activated, the patch will stay up until terminated by the timer or the knockdown code. No kerchunking is needed to keep it up. Three minutes is more than adequate for most autopatches. However, sometimes when in communication with police regarding an emergency it is desirable to continue the autopatch past the three-minute limit. Because of this, the timer is automatically deactivated when a *single digit* emergency number is used. The patch will not time out for these calls. For normal calls, it is not possible to extend the three-minute limit. For all calls, think of what to say before calling.

Tape Message Text
(Time: 2 minutes, 50 seconds)

Welcome to the Baltimore Amateur Radio Club's 07/67 repeater, WR3AFM. The transmitter is located at the old WBAL tower on Park Heights Ave., and drives a 250-Watt amplifier, though only a portion of that power reaches the antenna through about 500 feet of feedline. The repeater has receivers north of the beltway on Old Harford Road, at the WRBS tower near I-95 south and the beltway, downtown at 4000 North Charles Street, and at the QTH of K3VC and N3JC at the top of the Jones Falls Expressway. Each of these receivers drives a 440-MHz link transmitter. At the transmit site, there is a link receiver for each receive site. Each signal is fed to a voting selector, which continuously evaluates the signal-to-noise ratio of each receiver, the best of which goes to the transmitter. All of the repeater equipment is of the General Electric MASTR make.

At the transmit site, there is also a duplexed 440-MHz repeater, 444.35 in and 449.35 out.

You will note that a short click is heard after releasing your carrier. This signifies that the repeater timer has been reset, and leaves time for breakers. It is not necessary to let the repeater carrier drop. 07/67 has an autopatch, limited to travelers and club members, but open to anyone for emergency traffic.

The repeater is set up to block touchtone signals. After a long first tone of about one second, any further tones will be blocked from repeating, and only a short blip will be heard. There are several codes that anyone is welcome to use. One pound one links the 67 machine with the 440 repeater. To acknowledge that function, the repeater sends an "R" in Morse. The repeaters remain linked until a star is sent, again acknowledged with an "R". We do not desire to use this function for more than a calling mode. Two pound two gives this recorded message. Three pound three will disable the repeater's blocking function until the carrier is dropped, permitting the tones to be repeated. Any touchtone digits sent after four pound four will be verified in Morse after the carrier drop. Five pound five will repeat what was sent during a four pound four operation or the telephone number dialed during an autopatch, whichever was last.

The control system for the repeaters is an 8080-based microprocessor, which performs the various functions including multiple identifications, as well as redials telephone numbers for the autopatch.

The Baltimore Amateur Radio Club has another two meter repeater, 34/94, which is a duplexed repeater in the Towson area. We hope you enjoy the use of our repeaters, and would like to see you at our meetings on the first and third Wednesdays of the month at the Ames Methodist Church in Pikesville at 8:00 pm. Listen for interesting bulletins weekdays on 67 at 7:30 am and rebroadcast on 94 at 6:00 pm. Code practice can be heard Mondays at 9:00 pm on 34/94. Should you desire to contact the club, write the Baltimore Amateur Radio Club, PO Box 5344, Baltimore MD 21209.

system. The method of construction, a detailed circuit and program analysis, and some principles I learned in developing the project will be presented in subsequent parts.

Duplication

The 8080 control system can be duplicated for your repeater with few modifications. The control system supports some features of WR3AFM which may not be of use on an average repeater. If nothing but the basic user codes, the multiple IDs, the autopatch functions, and on/off control for a simple repeater is needed, the 8080 control system would still be worthwhile to construct. If the system is totally duplicated, and portions are left unconnected (due to having no voter, 440 repeater, etc.), the system will operate and leave room for expansion. Alternatively, the appropriate pieces could be left out easily. In either case, the program would remain the same. It may have codes which do nothing or do something different, but the program is the major work and is already done for you. If no changes are contemplated for the program, then it is not necessary to understand how it works. It is always informative to do so, but don't worry about it too much if you are not familiar with 8080 machine language. For those who wish to personalize the software, it can certainly

Controlling the System

The following text is intended for distribution to control operators of repeater systems utilizing the 8080 control system. The necessary codes will have to be changed.

The microprocessor control system is a complex but flexible and powerful system. It is of utmost importance to completely understand its operation before attempting to utilize it. Although at first the system may seem to be overly complicated, the structure of the control codes makes it easier to use than a first glance might show.

Basically, the system reads the output of the touchtone decoder to decipher the codes, and has 56 output lines which may be controlled by the proper input combinations. External to the processor itself is additional circuitry to perform the necessary functions, i.e., autopatch, remote base, control frequency repeat, and phone line control. User codes all operate on the outputs indirectly. The proper bits are set and reset to perform the desired function, but control codes are all direct changes of output lines which are assigned to control the various functions.

The basic decoding method used decodes three-digit codes. The first digit of the code must be held down for one second, or nothing will happen. After the release of the first digit, if three seconds elapse before another digit is received, the code will be canceled where it stands. After the release of the second tone, three seconds is likewise allowed to enter the third digit. During the time that the first tone exceeds the one second time period, and until the end of the digit sequence, the blocking relay will follow any valid touchtone signal. During an autopatch or remote base function, the blocking relay will follow the tones as well. At all other times the blocking relay is not activated. Due to this arrangement, in order to have voice signals blocked, the voice must be a valid touchtone signal for one second—certainly a rare if not impossible situation.

Telephone and Control Receiver Access

There are two modes for each of these devices: control and talk. The normal mode for both is control. For the control receiver, this means that the signal is not repeated on 67 but the control receiver grabs the touchtone decoder. The control receiver has highest priority, unless the control receiver touchtone bit is set, which effectively removes the control receiver from the system. If, while transmitting on the control frequency, a # is entered for five seconds, then the control receiver talk mode is entered. While in this mode, the control receiver is repeated on 67. The only way to exit this mode is to send a one-second * while on the control frequency. As long as the control receiver bit is not set, the control receiver always has the decoder. When in the non-talk mode, this allows control of repeater functions without bothering users of the repeater, except that they will not be able to access the touchtone decoder to make autopatches. For the telephone line, when a call-in is made, the mode is set to telephone control. You cannot hear anything. However, the touchtone decoder is listening only to the telephone line. In this manner, control can be exerted in the same way as with the control receiver. If you wish to hear the repeater on the phone line, a five-second # on the line will switch you out of the phone control mode, and the voter audio will be sent down the phone line when an incoming carrier is present. When a signal is present, it has the decoder, not the phone line. Otherwise, the phone line has the decoder. To return to the phone control mode, a * while on the telephone will do so, as will hanging up and redialing. If the telephone touchtone disable bit is set, it will be impossible to enter the phone control mode, and any touchtones received from the phone will be rejected.

Note that any of the three modes of control may be disabled: 150 input, control receiver, and telephone. *Beware:* If all bits are set, you go to the repeater and push the reset button (or wait for a power failure to reset it automatically). Naturally, it would be inconceivable to lock out all modes of control accidentally.

be done. If you do not have any support for the 8080, or for some other reason cannot program 2708 ROMs, I will provide the two ROMs for a cost of $50. Specify your choice for the following codes: 67#, 2*2, 9#5, 6*#, #*6, #48. The knockdown digit will be * unless requested otherwise. Codes may not start with whatever digit is chosen as the knockdown digit. Also specify the four IDs and the telephone numbers for the single-digit dialing. For obvious reasons, the above codes must be changed for each repeater.

This project is by no means a simple one, and it is not suitable for the beginner. Construction experience with integrated circuits and a basic understanding of the system are required. It is not an extremely difficult project as long as care is taken during assembly. Probably the most difficult part will be deciding how to interface a particular repeater to the system. The entire system can be constructed in one week (full-time) by a proficient builder. Do not shy away from the project if you have no prior experience with microprocessors. The "black box" approach is utilized, and detailed knowledge of the inner workings of microprocessors is not required. Total cost for the system is dependent upon how much peripheral equipment is available. The control system cost us about $225, exclusive of the touchtone decoder and pad, amplifiers, and tape loop.

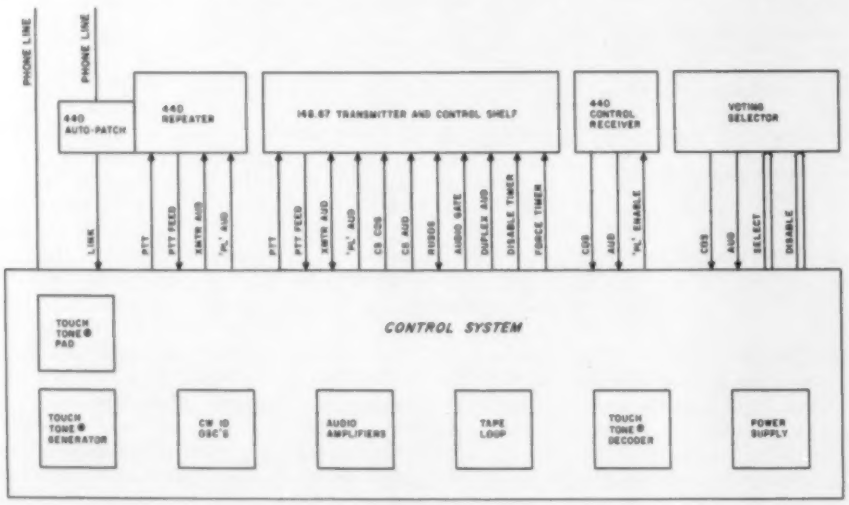


Fig. 2. Repeater/control system interface.

Hardware/Software Balance

Some of the control functions are implemented in software and some are implemented in special

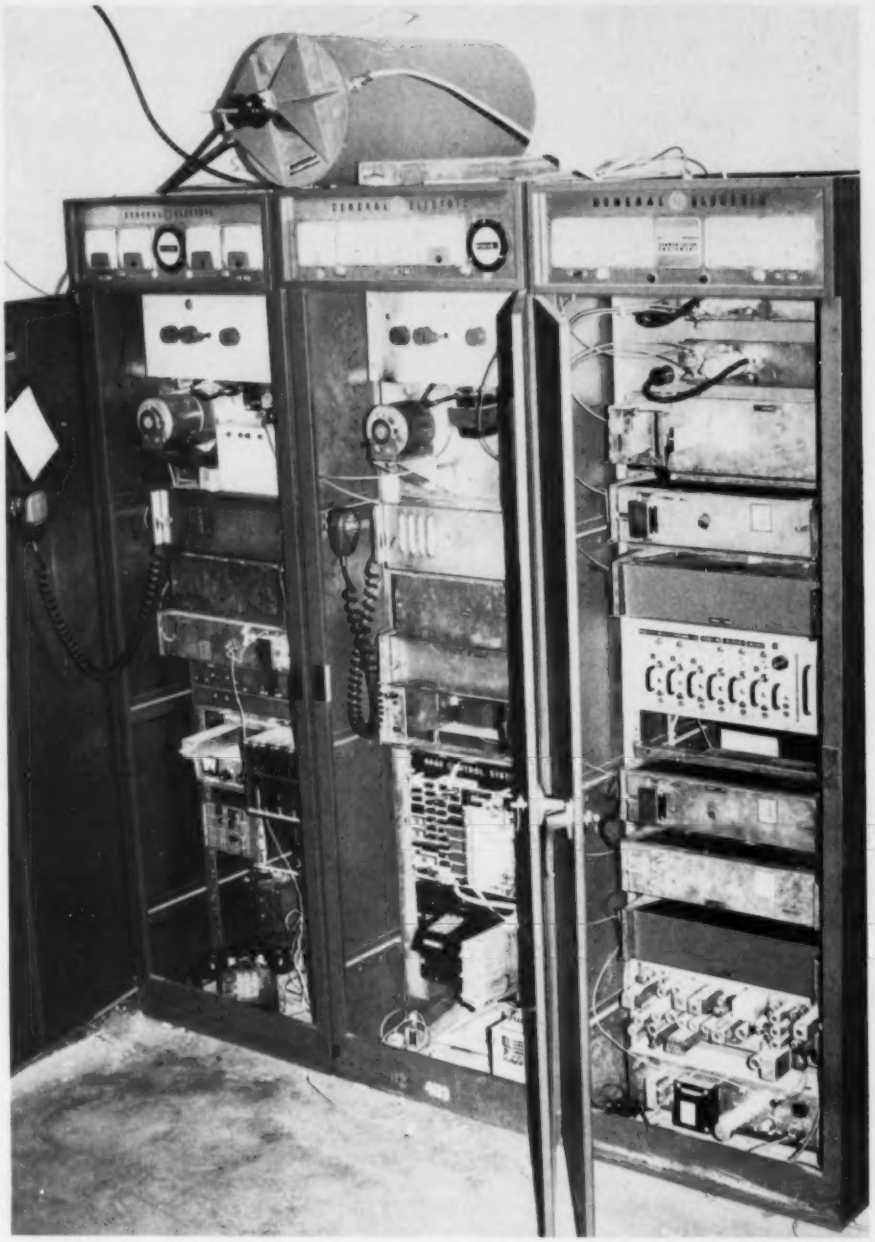
hardware. Deciding where to draw the line is an interesting problem. There are trade-offs which must be made. The major advantage of using a microprocessor is replacing hardware with software, so at first glance it may seem that everything that can be placed into software should be. However, I would rather add one flip-flop than add several hundred extra lines of program. Four years ago, I made the mistake of taking all possible hardware out of a system. My first attempt at computerizing WR3AFM started at that time when I constructed a system based on the 4004 CPU, a 4-bit machine. I designed the hardware, giving the software total control over the hardware. Everything was done with the software. At that time, being hardware oriented, I built the thing first and assumed that I would then write the program. The hardware functioned perfectly—unfortunately, I could not write the program. It could be done, but it was so complicated that it would have taken me several months of concentrated effort to accomplish the task. I effectively junked the project and am still trying to think up some possible use for the thing.

This time around I did not make the same mistake. There are four state flip-flops in the external hardware. These keep track of the autopatch, remote base, control receiver talk, and telephone control states. The processor does not know or need to know the current state to execute its functions. It basically acts as a CW identifier and a multiple digit decoder. It does keep track of many internal states, but these states are not needed until a function is called which needs them. The extra dozen ICs greatly simplify the software, and I believe that the hardware/software balance of this system is near optimal.

Hardware Description

The repeater block diagram shown in Fig. 1 was previously discussed. Fig. 2 shows how the control system interfaces with the repeater. Surely, each repeater will have to be reckoned with on an individual basis. Understanding how WR3AFM works should demonstrate how to interface the control system with any repeater.

The 146.07/146.67 MHz repeater is referred to as 150 and the 444.35/449.35 MHz repeater is referred to as either 440 or 450. The



WR3AFM. Left cabinet—444.35/449.35 repeater. Top to bottom: power amplifier, transmitter, receiver, control panel, autopatch circuitry. Center cabinet—146.67. Top to bottom: power amplifier, transmitter, control receiver, control shelf, 8080 control system. Right cabinet—link cabinet. Top to bottom: 440 multicouplers, power supply for receiver #6, 5 link receivers, voting selector. Tube receiver on bottom no longer in use. 146.67 pass cavity on top. 440 duplexer out of view in left cabinet.

User Codes

There are eight user codes. 1#1 links 67 and 449.35. The two repeaters remain linked until they are unlinked by a single *. The proper output line is automatically set and reset for the link and unlink commands. To tell the user that the link or unlink has been established, the repeater acknowledges with an "R" in Morse.

2#2 plays the prerecorded tape loop. Once it is started, there is no way to stop it short of shutting down the repeater.

3#3 is the disable blocking or selective call code. The blocking is disabled after the second three is received until the incoming carrier is dropped.

4#4 is the touchtone test function. Any tones up to a maximum of 24 will be played back on CW after carrier drop if preceded with the 4#4 code.

5#5 will repeat what was sent during a 4#4, or the telephone number requested in an autopatch, whichever was last.

67# is the autopatch code. In one transmission, the code plus the telephone number must be sent. The processor will not access the telephone line unless a valid telephone number is received. Normally this consists of exactly 7 digits, the first digit not a 1. Other valid numbers are 8 or 11 digits, with the first digit a 0 and the single digit codes. If the single digit code is correct, the proper emergency number will be found and sent. If an invalid number is attempted, nothing happens, exactly as if no autopatch attempt had been made. For valid numbers, the repeater will bring up the telephone line and redial the stored telephone number. This system prevents incorrect calls due to signal chopping which cause shotgunning of the touchtones (which result in more than 7 digits). When a single digit code is used, the three-minute timer is defeated automatically. If the 67# is sent by itself and the direct autopatch bit is set, then the repeater will bring up the telephone line and permit the user direct access to the telephone dialing system. This is not normally done, as it is not needed.

9#5 is the remote base code. The normal method is to use this by calling in on the phone line. However, nothing prevents its use on the air. All it does is connect the repeater to the phone lines, but it will not initiate a call. This is not strictly a user code, as the users should not know it, but there is no technical distinction between it and the other user codes. If the repeater times out during an autopatch or a remote base function, those functions will be canceled.

2*2 also performs the tape function. There is no distinction between this and the 2#2 except that the 2*2 is for control stations only. The two codes may be disabled separately. By using the 2*2 function, if it becomes necessary to disable 2#2, control operators may activate the tape upon request without needing to get into command mode and enable the 2#2 function.

In order to exert command on the repeater, it is necessary to enter the command mode. 6*# initiates the request. After entering this code, the carrier must be dropped. If the command is from the telephone line, the procedure may continue immediately. A confirmation code must be entered next. The confirm code is #*6. *Important:* Once the command code is issued, the system will wait for the confirm code forever. If no tone is given, the system will not be reset until it receives another touchtone. After the confirm code is entered, the carrier must be dropped again. Next, a single digit code is entered. If the single digit is a valid command, then the repeater will acknowledge with an "R". With the exception of three special single digit commands, the command mode is automatically left, and operation is again normal. A description of the single digit codes follows.

The system has five different messages. Four are permanently stored in the ROM. They are presently (1) "DE WR3AFM BARC," (2) "DE WR3AFM BALTIMORE," (3) "73 DE WR3AFM," and (4) "DE WR3AFM BALTO ARC." In addition to these four, there is a fifth which may be programmed through another command.

Commands one through five select that number ID to be used always. Command six rotates through 1,2,3,4,1,2,3,4, etc., each time the repeater identifies. Command seven rotates through all five IDs.

Command nine resets all functions to the normal state. Normal is both repeaters enabled, ID #1 selected, and all other outputs ungrounded. This is the same thing as pushing the reset button on the control system.

Command * resets the ID timer. The next time one of the repeaters is kerchunked, that repeater will identify. A word here about the timing of IDs is in order. In the rest mode, as after the * command, the first repeater used identifies. If, in the subsequent three minutes, one or both of the repeaters is used, then one or both of the repeaters will identify three minutes later. In this manner, the repeater is a "tail-ender," and always gets in the last word (something that is very difficult for one of us mortals to do on the repeater).

Commands 8, 0, and # are the commands which do not exit the command mode immediately. Command eight is the ID load command. This loads ID #5 into memory. It does not change the specification of which ID is to be used. After entering the eight, and dropping carrier to hear the "R", the load program is waiting for further instructions. The ID is loaded in a character-by-character fashion. Dits are zero, dahs are one. The characters are loaded in the same as they are in Morse. For instance, take the letter "F". This is di-di-dah-dit, corresponding to 0,0,1,0. To enter "F", then the sequence should be 0,0,1,0. When the letter is entered, enter a 2 to signify that that letter is done. Continue loading characters in this manner. A 2 entered with no zeroes or ones will automatically be translated into a space. When the entire message has been entered, a 3 signifies that you are

equipment is General Electric MASTR. This includes the voting selector, receivers, transmitters, and control shelves. The voter has two outputs: the COS line and the audio output. The COS (carrier operated switch) is low when an incoming signal is present. This is at a transistor level, and, actually, we added single transistor inverters in several places throughout the system to interface the various components exclusive of the control system. All audio lines in the system are balanced. The control system is designed for balanced lines; therefore, it will work with both balanced and unbalanced lines. If you use unbalanced lines, be certain to keep track of the hot and cold ends so that they match up. There are select and disable lines driving the voter. These lines are active low. The control system provides a ground when commanded; otherwise, the select and disable lines are open.

The 440 control receiver has the COS and audio lines the same as the voter. Additionally, Private Line™ or Channel Guard™ subaudible tones may be required to unsquelch it. This "PL" enable line requires a ground when it is desired to place the receiver into the PL mode.

The two meter repeater is connected to its control shelf (standard MASTR equipment) in the ordinary fashion. The PTT (push-to-talk) line is just that. The PTT interfaces with the rest of the system only through the control system. It is used for two purposes: to keep the transmitter on the air during IDs and to see if the repeater has timed out. The control shelf provides the three-minute timer and drop delay timer. The PTT line is disconnected from its normal feed. During normal operation, the control system reconnects the PTT and feed. The transmitter audio pair is the audio input to the transmitter. This is shorted out to block repeating of touchtones and is shorted with the same lines from the 440 transmitter for linkups. The "PL" audio input is any audio input

Command Codes

done. The repeater acknowledges this with an "R", and the ID load and command commands are exited. Normally, place a space at the beginning and at the end to make the IDs uniform. Always be certain that the ID load mode is left, or the controller will be waiting to receive a "3" before it resumes its normal functions. After loading a message, you should select ID #5 and either wait to hear it or reset the ID timer to hear it to verify that it received what you think it did. After loading and verification, the desired ID mode can be set (either 5 or 7).

Command zero is the most powerful command, and it is through it that positive control is established. After releasing carrier and hearing the "R", the output mode is entered. In this mode, the repeater is waiting for three digit codes specifying which output bit to change. There are 64 bits arranged as eight eight-bit ports. Port 0 is a dummy port; it has no output lines and is used to disable the user functions. Port #1 is used by the indirect commands and is not normally used in the output mode. Ports #2 and #3 are enable functions. Port #4 is completely spare, port #5 is voter receiver disable, port #6 is voter receiver enable, and port #7 controls the touchtone generator. For ports #5 and #6, the bit number is the receiver number. This leaves room for eight receivers with no changes necessary. The normal configuration is all ports zero. This gives an ungrounded condition on the voter and spare ports. The three digit sequence for the output mode is XYZ, where X is the port number, Y is the bit number, and Z is either 0 (normal) or 1 (asserted). After each output sequence, the output routine acknowledges with an "R" if the command is valid. Invalid commands would be 831, 690, 300, 236, for obvious reasons. After each sequence, the output routine waits for further commands until a * is sent. The repeater sends an "R" to this and output and command modes are exited. For example, to turn off 67: enter command mode (6*#, #*6), 0, (output mode), 281 (turn it off), * (exit command).

Command # permits loading of the telephone number stored for the single digit #1. Simply send the telephone number followed by a *. An "R" acknowledges loading and exits command mode.

Always be sure that you have left the ID load, output, and load telephone number modes. If the repeater IDs, you have. This is true for all commands. A useful command to execute before ending a control session is the reset timer command, to hear the ID which guarantees that all is OK.

```
1#1 - 150/450 link
2#2 - Tape loop
3#3 - Disable blocking until carrier drop
4#4 - Touch Tone(R) Test
5#5 - Repeat 4#4 or autopatch number
67# - Autopatch

2*2 - Tape
9#5 - Remote base
```

```
6*# - Command mode
#*6 - Confirm command mode

After in command mode:
1 - Select ID #1: " DE WR3AFM BARC "
2 - Select ID #2: " DE WR3AFM BALTIMORE "
3 - Select ID #3: " 73 DE WR3AFM "
4 - Select ID #4: " DE WR3AFM BALTO ARC "
5 - Select ID #5: programmable through command 8
6 - Rotate through IDs 1 through 4
7 - Rotate through IDs 1 through 5
8 - Load ID #5:
        0 - Dit
        1 - Dah
        2 - End character
        3 - End load mode
9 - Reset all outputs and modes to normal operation
0 - Output mode:
        XYZ - Port X, Bit Y, Output Z (exit output mode with *)
* - Reset ID timer (first repeater up IDs)
# - Load single digit #1 telephone number (exit with a *)

Output Ports:
Port #0
1 - 1#1 disable
2 - 2#2 disable
3 - Direct autopatch enable
4 - 4#4 disable
5 - 5#5 disable
6 -
7 -
8 - 2*2 disable

Port #1 - DO NOT USE

Port #2
1 - Beep disable
2 - Control receiver PL enable
3 - 150 Touch Tone (R) disable
4 - Telephone Touch Tone (P) disable
5 - Control Touch Tone (R) disable (when absolutely necessary)
6 - Autopatch disable
7 - 450 Repeater disable
8 - 150 Repeater disable

Port #3
1 -
2 -
3 -
4 -
5 - DO NOT USE
6 - Timer disable
7 - DO NOT USE
8 - DO NOT USE

Port #4
1 -
2 -
3 -
4 -
5 -
6 -
7 -
8 -

Port #5 - Voter disable
1 - Receiver #1 (Charles Street)
2 - Receiver #2 (Cub Hill)
3 - Receiver #3 (K3VC)
4 - Receiver #4 (WR8S)
5 - Receiver #5
6 - Receiver #6
7 - Receiver #7
8 - Receiver #8

Port #6 - Voter select, bits same as port #5

Port #7 - DO NOT USE
```

which is not affected by the normal talk audio. It is used for the CW ID tone. The CS COS (control shelf COS) will key the transmitter when grounded. This goes through the two timers in the control shelf and drives the PTT feed. The CS AUD (control shelf audio) pair goes through line amplifiers and compressors to drive the transmitter. This is normally connected to the voter audio output. The RUSOS lead is a lead which, when grounded, keeps the transmitter on through the timers. A ground on the RUSOS lead will not feed back on the CS COS lead. The RUSOS lead is grounded for autopatches. The DUPLEX AUD is a bidirectional audio path. It is labeled "AUD" on the rear of the control shelf. When the CS COS is low, audio exits from the DUPLEX AUD lead. If +10 volts is placed on the AUDIO GATE line, audio placed on the DUPLEX AUD pair will be fed to the transmitter. This is used to place telephone line audio on the air. When the DISABLE TIMER lead is grounded, the three-minute time-out timer is bypassed and the repeater will not time out. This is used during emergency telephone calls. The time-out timer is on the input, not the output of the repeater. Between each transmission, the timer resets. It is not necessary to let the repeater carrier drop. However, when the "beep" is active, a fraction of a second after the input signal disappears, the repeater will beep. The FORCE TIMER line, when grounded, makes the control shelf believe that a signal is present even if it is not. This is used so that when the "beeper" is enabled, not waiting for the beep will not reset the time-out timer.

The connections for the 440 repeater use the same definitions as the 150 repeater. There is a separate interface for that repeater which provides an autopatch on a second telephone line. That is not

—Correction—

Yaesu FT-227RA

The product review of the Yaesu FT-227RA in the January issue of 73 incorrectly states that a conversion kit is available through Yaesu. There is no conversion kit available.

of importance when interfacing with the control system, except that the autopatch logic includes a 1#1 output function so that when that code is sent, the LINK line is grounded. This permits linking up the repeaters from the 440 end.

The telephone line interfaces with the control system and is switched properly by it. In this system, the telephone company interface device is at a member's house. There is a dedicated line from his house to the repeater site. The audio and a reversing dc voltage are on the single pair, and its operation will be described later. If the telephone company interface device is to be located at the repeater, all of the necessary signals are present in the control system to handle it and it would be simpler than our arrangement. There is a tape recorder connected to the line during autopatches, and the recorder is located at the member's house rather than at the repeater. This allows changing tape easily.

There are various subassemblies in the control system. Rather than building everything from scratch, we used good quality commercial units where possible. There are three audio amplifiers. Two are used for the telephone line and one for driving the touchtone decoder. The amplifiers are IT&T K227s. They are balanced input/output, 600 Ohm. The gain is variable from −.5 to +36 dB, and they each draw 18 mA from a 16- to 24-volt supply. Similar amplifiers should not be too difficult to find, or a few op amps should do the trick nicely. The touchtone decoder is an IT&T K-247-B. It is normally 600 Ohms and is modified for 10k audio input impedance. The digit lockup is disabled. The decoder has 13 outputs: one for each of the 12 digits and one which detects any valid touchtone (VTT). Each of these lines is normally open and goes low when active. Any decoder may be used which follows these conventions, but beware of 567-type decoders which do not employ high/low audio group filtering. I encourage the use of commercial decoders. Lacking that, be sure to test homemade ones extensively. While the microprocessor is the brain of the system, the decoder is the heart of the system.

A standard touchtone pad is included to facilitate controlling the repeater when at the repeater site.

The tape loop is a Mohawk Message Repeater. This is an antique vacuum tube device which could certainly be replaced with a newer piece of equipment. When one pair of wires is shorted, it activates the tape. While the tape is running, an output pair is shorted. Any cartridge-type machine should be suitable, and a standard 8-track player could be modified for this use. The tape must turn itself off when completed.■

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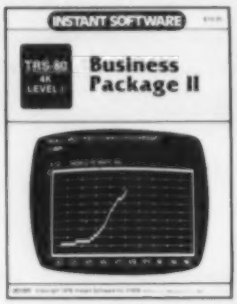

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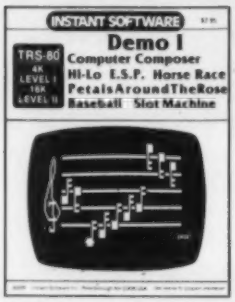

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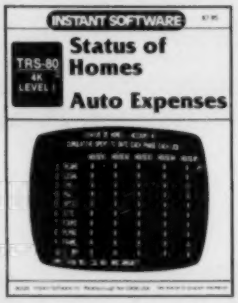

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Speed (wpm)	5	7	10	13	16	20	25	30	35	40
Hex code	3F	2D	1F	17	13	0F	0C	0A	09	08

Table 1. Hex byte for code speed desired is entered in M(0004).

One-byte characters

A	22	N	21
B	41	O	37
B	41	O	37
C	45	P	46
D	31	Q	4B
E	10	R	32
F	44	S	30
G	33	T	11
H	40	U	34
I	20	V	48
J	4E	W	36
K	35	X	49
L	42	Y	4D
M	23	Z	43
word space		EE	
stop		FF	

Two-byte characters

1	50	1E	.	60	2A
2	50	1C	,	60	33
3	50	18	?	60	0C
4	50	10	/	50	09
5	50	00	double dash	50	11
6	50	01	end of message	50	0A
7	50	03	end of work	60	28
8	50	07	wait	50	02
9	50	0F			
0	50	1F			

Table 2. Hex codes for letters and punctuation.

Equipment Required

The Cosmac microcomputer constructed around the CDP1802CD CPU is used with 256 bytes of RAM of which 105 bytes are used for the main program, the rest being used for storage of the messages. Program timing assumes a clock frequency of 1 MHz, but it is easily adapted for other clock frequencies. Other hardware that you will need is shown in Fig. 1. This includes some ICs to interface the computer and hand key to the transmitter and a sidetone oscillator.

How the Program Works

The byte stored in M(0004) is selected initially by the operator from Table 1. This byte sets the length of a dot and hence sets the speed of the code. The program triples this to get a number that will represent the length of a dash; this is stored in R6.0. Four times the dot byte represents a word space, and this byte is

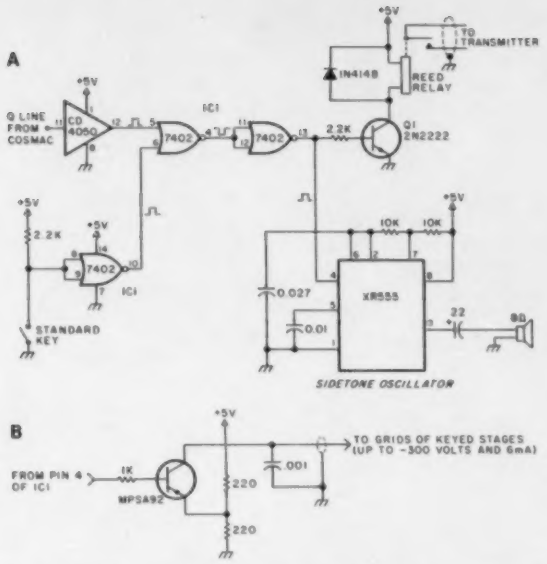


Fig. 1.(a) Interface between Cosmac and transmitter; (b) alternate circuit for rigs with grid-blocked keying eliminates relay and Q1.

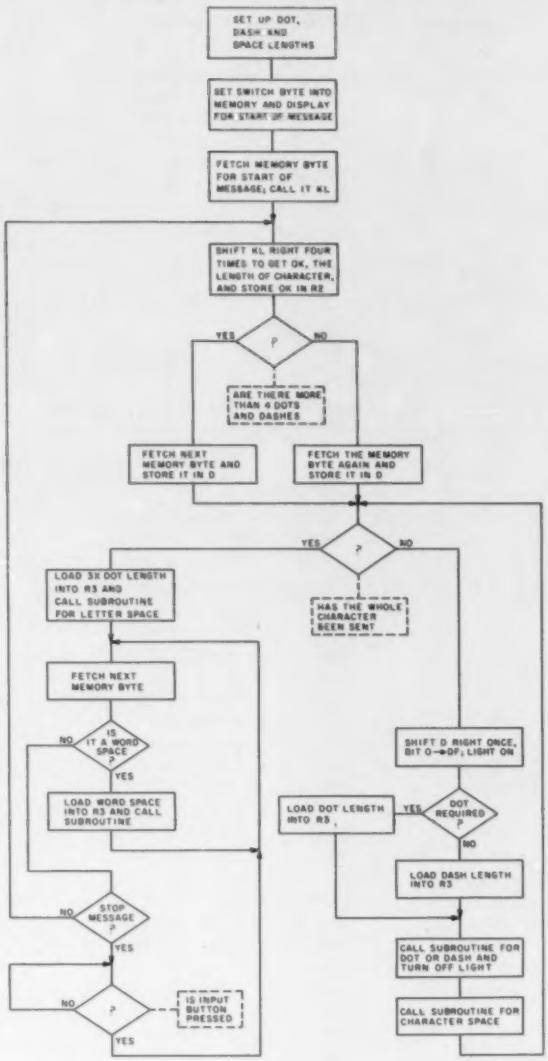
stored in R7.0. Actually, this space gets added to the usual space of three dots that follows every letter so that the actual space between words is equal to seven dots. These bytes are later used to specify the length of a timed loop and thereby set the length of all the dots, dashes, and spaces.

The program fetches the first byte of the programmed message from M(0069). It is 45, which stands for the letter C, as you can see from Table 2. The first digit, 4, is the total number of dots and dashes in the letter. The second digit, 5, specifies the order in which the dots and dashes appear. Taking C as the example, —·—· can be represented in binary form by 0101, where the 0 represents a dot and the 1 represents a dash. This is the binary code for the number 5. So byte 45 tells the computer the order of dots and dashes and the number of dots and dashes in the letter. To actually generate the code —·—·, the number 0101 is stored in the D-register. D is shifted right giving 0010, and the 1 that peels off the right end of the number tells the computer to send a dash first. D is shifted right again, giving 0001; this time, a 0 peels off the right end, producing a dot. A third shift gives 0000, pushing a 1 off the right end, thus making a dash. A fourth shift gives 0000, pushing a 0 off the right end; this makes the final dot. The computer stops shifting D now because the 4 in byte 45 tells it to make only 4 shifts. A letter space is then generated and the next byte is fetched from M(006A).

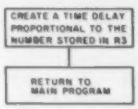
Since there are no letters that have more than 4 dots and dashes in total, the order of dots and dashes in any letter can be represented by four binary digits or one hex digit. The numbers, punctuation, and other special characters listed in Table 2 contain 5 or more dots and dashes. To handle each of these, two bytes are required; the first specifies the total number of dots and dashes, while the second specifies the order in which they occur.

The rest of the program is easy to follow from the

Fig. 2. Main program flowchart.


SET UP DOT, DASH AND SPACE LENGTHS
SET SWITCH BYTE INTO MEMORY AND DISPLAY FOR START OF MESSAGE
FETCH MEMORY BYTE FOR START OF MESSAGE; CALL IT KL
SHIFT KL RIGHT FOUR TIMES TO GET OK, THE LENGTH OF CHARACTER, AND STORE OK IN R2
YES
?
NO
ARE THERE MORE THAN 4 DOTS AND DASHES
FETCH NEXT MEMORY BYTE AND STORE IT IN D
FETCH THE MEMORY BYTE AGAIN AND STORE IT IN D
YES
?
NO
LOAD 3X DOT LENGTH INTO R3 AND CALL SUBROUTINE FOR LETTER SPACE
HAS THE WHOLE CHARACTER BEEN SENT
FETCH NEXT MEMORY BYTE
NO
IS IT A WORD SPACE ?
YES
LOAD WORD SPACE INTO R3 AND CALL SUBROUTINE
SHIFT D RIGHT ONCE, BIT 0→DF; LIGHT ON
LOAD DOT LENGTH INTO R3
YES
DOT REQUIRED ?
NO
LOAD DASH LENGTH INTO R3
NO
STOP MESSAGE ?
YES
CALL SUBROUTINE FOR DOT OR DASH AND TURN OFF LIGHT
NO
?
IS INPUT BUTTON PRESSED
YES
CALL SUBROUTINE FOR CHARACTER SPACE

Subroutine flowchart



R0—forms timed loop in subroutine, setting the speed of the code
R1—main program counter
R2—stores the total number of dots and dashes in the character being sent
R3—stores length of dot, dash, or space for use in subroutine
R4—subroutine counter
R5—memory pointer for length of dot
R6—stores dash length
R7—stores word space length
R8—stores address of the start of the recorded message
R9—stores hex code for character being sent
RA—memory pointer; points to M(0005)

Table 3. Register assignments.

Fig. 3. Program listing. Title: Programmable Morse code generator.

Address	Bytes	Comment
0000	F8	06→D set main
0001	06	program counter
0002	A1	D→R1·0
0003	D1	1→P go to main program
0004	0D	store dot length
0005		address of start of message
0006	F8	5C→D set subroutine counter
0007	5C	
0008	A4	D→R4.0
0009	F8	04→D set memory pointer
000A	04	
000B	A5	D→R5·0 points to dot
000C	E5	5→X
000D	F0	MX→D fetch dot length
000E	F4	MX + D→D
000F	F4	MX + D→D
0010	A6	D→R6·0 store dash length
0011	F4	MX + D→D
0012	A7	D→R7·0 store word space
0013	F8	05→D set memory pointer
0014	05	
0015	AA	D→RA·0
0016	EA	A→X
0017	6C	input switch byte→ MX, D
0018	A8	D→R8·0
0019	64	MX→display, RX + 1
001A	2A	RA-1
001B	E8	8→X
001C	F0	MX→D fetch byte KL
001D	F6	shift D right
001E	F6	
001F	F6	
0020	F6	
0021	A2	D→R2·0 store OK
0022	FD	04-D→D, carry→DF
0023	04	
0024	3B	go to 28 if DF = 0
0025	28	
0026	F0	MX→D fetch byte again
0027	C8	long skip to 2A
0028	18	R8 + 1
0029	F0	MX→D fetch next byte
002A	A9	D→R9·0 store character
002B	82	R2·0→D OK→D
002C	32	go to 44 if D = 00
002D	44	
002E	89	R9·0→D
002F	F6	shift D right, bit 0→DF
0030	A9	D→R9·0
0031	7B	1→Q start timed interval
0032	3B	go to 38 if DF = 0
0033	38	
0034	86	R6·0→D load dash
0035	A3	D→R3·0
0036	30	go to 3B
0037	3B	
0038	45	M5→D, R5 + 1 load dot
0039	25	R5-1
003A	A3	D→R3·0
003B	D4	4→P call subroutine
003C	7A	0→Q end of timed interval
003D	45	M5→D, R5 + 1
003E	25	R5-1
003F	A3	D→R3·0 make space
0040	D4	4→P call subroutine
0041	22	R2-1 decrement length
0042	30	go to 2B
0043	2B	
0044	86	R6·0→D load letter space
0045	A3	D→R3·0
0046	D4	4→P
0047	18	R8 + 1 fetch next byte
0048	F0	MX→D
0049	FF	D-EE→D
004A	EE	test for word space
004B	3A	go to 52 if D ≠ 00
004C	52	
004D	87	R7·0→D
004E	A3	D→R3·0
004F	D4	4→P make word space
0050	30	go to 47
0051	47	
0052	F0	MX→D
0053	FF	D-FF→D
0054	FF	test for end of message
0055	3A	go to 1C if D ≠ 00
0056	1C	
0057	3F	go to 57 if EF4 = 0
0058	57	wait
0059	30	go to 47
005A	47	continue message
005B	D1	1→P return to main program
005C	F8	4E→D start subroutine
005D	4E	set speed
005E	A0	D→R0·0
005F	20	R0-1
0060	80	R0·0→D
0061	3A	go to 5F if D ≠ 00
0062	5F	
0063	23	R3-1
0064	83	R3·0→D
0065	3A	go to 5C if D ≠ 00
0066	5C	
0067	30	go to 5B
0068	5B	end of subroutine
0069	45	C recorded message
006A	4B	Q
006B	EE	word space
006C	45	C
006D	4B	Q
006E	EE	word space
006F	45	C
0070	4B	Q
0071	EE	word space
0072	31	D
0073	10	E
0074	EE	word space
0075	48	V
0076	10	E
0077	50	3
0078	18	
0079	45	C
007A	36	W
007B	4D	Y
007C	EE	word space
007D	48	V
007E	10	E
007F	50	3
0080	18	

0081	45	C
0082	36	W
0083	4D	Y
0084	EE	word space
0085	35	K
0086	FF	stop
0087	33	G
0088	23	M
0089	EE	word space
008A	37	0
008B	23	M
008C	EE	word space
008D	50	double dash
008E	11	
008F	EE	word space
0090	34	U
0091	32	R
0092	EE	word space
0093	32	R
0094	30	S
0095	11	T
0096	FF	stop
0097	40	H
0098	32	R
0099	EE	word space
009A	20	1
009B	21	N
009C		etc.

flowchart in Fig. 2. Two special bytes were set up. One is EE, which calls for a word space; the other is FF, which halts the program until the input button connected to EF4 is depressed.

Using the Program

Select the code speed desired from Table 1 and store this byte at M(0004). Table 1 was constructed assuming a clock frequency of 1 MHz. If your crystal is not 1 MHz, simply experiment a little with different hex bytes to get the different speeds. The code speed varies inversely with the size of byte.

After entering the main program, decide on the messages you want and select from Table 2 the bytes for each letter, number, or punctuation. Note that the numbers and punctuation require two bytes each. Terminate each message with FF so that the program will halt. To initiate one of the messages, enter the memory address of its first byte from the front panel of the computer using the toggle switches. Turn on the run switch. When the message terminates, you can make it carry on with the next stored message by pressing the input button which is connected to EF4. This way, you can have pauses inserted in messages to allow you to enter a signal report or callsign manually.

Interface Circuitry

The circuits shown in Fig. 1 are just suggestive. They work for me, but you may have to adapt them to your own rig. One possible area of difficulty I have noticed is that of rf from the transmitter getting into the IC gates and playing havoc with them. The problem seems accentuated at 14 MHz and higher with my 180-Watt rig. Typically, after a few dots and dashes are sent, the transmitter comes on and stays on. The cure is to shield the IC circuits in a metal enclosure and bypass incoming and outgoing leads with 0.001 uF ceramic capacitors. ■

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To get my ham license in 1949, I had to produce one minute of perfect copy at 13 wpm. A full year's striving to reach this goal resulted in a set of conditioned reflexes by which the code sounds entered my ears and came out my fingers as written text, after which the message was interpreted by my eyes. This roundabout process caused habits which have ever since inhibited both my skill and enjoyment where CW is concerned. The inclusion of my handwriting in the process was particularly unfortunate since, under pressure, my writing tends to become rather spastic. The process inhibits the ability to "copy behind" and to "copy in the head."

I needed a method of creating a new set of reactions which would generate mental images from the code sounds. Many ideas came to mind, but none provided a simple method of coordinating audio and visual presentations of characters, together with flexibility, without complicated special-purpose equipment.

Then, a couple of months ago, we added an audio alarm to our office minicomputer. This alarm gives a single 960 Hz beep in response to PRINT HEX(07). It is used to signal the operator when the machine needs attention for any reason foreseen in the program. Once I found that the duration of the tone could be controlled by changing the number of iterations in a loop containing this statement, it was inevitable that I would program a code teaching machine.

I have written this article hoping that others with similar CW problems, or those conducting code classes, will find the system useful and will let me know how they fare. The program contains a few wrinkles which may prove interesting to persons concerned primarily with programming methods.

Practice material can be stored in data statements in the program or, with simple changes, in external files. The program accommodates a full range of numerals, punctuation, and upper and lower case alphabetic character material. As the text is scanned, each character is converted into its audible CW equivalent and, an instant later, appears on the CRT as an addition to the string of previously sent characters.

The code element speed and the element and character spacings are adjustable, as well as the delay of the CRT display of the character. There are a number of apparent advantages to this system. A student working solo with this program need never try to memorize the code from any printed representation, either in dots, dashes, or didahs. All that is stored in the program. The code sound is emitted, and then the letter appears on the screen to reinforce the character recognition. For code classes, practice material can be selected from any source and stored for later use. The instructor can input text to his machine and then recall it as CW at any speed appropriate to class needs. My equipment will store 80,000 characters on a cassette, some 16,000 words, or 64 typed pages of text. Such material can be used over and over at any desired speed.

Characters are handled in a computer as binary numbers which have decimal, octal, and hexadecimal equivalents. In developing this program, it was necessary only to consider the ASCII decimal equivalents of the various CW characters. Fortunately, and possibly not coincidentally, the characters used in CW transmissions

are represented by ASCII decimal numbers lying in the range 40 to 90. A table of these characters is shown in Fig. 1, together with the string symbols used to control the audio output. Lowercase letters are represented by ASCII decimals 97 to 122. A few characters — the star, semicolon, "less than" and "greater than" symbols, and the @ sign — have no international Morse symbols that I could find, so provision is made to skip these characters when encountered.

The equipment required to use this program is a small computer programmable in BASIC with STRING functions, a CRT display, and an audible tone alarm. The version of the program given here, which includes several lines of practice text, runs in about 2350 bytes.

My machine is a Wang WCS1OT, which includes the CRT, cassette drive, and keyboard in a single console with an outboard CPU. The BASIC compiler is hard-wired, so I do not have access to the machine language. Wang BASIC is an augmented subset of general BASIC, and only those features special to STRING manipulation and character identification have been used. If your BASIC lacks any of these features, but you can write machine language functions, you should be able to run a version of this program. Notes relating to conversion of the program to other dialects are located at the end of the article.

The program can be followed readily from the listing of Fig. 2. A word is in order about this listing. The program was originally written and debugged using one statement per line. When operation was satisfactory, the program was "compressed" by removing REMs and combining as many statements as possible on each line. This saves a sensible amount of core and results in an almost unreadable LIST. To get the listing given here, the compressed program was processed by a utility which prints one statement per line and indents FOR/NEXT loops. The line numbers went unchanged throughout, except for deletions, accounting for the peculiar sequence shown here.

ASCII No.	Character	Code Symbol
40	(	101101
41	)	010010
42	*	2
43	+	01010
44	,	110011
45	-	100001
46	.	00200200
47	/	10010
48	0	11111
49	1	01111
50	2	00111
51	3	00011
52	4	00001
53	5	00000
54	6	10000
55	7	11000
56	8	11100
57	9	11110
58	:	111000
59	;	2
60	[	2
61	=	10001
62	]	2
63	?	001100
64	@	2
65	A	01
66	B	1000
67	C	1010
68	D	100
69	E	0
70	F	0010
71	G	110
72	H	0000
73	I	00
74	J	0111
75	K	101
76	L	0100
77	M	11
78	N	10
79	O	111
80	P	0110
81	Q	1101
82	R	010
83	S	000
84	T	1
85	U	001
86	V	0001
87	W	011
88	X	1001
89	Y	1011
90	Z	1100
97	a	01
98	b	1000
99	c	1010
100	d	100
101	e	0
102	f	0010
103	g	110
104	h	0000
105	i	00
106	j	0111
107	k	101
108	l	0100
109	m	11
110	n	10
111	o	111
112	p	0110
113	q	1101
114	r	010
115	s	000
116	t	1
117	u	001
118	v	0001
119	w	011
120	x	1001
121	y	1011
122	z	1100

Fig. 1. ASCII decimal codes, characters, and CW sound codes.

Now for program operating: At LN 30, the variables are dimensioned as necessary. C$(52)8 provides for a list of 52 code symbols, each 8 characters or less.

M$64 sets up a string variable containing up to 64 characters to receive text lines.

T(4) is a list of the speed control numbers.

T$(4) is a string list to receive speed prompts. In this BASIC string, variables with no specified length take a default of 16 characters. So the prompts can be up to 16 characters in length.

A$1 sets up a single character variable.

At LN 80, a loop READs the speed data prompts from DATA into list T$(). Then another loop READs the code symbol strings into 52-element list C$(). At LN 170, a third loop displays each of the prompts on the screen. An "edit" routine follows, providing for inputing the necessary control numbers. This method of data INPUT is one I use rather routinely, but it is not essential to the program. The Wang INPUT statement allows the inclusion of the prompt message in the statement. If you lack this feature, you should use a PRINT statement "CHANGE ITEM #" preceding INPUT. Each INPUT of a value causes a loop back to LN 170 where PRINT HEX(03) blanks the screen and prints a new data display from the top. When the necessary controls have been entered, "0" used as an answer to "CHANGE ITEM?" will exit the edit routine.

The change of variables at LN320 may seem unnecessary. My computer has a HALT/STEP key which will interrupt program operation at any time and permit the program to

be restarted after changing the value of a variable. Use of the unsubscripted variables makes the value changing a mite simpler during an interrupted RUN.

The next statements blank the screen, set the DATA pointer to the beginning of the practice text, and move the cursor to the center of the screen, respectively. HEX(OA) is a line feed.

At LN 410, the next text line is READ and tested. If the DATA is not "***", the program continues, otherwise the DATA system is reset and the program repeats from LN 410. If your BASIC does not have the ability to RESTORE to a particular DATA item, you will have to program an alternative at this point. This version of the program assumes the practice text is stored in DATA statements. Changes at this READ routine will permit the text to be taken from some other storage medium.

LN 490 counts the characters in text line M$, and the program enters a loop to process the line one character at a time. The next character is stored in A$, and the ASCII decimal value of A$ is put in A.

The following IF statements provide a means for accepting a variable only if it has a value between certain limits. Letting U, L be the upper and lower limits, respectively, the comparison statement is set up as:

ABS(A − (U + L)/2).LE.(U − L)/

and will reject any value outside the limits.

The first comparison rejects A unless it has a value between 40 and 90, which includes characters from "(" to "Z". Any value outside this range is tested again at LN 490. Values from 97 to 122 represent lowercase letters and are shifted to uppercase at LN 640. Any other value of A results in a blank being printed on the screen, and no code sound is generated. If your machine does not have lowercase, you can simplify the program by removing the second test of A.

A anomaly of the program as written is that a lowercase letter is interpreted so as to produce the same code sound as an uppercase, but the lowercase character is added to the screen. Of course, this presents no difficulty.

At LN 660, A is shifted in value to serve as the subscript for array C$(), and the coding for the corresponding CW sounds is stored in C$.

There follows the loop to process the code symbols. There are other ways of analyzing the symbol

Fig. 2. BASIC program listing.

```
10      REM  DIDAH1.2    GW     FEB 04, 1978
20      REM  GEORGE WALDIE     26½ S.MAIN, MT. GILEAD, OHIO 43338
30      DIM C$(52)8,M$64,T(4),T$(4),A$1
80      FOR J = 1TO 4
          READ T$(J)                                    Read speed prompts
          NEXT J
        FOR J = 1TO 52
          READ C$(J)                                    Read code symbols
          NEXT J
170     PRINT HEX(03)
          FOR J = 1TO 4
          PRINT J;T$(J);TAB(15);T(J)                    Display control data
          NEXT J
        PRINT
        Q = 0
        INPUT "CHANGE ITEM #",Q                         Edit control data
        IF Q = OTHEN 320                                Exit edit routine
        INPUT "CHANGE TO",T(Q)
        GOTO 170
320     T1 = T(1)
        T2 = T(2)                                       Change variables
        T3 = T(3)
        T4 = T(4)
        PRINT HEX(03)                                   Clear screen—home cursor
        RESTORE 57                                      Reset data
        PRINT HEX(030A0A0A0A0A0A0A0A)                   Center display
410     READ M$                                         Read data line
        IF STR(M$, 1, 3)<>"***"THEN 490                 Test for end
        RESTORE 57
        GOTO 410                                        Repeat
490     M = LEN(M$)                                     Length of data string
        FOR J = 1TO M
          A$ = STR(M$,J,1)                              Next character
          A = VAL(A$)
          IF ABS(A-65)<25THEN 660                       Test for uppercase
          IF ABS(A-109.5)< = 12.5THEN 640               Test for lowercase
          A$ = " "
          GOTO 940
640       A = A-32                                      Shift from lowercase
660     C$ = C$(A-38)
        FOR I = 1TO LEN(C$)
          CONVERT STR(C$,I,1)TO C
          ON C + 1GOTO 790,840
```

strings, but the method shown suits my equipment and is efficient. The next character in the symbol string is CONVERTed to a numeric which then controls the branching. Any value of C but 0 or 1 generates a blank.

In the DATA statements for the character codes, you will notice the appearance of "2"s in several places. In most cases, these mark characters for which no CW code combinations were found. However, the CW period does include internal spaces which require this "2".

The "normal" branches to LN 790 and 840 go, respectively, to generators for dits and dahs. These are identical loops, except that the dah loop has twelve times as many iterations as the dit loop. If you are puzzled because you understand that a dah should be only three times as long as a dit, remember that the speed of the CPU enters here. In fact, you may have to adjust these loops to make the output sound right. The twelve multiplier was arrived at experimentally.

Both the dit and dah loops exit to 880, the intracharacter space loop. This is simply a "do nothing" loop to use up time. Again, you can change the multiplier to suit your taste (ear?). Notice that both dit and dah loops are controlled by T1, and the intracharacter loop by T2. At 940, B$ is a shift register to maintain, on the screen, the last 16 characters sent. In Wang BASIC, string variables are 16 characters long unless otherwise dimensioned. You must use whatever string length specification is required by your language. LN 940 moves the last 15 characters of B$ to the first 15 positions, leaving a space at the tail of the string for the next character, which is added in the next statement.

Another loop delays the display of the shift register. In this case, a meaningless arithmetic operation is included to provide the delay with fewer loop iterations. In the initial learning stages, this delay can allow "capture" time for CW character recognition. The delay can be reduced as the recognition time decreases.

Remember that, when a FOR/NEXT loop is encountered, it is exercised once even though zero iterations are called for. So, in this case, there will be a delay of the screen display equal to one iteration of the loop even if T4 is zero. This is the reason for the inclusion of the arithmetic operation within the loop. This seems to work well at CW speeds up to about 20 wpm, but this loop is a factor limiting maximum speed, since it does work once for every character. This is a point to look at when you try for maximum possible code speed.

After the shift register B$ is printed, there is a space

```
            IF I<>1THEN 880
            A$ = " "
            GOTO 880
790         FOR T = 1TO T1                                  Generate dit
              PRINT HEX(07);
              NEXT T
            GOTO 880
840         FOR T = 1TO 12*T1                               Generate dah
              PRINT HEX(07);
              NEXT T
880         FOR T = 1TO 9*T2                                Intraelement space
              T = T
              NEXT T
            NEXT I
940         STR(B$,1,15) = STR(B$,2,15)                     Register shift
            STR(B$,16,1) = A$
            FOR T = 1TO 4                                   Print delay
              T = SQR(T*T)
              NEXT T
            PRINT HEX(0C);TAB(20);STR(B$,1)                 Print register
            FOR T = 1TO 4*T3                                Space
              T = T
              NEXT T
            NEXT J
      GOTO 410
1120        DATA "CHAR. SPEED","LTR.SPACE","WORD SPACE","PRINT DELAY"   Speed prompts
1180        DATA "011110","101101","010010","2","01010","110011"
1190        DATA "100001","00200200","10010","11111","01111","00111"
1200        DATA "00011","00001","00000","10000","11000","11100","11110"   Code symbols
1210        DATA "111000","2","2","10001","2","001100","2","01","1000"
1220        DATA "1010","100","0","0010","110","0000","00","0111","101"
1230        DATA "0100","11","10","111","0110","1101","010","000","1"
1240        DATA "001","0001","011","1001","1011","1100"
1290        DATA " THIS IS A PROGRAM TO TEACH THE INTERNATIONAL MORSE"
1300        DATA " CODE."
1302        DATA " A B C D E F G H I J K L M N O P Q R S T U V W X Y Z"
1304        DATA " 1 2 3 4 5 6 7 8 9 0"                     Practice text
1306        DATA " ()* + - ./0123456789:;[ = ]?@abcdefghijklmnopqrstuvwxyz"
1310        DATA " THE QUICK BROWN FOX JUMPED OVER THE LAZY DOG"
1350        DATA "***"

1360        REM Compressed approx program length—1620 bytes
1370        END
```

between characters generated by the delay loop controlled by T3, after which the program goes back for the next text character and repeats the process just described until the entire text string has been used. It then proceeds to the next string of text data.

There is another possible anomaly you should be aware of. Some BASICs include trailing spaces in text strings; others do not. If your version of the language crops trailing spaces from the strings, as mine does, you will have to add a leading blank to each text line, or the last word of each string will run into the first word of the next string without a separating space. Notice the space I have included after the leading quote in each line of the DATA statements at LN 1290 to 1330.

This program illustrates very nicely how a general-purpose computer can serve a very specialized purpose merely by software implementation.

Conversion Notes

The manual for Ohio Scientific, Inc., 6502 8K BASIC states that this dialect will run, without change, programs written for ALTAIR, IMSAI, and SWTP machines and, with slight changes, programs for PDP-8, PDP-11, and NOVA BASICS. The following notes have been prepared using this information. I regret that I have not been able to test the effects of these suggestions.

LN 30 — In Wang BASIC, the DIM statement is used to set the sizes of lists and arrays and also the number of bytes reserved for string variables. Thus C$ is defined as a list of 52 elements of 8 or less characters. There is a default length of 16 characters. This specification appears to be unique to the Wang system.

LN 170 — When the system is turned on, output is selected to the CRT. Alternate outputs can be selected, but are not pertinent to this program.

LN 170 and LN 320 — PRINT HEX(03) clears the screen and homes the cursor to the upper left corner of the screen — corresponds to TTY keyboard CTRL C.

LN 790 and LN 840 — PRINT HEX(07) keys the audio tone — corresponds to TTY keyboard CTRL G.

LN 940—Each 0A in PRINT HEX(0A) issues a line feed — corresponds to TTY keyboard CTRL J. PRINT HEX (0C) moves the cursor up one line.

LN 320 and LN 410 — RESTORE 57 resets the DATA pointer to the 57th item of data, beginning of sample text. OSI BASIC does not offer this feature. Some other BASICs allow RESTORE to a particular DATA line number.

LN 410, LN 490, LN 660 and LN 940 — STR(M$,1,3) refers to string M$, starting with the 1st character, and including 3 characters, to create a substring of M$. OSI uses MID$(M$,1,3) with same meaning.

LN 490 and LN 660 — LEN(M$) returns the number of characters in M$. OSI uses same function.

LN 490 — VAL(A$) returns ASCII decimal value of 1st character of A$. OSI uses ASC(A$).

LN 660—CONVERT STR(C$,I1) to C sets to the numeric value of numeral(s) in string variable—corresponds to OSI CHR(MID(C$,I,1).

The relation operator .LE. is not accepted by my equipment, but is used here because my output writer does not have the usual left arrowhead on its type ball. The operator stands for "less than or equal to."■

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Rod Hallen WA7NEV
Road Runner Ranch
PO Box 73
Tombstone AZ 85638

Programming a Microcomputer —6502, Caxton C. Foster, Addison-Wesley Publishing Co., Reading MA 01867, 230 pages, 6" x 9" softcover, $9.95.

The Little Book of BASIC Style, John M. Nevison, Addison-Wesley Publishing Co., Reading MA 01867, 150 pages, 6" x 9" softcover, $5.95.

Although the instruction contained in *Programming a Microcomputer —6502* pertains in a general way to any 6502 machine, it is based specifically on the KIM-1. In fact, for best utilization of this book, a KIM-1 should sit at the reader's fingertips. This would also make an excellent classroom text as long as one or more KIMs were available to the students.

An advertising flyer states that this book is also usable with the PET, but since the PET is hard to program in assembly language as yet, this hinges on Commodore providing more information about how to operate the PET.

One unusual aspect of the book is a complete lack of mention of the 6502 except in the title and in the appendix, which lists op codes and addressing modes. All 6502 attributes are indicated as if they were KIM-1's exclusive features. To quote, "... the inventors of the KIM-1 provided a form of addressing that circumvents the problem. It is called 'immediate addressing.'" The inventors of the KIM-1 and the MCS6502 are indeed one and the same, but emphasis should be placed on the fact that we are really talking about the KIM-1.

As the result of a coincidence, I became the happy owner of a KIM two days before I received these books. I am an 8080-Z-80 programmer and the 6502 instruction set was a foreign language to me. From that point of view, I'm a beginner, I guess.

Chapter one is a discussion of how the instruction set is used and chapter two takes you step by step through the operation of the KIM-1. Both are well done, but the true neophyte would do well to go very slowly in chapter one. At one point in chapter two, the author failed to tell the student (me!) to restore the program counter after a STOP and before a GO, which means that the following steps didn't work.

Chapters three to thirteen comprise a group of experiments. A problem is presented and instruction on methods is given. The student then writes a program to gain the desired results and attempts to run it. The author's reasoning and solution to each problem are covered in an appendix. Extensive debugging help is also given.

The experiments included involve a Morse-code oscillator, a piano keyboard, a combination lock, a tune player, a digital clock, and many more. In each case, whatever hardware is needed (very little) is fully explained. The chapters that I found most interesting concerned an interpreter and an assembler for a "Dream Machine." The "Dream Machine" is a pseudo-sixteen-bit processor whose instruction set is interpreted by a KIM program. While the instruction set is limited by the amount of KIM memory available, it is an informative and effective means of examining the operation of any instruction on any processor.

The appendices contain sections on binary math, KIM routines, 6502 op codes and addressing modes, and solutions to the programming problems contained in the text. These solutions are written

in assembly language and the student will have to reduce them to machine code in order to run them.

I would hesistate to recommend this book to the complete novice unless he has access to a KIM-1. However, by combining the information contained in the three manuals that come with the KIM-1 with *Programming a Microcomputer—6502*, I feel that I have become an effective 6502 programmer.

The Little Book of BASIC Style wasn't what I thought it would be. Rather than attempting to teach you how to program in BASIC, it is concerned with writing programs so that they can be more easily read by the user.

Nevison contends that programs that are readable are better programs and that they will run the first time with fewer problems. Twenty rules are presented and woven into a discussion which advocates clear structured programs. Many of these rules make good sense, but some are difficult to put into practice.

Variable spacing within a line to make it easier to read won't work if your BASIC interpreter (like mine) eliminates all excess spaces. Using a blank line to separate blocks of code is also a good idea, but it is another no-no for my BASIC.

The author calls for more comments within the body of a program to make for better understanding. One of his programs contains more lines devoted to remarks than it does operational statements. If you are like most computer hobbyists, you don't have the excess memory that all of those remarks take. I like well-commented programs, but I usually strip off the remarks at entry time. But that doesn't mean that you shouldn't use remarks while writing programs. They will clarify to you and anyone else who uses them what is intended.

Each of the rules is presented with one or more examples. Both good and bad methods are shown side by side so that it is easy to see the advantages of style. Many of the rules, such as matching the variable to its meaning—V = Value, I = interest, etc.—and labeling constants, make very good sense. Have you ever attempted to read a poorly-commented program and tried to figure out what purpose each variable and constant served?

After a discussion of the rules of style, some practical examples are given: sorting, craps, plotting, bar graphs, dealing a deck of cards, and more. And then comes the biggest program of all—STYLIST. STYLIST is designed to style your programs for you. While it is a huge program meant to do a task that the programmer should be doing for himself, it does present itself as an example of how to structure a program correctly.

After studying *The Little Book of BASIC Style*, take one of the better programs that you have written and rewrite it according to Nevison's twenty rules. You'll be surprised at how much more readable it is, and six months from now, you'll still be able to figure out how it works without having to rewrite it again.

Addison-Wesley publishes many other computer titles and their 100-page *Business and Computer Science Catalog* should be in every computerist's library. I have just read an advance flyer on the third volume in *The Joy of Computing* series, *BASIC and the Personal Computer*, and I am looking forward to its publication.■

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The 2 Meter ECM Caper

— James Bond, move over!

Snake-Oil gets shut down.

Byron H. Kretzman W2JTP
431 Woodbury Road
Huntington NY 11743

The "Conditional," or Class C, license began many years ago when regular licenses were Class A and Class B. Honest in original intent, the Class C license was supposed to encourage ham radio for the handicapped and others who lived more than 75 miles from an examination point and couldn't make the expensive and time-consuming trip to an FCC office. Later, the distance limit became 175 miles. General Class privileges were available to the Conditional Class, which replaced the old Class C. All that was needed was for someone to swear that 13 wpm could be copied and, as for the Technician Class, to "supervise" the mail-order technical exam.

Because the change from 75 to 175 miles was made not too many years ago, a fair number of phony Conditionals exist, many of whom "bought" their licenses for cash or favors from some radio amateur without ethics. Phony Technicians exist, too, but we won't go into that since this is the story of what happened to a certain phony Conditional. Two meter FM seems to attract these people, for some reason which escapes me.

The story is fascinating. I wouldn't believe it if it were told to me. I'll change a few names to protect the guilty. Even so, I'll bet a dime it reminds you of somebody on FM you know.

It all started when my old friend John came over one night to chew the rag about the DX he works and the DX I used to work. John is an electronics engineer at the local electronic countermeasures (ECM) factory, but he gets his kicks out of working DX on CW. Like me, he uses 146.94 to keep in touch with his local ham friends. We were discussing VR6AY on Pitcairn Island when the .94 receiver opened up to interrupt us. There was Snake-Oil, sounding off like an expert to his phony Technician friends. John says, "Let's have some fun," taking my code practice oscillator off the shelf and standing it in front of the microphone. As soon as Snake-Oil stands by, John gives him a one-by-one call on the straight key at a brisk 10 wpm. Snake-Oil comes back, not to John, but to one of his friends, saying "Hey, the band is

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really open tonight! Just heard the code ID of the repeater upstate!" John looked at me, reached for my *Callbook* and quickly thumbed through it. Finding Snake-Oil's call, he says, "Just as I thought!" and points to the "C". To prove the point, John broke in again with the CPO, sending only Snake-Oil's call, but three times, at about 5 wpm. No answer. Snake-Oil couldn't even recognize his own call!

As time went on, Snake-Oil more and more incurred the wrath of John and other old-timers by setting up a .34/.94 repeater, but his popularity as the local FM "expert" grew as the number of appliance operators grew. Within about six months, .94 became almost useless for a simplex channel. I told John it was impossible to fight this, but he answered, "Don't you ever watch 'Mission Impossible' on TV?" I thought he was kidding.

As I worked around the shack now, .94 never seemed to shut up. It was alive with talk about the coming Division convention. Snake-Oil was on the program and would demonstrate his FM repeater with its vast satellite receiver system which enabled anyone with a hand-held rice box to use the repeater from anywhere in the county. (Snake-Oil was a really busy fellow.) As I said, there wasn't much simplex activity on .94 anymore, and the old-timer didn't like standing in line to use the repeater while all those rice-box mobiles were telling each other what exit they just passed on the expressway. The local intercom feature of .94 seemed to be giving way to "progress."

One Sunday morning, while driving down a street near Snake-Oil's house, I noticed a cable-TV truck parked by a telephone pole about a block away. I caught a quick glimpse of a guy in coveralls and a hard hat. There was something familiar about the guy, but I couldn't put my finger on it. On the way home that afternoon, I saw the cable-TV truck in another part of town. This time I took a real close look at the guy in coveralls. The bell rang—it was John, but with a mustache??? The next Sunday I saw him again in another part of town. What the hell was going on? John is a well-paid engineer. He wouldn't be moonlighting as a pole jockey for a cable-TV outfit, would he? And, how come on Sunday? Was this a gag?

The more I thought about it, the more curious I got. Finally, I couldn't stand it any longer. I called up John, who had been "too busy" lately to come over to chew the rag about DX, and insisted upon going over to see him that night. John was in his basement, at his workbench, apparently breadboarding a bunch of transistors and ICs. This struck me as strange, too. John wouldn't be doing any homework for his job, as his work was highly classified, and John's ham interest was operating—working DX.

I let him have it with both barrels. We were old enough friends, I told him. He could darn well let me know what was going on, as I had a strong feeling that it had something to do with ham radio.

John swore me to secrecy, and then proceeded to unfold the wildest, most complex scheme imaginable, a scheme designed to completely foul up Snake-Oil's coming Division convention demonstration of his repeater system. Pulling out a drawer of his workbench, John showed me a small collection of plastic pill bottles, each with a very short, stiff wire coming out the top and a longer, flexible wire coming out the bottom. Then John took down from a shelf above his workbench a small black box, also with a short stiff wire on its top. The box had several push-button switches, one of which was labeled, "destruct." This switch had a safety cover which had to be flipped up and held up before the switch could be actuated.

As John explained it, each pillbox was a transponder which would generate white noise, upon command, across the entire 2 meter band. John demonstrated it on his .94 receiver. The noise compensated squelch of the FM receiver would simply cut off the audio in the presence of the white noise, which also covered any signal. Of course, the small size of the transponder made its range very short—hence John's crazy scheme of planting one on top of a convenient telephone pole (so it wouldn't be noticed from the ground) close to each one of Snake-Oil's satellite receivers. This he did by borrowing the cable-TV truck from another friend and using it on Sundays to climb the poles himself. The truck was as common a sight in this county as a telephone company truck.

"What's with the 'destruct' switch?" I asked John, having the distinct feeling that this was no gag either. Obviously, John was utilizing considerable know-how from his job at the ECM factory.

"Well," John replied, "with all these transponders out, sooner or later one would be discovered, and it wouldn't take the FBI long to trace it to me."

At this point, John took one of the miniature transponders and set it up on top of a stick stuck into the ground in the middle of his backyard. "Watch!" John manipulated the buttons on his black box and the transponder went "poof!" A bright flash, a small wisp of white smoke, and the transponder was gone! John said, "Don't worry, I've got plenty more of them!"

"What happened?" I asked.

"Thermite," John answered. "A small amount, in the bottom of each pill bottle."

I went home shaking my head. This whole crazy scheme (were all ECM engineers this crazy?) seemed to be an awful lot of trouble just to foul up Snake-Oil. I could think of lots of ways to foul him up, more simple ways, but they all involved long jail sentences for the violence required.

Two days before the convention, John called me up and told me that all was ready. All the transponders were planted, one near every one of Snake-Oil's satellite receivers, all over the county. The black box was mounted in John's car, ready for the operation and then the "destruct" trips around the county.

The night before the convention, John called me up excitedly. "Guess what?" he asked, immediately answering the question himself. "Snake-Oil got called in by the FCC for reexamination, and he flunked not only the 13 wpm test, but the 5 wpm test as well, so they lifted his license!"

What a let-down! All I could think of was the tremendous wasted effort John had put into this crazy jamming project. That night, on the ten o'clock news, it was reported that police switchboards all over the county had earlier lit up with a rash of phone calls, each reporting a mysterious flash of light in the sky. ■

"I Love My Ten-Tec!"

—a look at the 540/544

It's tough to argue with pulpit praise.

Rev. James R. Belt WAØJIH
1006 N. 76
Omaha NE 68114

For the past six and a half years, my hamming had become less and less enthusiastic. My reliable Swan 350 wasn't at fault. The level of activity on my favorite bands had increased, not diminished; that wasn't it either. There is just no way to know why our interests rise and fall. But then, something did happen. One morning, on one of my few remaining skeds, a good friend commented on the fact that tubes were becoming scarce. RCA had gone out of manufacturing tubes and others were soon to follow. What would replace them? Transistors, of course.

That did it. My mind went into a "red alert" condition, and I began reading and rereading all the ads and specs of solid-state rigs. True enough, there were more and more solid-state transceivers for the HF bands. Heathkit's SB-104A and the Atlas 180 had given way to the 350XL, and the little 210X and 215X seven-pound delights were right there in the Atlas lineup. A strange new company had come out of nowhere, and they were producing something called a Triton IV (now termed the 540 or 544) which sounded good. Ten-Tec was its name. A quick overview of the situation reminded me of what I had forgotten. These were the people that came out with the little modules and finally the QRP rig, the Argonaut with 5 Watts input. That did it. Over to the local radio emporium I went. What a display. There they were—the Kenwood TS-520S and the TS-820S, the Yaesu models, the Atlas, the ever-changeless Drake line, and the Ten-Tec 540. One by one, I listened to them all, but one was a standout: the Ten-Tec 540. Words fail me. It was like listening to pocket radios before walking into a high fidelity store for a demo. The receiver on the 540 was fantastic!

But, when I listened around the band, all I heard were TS-520s. What could I do? I took the plunge and bought a Ten-Tec 540, the CW filter, and the ac power supply. My ham life hasn't been the same since. My ham activity has skyrocketed.

It's been about 16 months since I first put the 540 on the air. The first thing I noticed was the absence of warm-up. Press the button and the machine speaks. The single-conversion receiver has a bandwidth of 2.7 kHz, which gives none of the squeezed audio that is often apparent with narrow designs. One overlooked factor comes in the audio distortion spec. Every receiver on the market has a 10% distortion allowance, but not the 540. It has 2%, or 1/5, the amount of unpleasant noise to listen to along with the signal. That makes a big difference when you are on the air for over an hour or so. The 540 has a little 2" speaker located in the center of the bottom of the unit that outperforms two separate outboard speakers that I've tried so far. The receiver and the transmitter are not tied together as they are in most of the transceivers on the market. Peaking up or detuning the receiver doesn't affect the transmitter at all. Using the remote vfo doesn't automatically mean that the further you go from the transmit frequency, the more your receiver is off resonance! That's quite a remarkable feature of broadband design, especially if you are a DXer. Stable? You bet. 10 Hz allowed by the specs per hour hardly makes it worth mentioning. The sensitivity is really closer to .2 μV instead of the .3 that is advertised.

The standard for most units is .5 μV. The receiver is quiet. The absence of the ac supply from the unit and the lack of tubes all make a contribution here.

The transmitter does as well as the Swan 350 with its 400 Watts input. The Ten-Tec 540/544 has 200 Watts input on all bands and all modes including CW and RTTY. Output is about 100 to 110 Watts. I have had many, many QSOs on crowded bands that have lasted 45 minutes to an hour with the Ten-Tec. The reports all indicate good audio and a lot of punch to the SSB signal.

It really does get out smoothly and superbly. I did buy a DenTron Super-Tuner to match the 540 to my old inverted-vee dipole. The swr bridge is built right into the 540/544 so that, in the transmit mode, you can monitor swr without an external meter. I just reach over and touch up the knobs on the tuner while I'm transmitting if I change frequency very much. This past year, I worked Sweepstakes for the first time. What fun! I'd just go from one end of 40 meters to the other, hitting all the strong signals instead of sitting in one place with a kilowatt. The sprightly rig and that broadbanded design made it work. Many folks don't like contests and don't move around the band that much, but I do and it's nice to have the capability.

The features of the Ten-Tec are well chosen, making it the most versatile rig I've ever come across. Take the 25-kHz calibrator. It's pulsed so you can distinguish it from a carrier. WWV is obtainable on both 10 and 15 MHz. It's the only rig I know of that has that capability on two frequencies. For the CW man, there is a $25 filter for 150 Hz—that's right, a two-position filter. I tried another well-known outboard CW filter, and it didn't surpass this little wonder. The full break-in keying for CW is like having your sinus cavities open . . . wide! One fellow 540 owner told me that he thought his transmitter wasn't working until the station came back to him. You can listen to the band in between the dits on the number 5. There's more for the CW addict. The sidetone not only has adjustable volume, but there is also an adjustment for the tone over a full octave to beat off the wearies of listening to the same tone. Both adjustments are made through a hole in the bottom of the unit that doesn't require moving the unit.

If you work round tables, you know how vexing it is to wander around from one station to another, so the Ten-Tec people have incorporated an offset tuning control on the front panel . . . with a little LED to let you know when it's working. It has an effective noise blanker for any kind of impulse noise for an additional $29.

The back of the radio has all kinds of switches and plug-in possibilities. All of the plugs are available for phone patches, linear amplifiers, external receivers, external speakers, foot switches to activate the mike, and a plug to take the remote vfo or 160 meter converter.

The alc is adjustable on the front panel so you can reduce the power input to 75 Watts if you are on emergency power. The 540/544 is essentially a 12-pound dc-powered unit drawing 15 Amps on peaks, so it can function well on a 12-volt battery stuck in a corner of the shack for emergencies. Naturally, that 12 lbs. goes a long way toward making it an ideal mobile station. The dimensions are a bit larger than the Atlas 210X, but not nearly as great as many of the hybrid (tube-transistor) rigs on the market.

What about protection? Well, the radio is designed to shut down if you forget to put the antenna on or if the swr is too high. It doesn't blow a fuse; it just quits playing. That has gone a long way toward keeping the transistors in the final from requiring replacement. The factory said that they have only replaced 6 transistors so far in the thousands of units on the air around the world.

The service of the Ten-Tec people is outstanding. I started off with a used Triton IV, and, soon after I purchased it, the antenna relay stuck and I had to key the mike to get it to go back into receive. It wasn't a big problem, but it was annoying. I called the factory, and they shipped me a little circuit board via UPS that took 3 days to arrive. I sent the old one back. Even though the unit was way out of warranty, they made that swap at no expense to me. There are ten circuit boards in the unit that are all field replaceable. The rig is sure easy to service. There are no high voltages to induce a healthy fear in the amateur. The layout is clean, neat, and simple to get at. The manual is a joy to read. Every circuit board is clearly described and defined.

The Ten-Tec 540/544 is one of the finest, most versatile HF rigs I've ever seen and easily the best radio that has ever graced my ham shack. Over the months that I've been on the air with it, I've listened to many other amateurs operating this particular piece of equipment. They have experienced the same service that I've experienced from the factory, and they are uniformly delighted with their good fortune. ■

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After reading Mr. Johnson's home brew phone patch article (D.H. Johnson, "Phone Patch Tips," *73 Magazine*, July, 1977, p. 138), I thought I might throw my hat in the ring, too. I built this phone patch into an old desk model extension phone several months back and it has worked great from day one. In building it, I discovered some very useful hints I'd like to pass along.

Before building or buying a phone patch, I had a few basic criteria to meet. First it had to be cheap! Also, I didn't want VOX—it costs more and its features appealed to me less. With VOX, the beginnings of sentences sometimes tend to be clipped off. Being picky, I preferred the more natural sounding voice. Since I had to monitor the QSO and add 10-minute IDs anyway, I opted for manual control of transmission and receive. Installation of a small SPST switch to control my Drake T-4XC push-to-talk (transmit relay) circuit would allow the person on the phone to talk without receiver noise being present. Any transceiver or transmitter/receiver combo should be able to accept this simple switch, allowing hassle-free communication.

Once the decision had been made, I went to work drawing on paper what I needed and then scrounging in my junk box for the parts. Being a recording engineer, I found one small low-to-high impedance transformer, some audio cable, and all the plugs and jacks (audio-type) I needed. A quick trip to the neighborhood electronics shop took care of the rest.

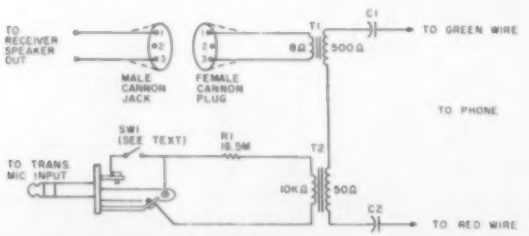


Fig. 1. Phone patch schematic.

Construction

The phone patch schematic is shown in Fig. 1. The phone line impedance is about 600 Ohms. It makes sense to match that impedance as closely as you can because doing so will yield excellent fidelity from the phone mouthpiece. Since I had one transformer with a low impedance side of 50 Ohms, I connected, in series with it, another transformer with a 500-Ohm side. Figuring 550 Ohms to be close enough, I let it go at that. Then I connected up one capacitor in series with each "hot leg" of the phone. This gave me isolation from any dc. I found that 3 uF was a good choice for fidelity reasons. This side of the circuit was then permanently connected to the phone inside the phone cover. I'd like to add that there have been no problems with this permanent arrangement and one could easily put in a switch to disconnect it if desired.

The other side of each transformer was hooked up to its respective device. The high-impedance (10k) leads went to the mic input of the transmitter and the low-impedance (8-Ohm) side went to the speaker output of the receiver. For the speaker, I ran speaker cable connected in parallel to the speaker output of the receiver, soldered on a male Cannon connector, mounted it in a small metal box I had handy, and attached it to the front of my ham desk. It's very accessible. I then soldered a female Cannon plug with about 3 feet of wire to the 8-Ohm side of the transformer. Thus, whenever I want the receiver audio in my phone, I simply plug the Cannons together. I made a plug which, when inserted in the mic jack of my Drake, connects together both the audio wires from the transformer and the two wires leading from my trans/receive (PTT) switch mounted in the phone cover. (For Drake, PTT amounts to shorting out ground and ring on the plug for transmit. I presume most ham PTT functions can be switched in and out similarly.) Cable for the mic section of the phone was good shielded cable. Its use prevented any possible hum from entering during transmission. I recommend always using shielded cable for high-impedance applications in audio.

Originally, the 16.5-megohm resistor (made from a 10-megohm and a 6.5-megohm in series) wasn't part of my plan. Without it, however, I cleverly discovered the phone mouthpiece would *clip* the input of the transmitter. Turning down the transmit gain didn't stop the distortion. Instead, I made the phone yield the same output voltage characteristics as my Shure 444. By inserting the resistor, I had *no* distortion and excellent voice quality. Hooray for carbon mics!

Results

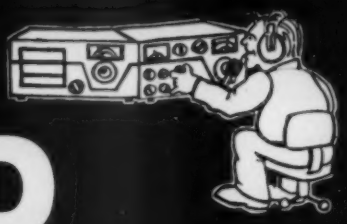
The very first day I assembled my phone patch I had the opportunity to use it. There was a ham in Iowa who wanted to patch into Glendale, California. I answered his CQ Glendale, and he explained he wanted to talk to a sick friend who had almost died from illness a week earlier. I made the patch without hesitation. When the call was done, I received many compliments from both sides, thanking me for helping out. I felt extremely good to have participated in what was a very happy occasion for all.

I later made some on-the-air tests for voice quality. Nothing but compliments came from all those who heard me testing. Many times people couldn't tell the difference between my phone and my Shure! Having the ability to hook up my receiver to my phone (without the transmitter) is nice, too. When I hear something interesting, I call up a friend, plug my phone into my receiver, and we both listen. I might add that I find the transmit switch arrangement very convenient. All communications are done with the phone handset. Since my transmit switch is mounted on the phone, my left hand holds the handset, and my right hand switches the trans/receive switch. Those of you inclined to mount the switch in the handset could pull off one-handed operation. Or, how about a footswitch?

The only change I've made was to add an on/off switch for my receiver. Now I can adjust the receiver gain in the phone to any level without the distraction of an outside speaker blaring away. Since then, I've been quite happy with my home brew phone patch. All in all, I spent less than five dollars. That's what I call cheap! ■

Underside view of phone with patch inside. The wire coming out of the uppermost part plugs into the Drake's mic input. The lower wire plugs into the Cannon box below the electrical outlet (bottom of picture). The PTT switch is centered in the bottom of the front of the phone.

Longs suggests KENWOOD



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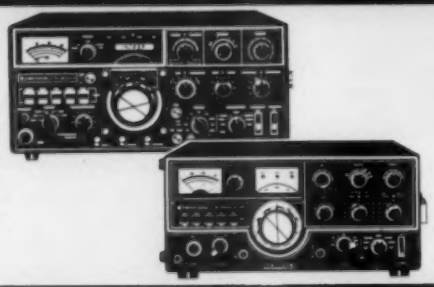


KENWOOD TS-820S transceiver

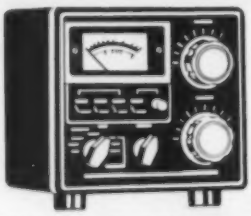
Features a factory installed digital freq. readout. • 160 thru 10 meter coverage • Integral IF shift • RF speech processor • VOX • Noise blanker • PLL • Built-in 25 KHz calibrator • CW side tone & semi-break-in • IF OUT, RTTY, & XVTR • Phone patch IN and OUT terminals.

1249.00 list. Call for quote.

KENWOOD TS-520S SSB transceiver

160 thru 10 meter coverage • Optional DG-5 frequency display • New speech processor with audio compression amplifier • Built-in AC power supply (DC-DC converter, optional) • RF attenuator • Provision for separate receive antenna & phone-patch.

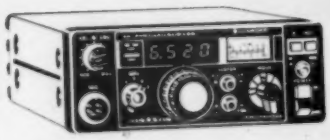
799.00 list. Call for quote.



KENWOOD AT-200 6 band antenna tuner

Features a through line watt meter, SWR meter, antenna selector switch, & antenna coupler. Freq. range 1.8 to 29.7 MHz. Through power 200W at max. connectors for UHF, wire antenna, & a dummy load.

159.00 list. Call for quote.



KENWOOD TR-7600 The radio that remembers

Full 4-MHz coverage (144.00-147.995), 800 channels, 10 watts RF output/1 watt low, memory channel w/simplex or repeater offset, & LED. With the optional RM-76 select any 2m freq., store freq., auto stop on first busy or open channel, scan memories.

375.00 list. Call for quote.

KENWOOD TR-7400A 2m FM transceiver

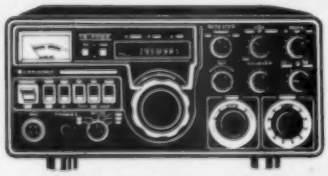
Features: • CTCS provisions, encode and decode • 25 watt output RF • Solid-state final stage • LED readout • PLL gives 800 discrete channels • Repeater offset circuit • PLL unlock protection circuit • MOS FET.

449.00 list. Call for quote.

KENWOOD TL-922A HF linear amplifier

Featuring a time delay fan circuit, freq. 160 meters to 15 meters, drive power 80 watts, SSB; 2000W PEP CW, RTTY; 1000W DC. Power req. 120/220/240 VAC. 50/60 Hz.

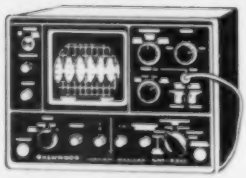
1199.00 list. Call for quote.



KENWOOD TS-700SP all mode 2m transceiver

Covers the entire 2 meter band. The features are SSB, CW, FM, AM and semi-break-in CW. Also side tone monitor, digital freq. readout, receiver preamp and 600 KHz repeater offset op (144.5-145.5 Hz) 10 watts RF output, AC/DC pow. supply.

759.00 list. Call for quote.



KENWOOD SM-220 station monitor scope

Features: built-in two tone generator, monitors SSB wave forms, helps adjust mic gain & speech-processor compression level & monitoring key clicks on CW, tests linear amps, observes signals transmitted from 1.8-30 MHz.

349.00 list. Call for quote.

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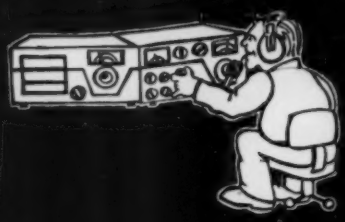
Longs suggests YAESU



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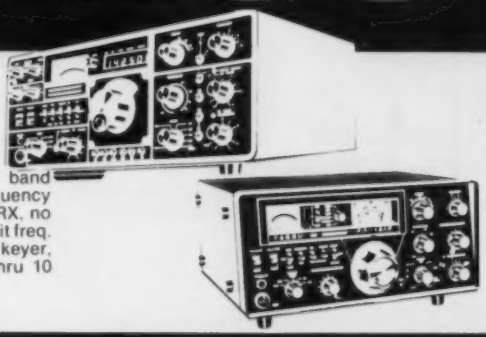


YAESU FT-901DM HF transceiver

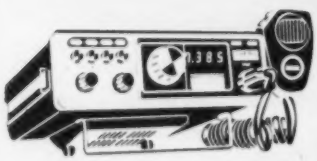
Reject tuning, variable IF band width tuning, audio peak frequency tuning, LED w/memory TX/RX, no external VFO required for split freq. operation, built-in Curtis keyer, 6146B final tubes, & 160 thru 10 meter coverage.

1459.00 Call for quote.

YAESU FT-101F transceiver

- Coverage: 160 thru 10 meters
- Built-in AC/DC power supplies
- Built-in RF speech processor
- 260 watts PEP on SSB, 180 watts on CW, 80 watts on AM
- Solid-state VFO
- VOX
- Auto break-in CW sidetone
- WWV/JJY reception
- Heater switch.

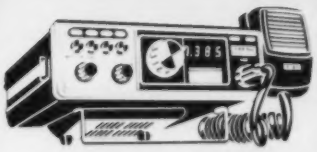
799.00 list. Call for quote.



YAESU FT-227RA

One knob channel selection for 800 channels, frequency 144-148 MHz, 4-digit LED readout, fully synthesized frequency control, selectable 10 watt Hi/1 watt Low output, 4 memories, touch control on mic for scanning, scan selectable for clear or busy channels.

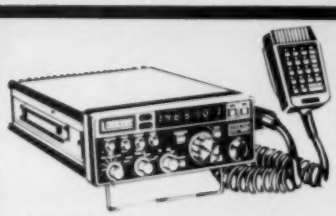
399.00 Call for quote.



YAESU FT-227R "Memorizer"

- One knob channel selection using optical sensing to select 800 channels
- Memory circuit allows instant return to any frequency between 144-148 MHz
- 4-digit LED frequency readout
- Fully synthesized frequency control
- Selectable 10 watt HI/1 watt LOW output with one memory.

385.00 Call for quote.



YAESU CPU-2500RK 2m FM transceiver

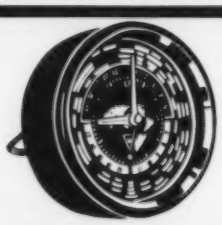
Full 4 MHz coverage in 5 KHz steps 144-148 MHz • 4 memory channels may be programmed • Built-in scanner • keyboard mic allows for remote control of memories & dial frequencies • Also serves as an auto patch encoder • Power output 3 watts/25 watts.

585.00 list. Call for quote.

YAESU SP-101PB speaker/phone patch

The SP-101-PB features: • A shaped response speaker from 300 to 3000 Hz • Built-in hybrid phone patch with individual gain controls • VU meter. Full VOX operation • Receiver input impedance: 4 or 600 ohm • Output impedance: 600 ohm or high impedance.

67.00 Call for yours today.



YAESU QTR-24 world clock

Features world time at a glance. Time in any principal city or time zone can be coordinated with local time on a 24-hour basis. The Time Zone Hour Disc automatically retains the correct time. Uses one "C" battery.

35.00 Call for yours today.

YAESU FT-202R 2m handheld FM transceiver

1 watt output min., 6 channel capability, flexible helical whip antenna, tone burst, compact size and light weight, S-meter and battery condition indicator, operates on NiCad or dry cell batteries, built-in speaker-mic.

199.95 Call for quote.

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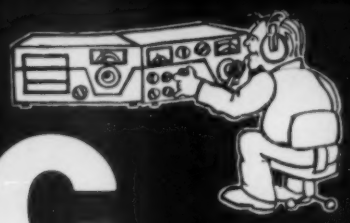
Longs suggests TEN-TEC



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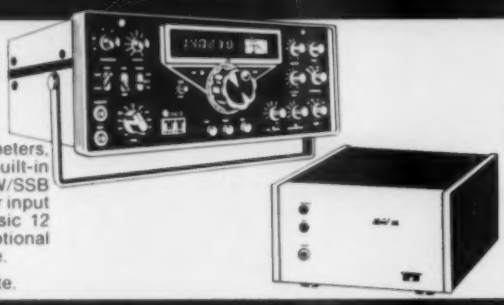


TEN-TEC Omni D transceiver

Totally solid state, 160 to 10 meters, LED readout, VOX and PTT, built-in squelch, built-in 4-pos. CW/SSB filter, 2 speed break-in, power input 200W, 100% duty cycle, basic 12 VDC operation, and more! Optional power supply 252M available.

1069.00 list. Call for quote.

TEN-TEC 252M power supply

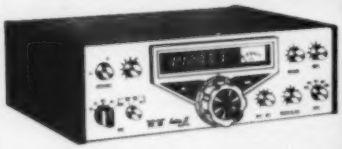
The 252M features: solid state circuitry with built-in metering, input 117 VAC, 50-60 Hz, output 13 VDC plus or minus 0.5V, regulation: better than 1% NL to FL at 117 VAC, current 0-18 amps.

119.00 list. Call for quote.

TEN-TEC Century 21 CW transceiver

Features: • Full break-in • 70 watts input • Solid-state • Built-in speaker • Receives CW or SSB • Instant band change • Offset receiver tuning • Overload protection • Sidetone with adjustable level • Regulated power supply • 80 thru 10 meters with crystals supplied.

299.00 list. Call for quote.



TEN-TEC 544 digital HF transceiver

The 544 features: • 3.5 to 30 MHz coverage • Solid-state • Instant band change • 8-pole crystal IF filter • LED digital readout • 200W input on all bands • WWV at 10 & 15 MHz • Full CW break-in • "S" meter and SWR bridge • 100% duty cycle, full power for RTTY & SSTV.

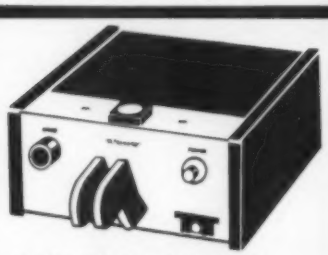
869.00 list. Call for quote.

TEN-TEC project boxes

A complete line of modern enclosures to give your handcrafted gear professional appearance. They are high impact polystyrene with a brushed aluminum front.

ME-10	4½" x 10-3/16" x 6-9/16"	14.00
DE-8	4½" x 8½" x 10-3/8"	18.50
DE-14	4½" x 13¼" x 10¼"	25.00
JE-5	2-9/16" x 4-15/16" x 6"	7.00
JE-10	2-9/16" x 10-3/16" x 6-9/16"	14.00

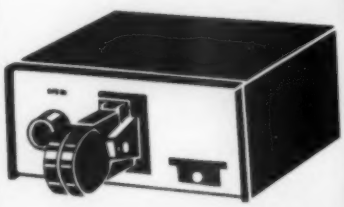
Order yours today.



TEN-TEC KR-50 electronic keyer

• Speed range: 6-50 wpm • Weighting ratio range: 50-150% of classical dit length • Output: reed relay, contact rating 15 VA, 400 V max. • Sidetone: 500 Hz tone • Dit & dah memories with defeat switches.

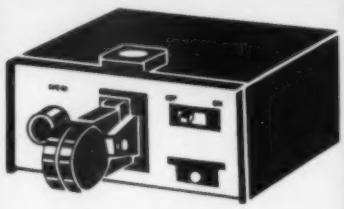
110.00 list. Call for quote.



TEN-TEC 670 keyer

This is a solid state electronic keyer made especially for use with the Centry 21 CW transceiver. It has adjustable speed.

29.00 Call for yours today.



TEN-TEC KR-5A electric keyer

For portable, mobile or fixed stations • Reed relay 15 V-amp contacts, 400 V max. • 6 to 50 WPM • Self-completing dits & dahs • Dit length increased approx. 10% @ 20 WMP.

39.50 Call for yours today.

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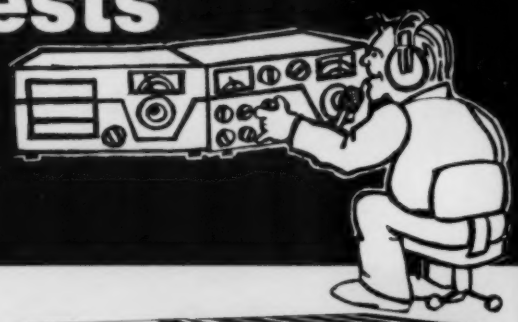
Longs suggests ICOM



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ICOM IC-701 HF transceiver and power supply

All solid state, even the finals, 100W continuous duty on all bands, all modes, 160 thru 10 meters, dual built-in individual digital VFO's for split freq. operation, VOX, semi-break-in CW, RIT, AGC, noise blanker, & built-in RF speech processor. Includes IC-701 PS (AC power supply).

1700.00 list. Call for quote.

ICOM IC-280 remotable 2m FM mobile

Frequency 143.90-148.11 MHz • Power: 10 watts Hi, 1 watt adj. Low • Power requirements: 13.8 VDC at 2.5 amps • Main PLL control head may be detached and remotely mounted • With microprocessor, stores 3 frequencies • Easy to read LED's.

480.00 list. Call for quote.

ICOM IC-402 432 MHz SSB & CW portable

Frequency range 430-435.2 MHz in any 200 KHz bands • Power output 3 watts PEP SSB • CW, USB, LSB • Receiver sensitivity 0.5 UV at 10 dB SINAD. Provisions for external antenna & power sources • BC-20 NiCad battery pack & charger optional 49.95.

499.00 list. Call for quote.

ICOM IC-215 2m FM transceiver

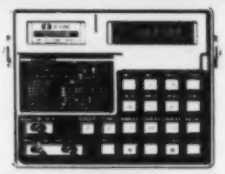
Features: • 15 channel capacity • MOS FET RF amplifier & 5 tuned circuits in the front end for optimum sensitivity and selectivity • S-meter on front panel • Dual power level, 3 watts HI for long distance, 0.5 watt LOW for local • Uses C batteries or rechargeable cells.

239.00 list. Call for quote.

ICOM IC-202S 2m SSB portable

The IC-202 features: • Frequency coverage: 144-146 MHz • Modulation: A3J and A1 • RF output power: A3J 3 watts (PEP), A1 3 watts • Sensitivity: 0.5 microvolts at (S+N)/N 10 dB or better • Includes a true IF noise blanker • Requires "C" batteries or external 12 volt source.

379.00 list. Call for quote.



ICOM RM-2 microprocessor keyboard

This is a touch tone unit adaptable to the IC-701, IC-211, and the IC-245. It permits selectable scanning up or down, has four memories, a LED display, can program split freqs., and also serves as the touch tone pad for the IC-211 and the IC-245.

199.00 list. Call for quote.

ICOM IC-502 6m SSB, CW portable

The 502 is a 6 meter SSB and CW portable with telescoping antenna & hand mic. • Frequency coverage: 50 to 51 MHz • Modulation: A3J and A1 • RF output power: A3J, 3 watts PEP and A1, 3 watts • Sensitivity: 4 microvolts for 20 dB quieting • Virtually no intermod.

269.00 list. Call for quote.

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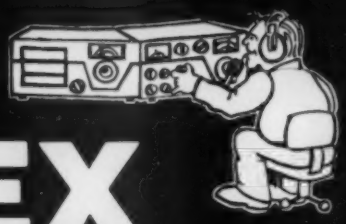
Longs suggests VIBROPLEX



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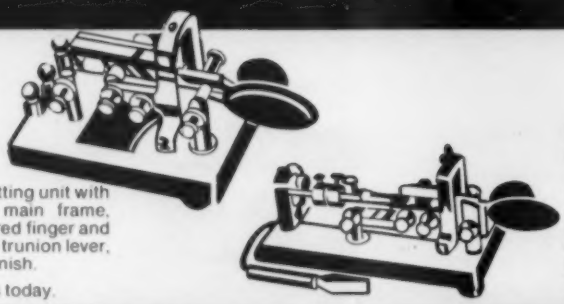


VIBROPLEX vibro-keyer standard

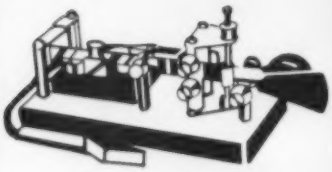
An electronic transmitting unit with large size contacts main frame, super finished parts, red finger and thumb pieces smooth trunion lever, adjustable standard finish.

46.50 Call for yours today.

VIBROPLEX "The Original" deluxe

Can be sloed to 10 WPM or less or geared to a high rate of speed keeping high quality signal. Deluxe model-polished chrome w/jeweled movement & grey base.

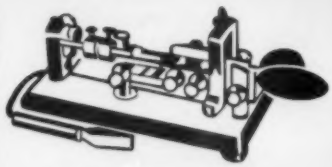
59.95 Call for yours today.



VIBROPLEX Lighting Bug Keyer deluxe

For high quality signals at all speeds use this flat pendulum model. The deluxe has a polished chromium base and top parts with a grey crystal base with a jeweled movement.

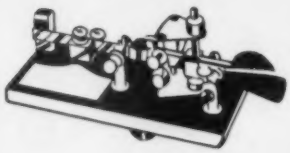
59.95 Call for yours today.



VIBROPLEX Presentation Super deluxe keyer

The finest bug ever built with 24 K gold-plated base top, patented jewel movement. It has a wider range of speed because the jewels in the movement reduce friction and maintain smoother operation.

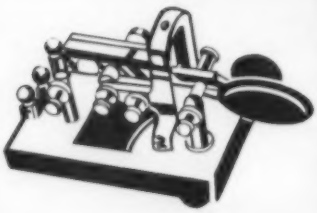
72.50 Call for yours today.



VIBROPLEX Champion standard keyer

Heavy base to prevent walking, grey crystal base with chromium finished top parts. Without circuit closer the keyer gives smoother even operation and a wide range of speeds.

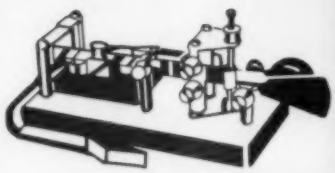
46.50 Call for yours today.



VIBROPLEX vibro-keyer deluxe

An electronic transmitting unit with large size contacts main frame, super finished parts, red finger and thumb pieces smooth trunion lever, adjustable. Deluxe finish.

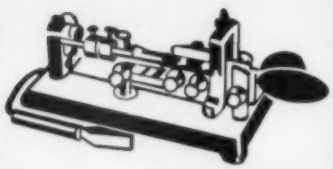
58.50 Call for yours today.



VIBROPLEX Lighting Bug standard keyer

The standard model gives you the same high quality signals at all speeds using the flat pendulum model. It has polished chromium top parts and a grey base.

49.95 Call for yours today.



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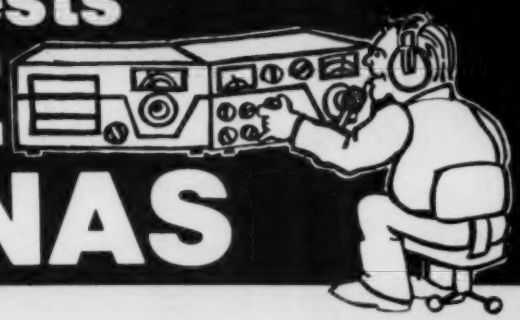

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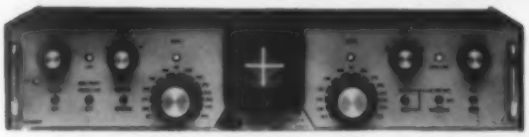

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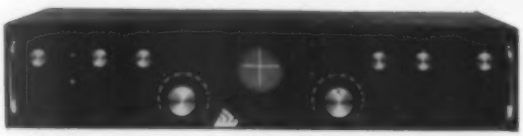

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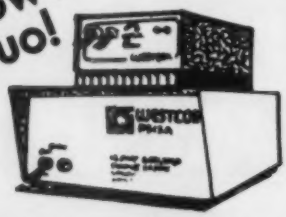

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100 watts	100H	100A	100B	100C	100D	100E
250 watts	250H	250A	250B	250C	250D	250E
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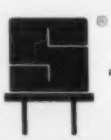

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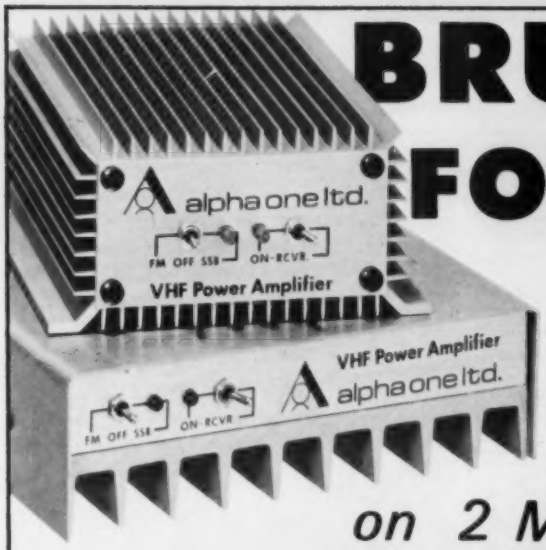

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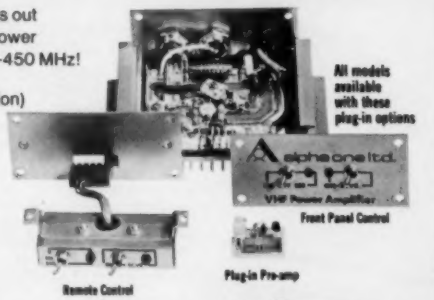

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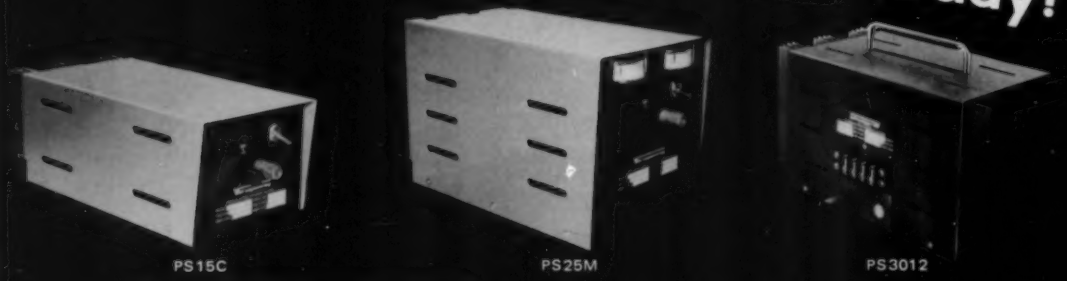

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The Filcher Foiler Revisited

— vehicular protection

The best news for hot rods since the green light.

After reading Mr. Helvey's article ("Filcher Foiler Car Alarm," *73 Magazine*, Dec., 1977), I decided that it was just what I needed to protect my old Ford hot rod with its chrome-plated engine, dual quads, custom gauges, etc. Being a middle-aged hot-rodder in a neighborhood full of fifteen-year-olds will almost always ensure a good-sized audience for my car projects. This day was no exception.

The first thing I did was purchase all the required parts, including the door switches. Upon completion of one door jamb, I overheard a supportive ten-year-old telling his older brother in no uncertain terms that, no, Mr. Davis wasn't crazy, and, yes, it was undoubtedly going to be faster with dual light switches! After pretending (?) to go berserk and chasing all the youngsters away, I went inside to reread the article and see just why I was installing another set of door switches.

The very first thing I discovered, which was incidental to my quest, was that the relay as shown is not in a true latching-type configuration. The next thing I discovered is that most vans don't have door switches for the courtesy lights already installed. Hence Mr. Helvey's installation. Well, the Bondo job on the doorpost wasn't too difficult and neither is the new alarm system outlined here.

My hot rod and my Mustang were both wired the same, insofar as the courtesy lamps use switched 12 volts from the door switch while the other side of the lamp is grounded. Car manufacturers, however, being what they are, have probably made cars where the lamp is at 12 volts on one side and uses a switched ground on the other side. If your car falls in the latter category, simply reverse the grounds and 12-volt sources on the large schematic (not the two smaller alarm schematics), and reverse the polarity of diode D1. I have made provision in my system for hood and trunk switches; however, any number of extra switches may be used.

Isolation diode D1 has been included to prevent the courtesy lights from coming on when the trunk or hood switch is closed. The size of this diode is not very critical, but it should be at least 25 V piv and have a current rating capable of handling the relay coil. Notice the configuration of the latching circuit for relay K1. This corrected design ensures that the relay will latch by positively holding the relay closed for as long as a switch is closed, which will be more than long enough for the armature to contact its latching contact. Mr. Helvey's problem with the relay buzzing rather than latching is not due to a defective relay, but rather to trying to have the relay do something it wasn't designed to do.

Two different methods of activating an alarm device are shown in my schematic: 1) using the existing car horns, where the

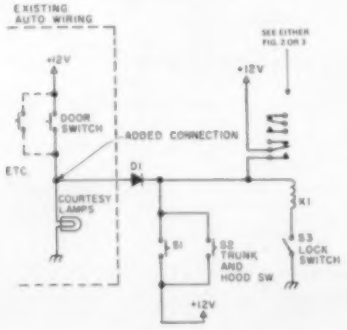

Fig. 1.

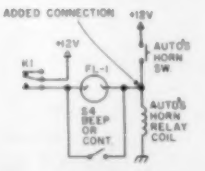

Fig. 2. For use with existing car horns with horn relay.

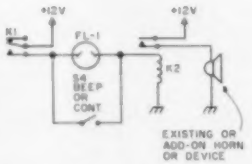

Fig. 3. For use with existing horns without horn relay or to use sirens, bells, or add-on horn.

horns are operated from a horn relay in the car, and 2) using the existing car horns where there is no horn relay (as in the case of most mid-60s Ford products) or for using a siren, bell, add-on horn, etc. Both above circuits are shown with a heavy-duty automotive flasher installed to provide a beeping alarm, rather than a continuous tone. A switch (S4) is included to change from beeping to continuous tone. If not desired, this feature may of course be deleted entirely, thereby eliminating S4, the flasher, and relay K2 from the circuit. K2 is required only because the large current drain of the horns will not permit the flasher to operate properly and will burn out the flasher very quickly.

One last note: Use only a 12-volt source capable of supplying high current (cigarette lighter, battery terminal, etc.), and use a heavy-gauge wire for all wiring. This will prevent an electrical fire, which in a car is very dangerous■

Parts List

D1	50 V 3 A silicon rectifier (Radio Shack 276-1141)	$ .69
FL1	Tung Sol 552 heavy-duty flasher (Auto Parts Store)	2.50
K1, K2	DPDT 12 V relay 10 A contacts minimum (275-208)	4.99; 9.98
S1, S2	Contact switch (for trunk and hood) (275-513)	1.49; 2.98
S3	SPST locking switch and key (275-511)	7.95
S4	SPST toggle switch (mode selection) (275-701)	.99

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Build An Economy Zener Checker

—versatile test rig

Why not do it right?

The device shown in Fig. 1 was developed to check zener diodes but it has also been found useful for other purposes.

With no load across the alligator clips, the panel meter will read about 50 volts. With a *silicon* rectifier across the clips, the meter will still read 50 volts for one position of the switch but only .6 volt for the other position. Note that the switch is cross-connected to provide voltage reversal across the diode.

When the alligator clips are connected to a *zener* diode, the meter will read .6 volt for one position of the switch, but for the other position it will read the rated zener voltage up to a maximum of 50 volts.

A third use is to check the total forward voltage across a string of series-connected rectifiers without applying power. This would be about .6 volt per rectifier. This check could not be made with most VOMs because their ohmmeter source voltage is not high enough.

This device *should not* be used to check *germanium* diodes unless the supply voltage is reduced. This can be done by forward biasing a silicon rectifier to obtain a .6-volt source. Then the germanium can be connected across the .6-volt source in both forward and reverse directions to see if the meter reading will drop to .2 volt in the conducting direction.

A 50-volt panel meter is probably optimum for this checker. However, other voltages could be used if the values of R1 and R2 are changed■

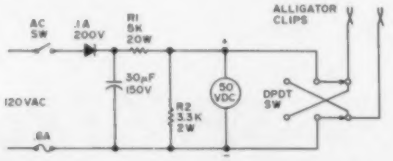

Fig. 1. Zener checker schematic diagram.

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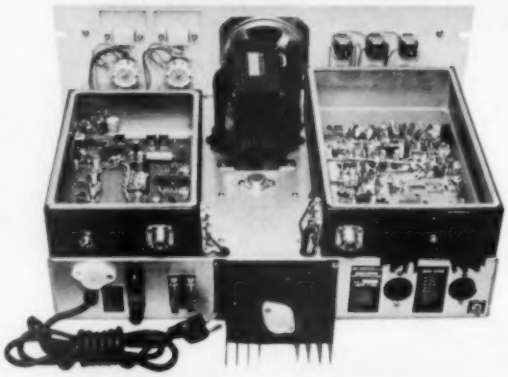

Rear View of SCR1000
Receiver—Left. Transmitter—Right.

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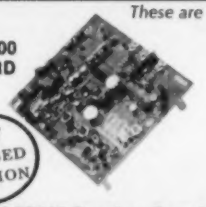

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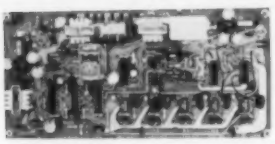

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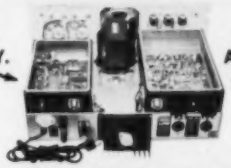

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Alaskan Adventure

—stalking the elusive KL7

If you crank up your perseverance, you can WAS.

Yep, I got Alaska! After a solid year of frustration, anxiety, and keen disappointment, I finally corralled a KL7 station.

I believe *Reader's Digest* said that Alaska has something like thirty-seven million acres of land, and the *Callbook* shows something like fifteen hundred amateur radio stations having KL7 calls . . . so it looks like getting Alaska would be about as hard as hitting Texas with a seven and a half gallon hat.

Well, believe me, it ain't! The first thing I did was set up a sked with a station at the North Pole. I had already worked Hawaii and Australia, plus a few other DX points of interest, so, with a sked, things would be easy and I could spend more time on Delaware and the Dakotas. But the sked just didn't come off as expected . . . three times each week KL7IUM and I would toss CQs back and forth at each other, but none of them made connections in a faithful six months of effort. One by one, the other states came dropping in until I was down to Delaware and Alaska . . . and try as I would, I just couldn't find the range.

A funny thing happened on the way to WAS, however . . . I was glued to the CW bands, and one day I heard a CQ that ended: "CQ, CQ, CQ de LA WARE!" I went back to him, not being sure where LA was, nor what country had calls without numbers. The *Callbook* said that LA was Norway, but they had a number after the "LA" . . . so I assumed I had read 3 into a W . . . missing a few dits in the translation. Could happen! So I called and called . . . no reply. Then I told my friend WB5WDD about it, and he said he had heard the same station but couldn't get it to come back. We agreed it was Norway . . . and let it go at that. Finally I landed a Delaware station, and it was then and only then that I realized the CQ I heard was FOR Delaware and not FROM Norway. It could happen to anyone!

But, after concentration on Alaska, I began to hear a few KL7 stations . . . one of them coming in quite clearly on a Sunday afternoon. He called CQ South America, so I waited through several of his calls until finally I assumed he would not get his desired station. Then I called him and anxiously awaited his return call. It came like this: "Can't you hear? I am calling South America!" So there was lesson number XX on CQ courtesy . . . but I kept listening and dialing. One evening I heard a truck driver, mobile in California, rag chewing with a strong KL7 station . . . so I waited . . . and waited . . . and waited . . . not daring to holler "break" after the previous experience. They gabbed a good half hour, and the truck driver, who evidently had not read the book on ham courtesy, either, closed by saying, "I have a buddy tuned in on us now that would like to have a word with you . . . so I'll be . . . etc., etc." And the buddy took over until the band closed! Well, it was important . . . the buddy was trying out a new rig, and he wanted the opinion of this stranger in Fairbanks on whether he should buy the rig or not!

Finally, in desperation, I decided that the next KL7 I heard would either pitch me out on my ear . . . or QSL! And then it came . . . again, a strong station in KL7-land hooked up with a California ham . . . and I sat through the usual routine of statistics before timidly shouting "break" plus other pertinent data that I thought would get

me through. There was a short silence and KL7 said, "I believe we had a breaker . . . come on in, breaker!"

Here was the chance I had been so long waiting for . . . and behold, my voice almost failed me! Finally I got it out: "KL7ABC, this is WB5WDG, Muskogee, Oklahoma. Do you copy?"

There was an exciting few seconds of dead silence, and then California said, "I believe he is calling you, KL7."

Then KL7 said, "No, I think he was calling you." and with that, they went back to their aforementioned QSO and never paid me another bit of attention. I snapped off the rig, snapped at my XYL, and told her where they could put Alaska if Russia ever wanted her back . . . and went to bed, only to roll and toss and count caribou, grizzlies, fjords, and permafrost.

But the final blow came a couple weeks ago when KL7 came in quite clearly, slowly, and with a hesitating dahdididahdit followed by SA . . . so, naturally, I assumed that this was a Novice newly upgraded who was trying out his new wings. I went back to him in fear and trembling, hoping that this was it. And it was . . . he heard me and came back loud and clear. A real live KL7 . . . and he was answering my call . . . at last, the big hunt was over. I was so excited that I almost missed his QTH when he gave it as Ft. Bragg, North Carolina. He had been transferred from a military base in Alaska and was still using his KL7 call . . . the SA I had heard after the dahdididahdit was not an SA at all, but a four. Your ears hear what you want them to hear.

But enough of that stuff . . . quitting never gets it . . . and I just didn't quit. Quite by accident, I heard a QSO that ended identifying itself as having a treasured Alaska station as one of the participants. Again I waited patiently until it ended, and I swung in behind the finale with my call. Believe it or not, the KL7 answered.

At last, my luck had changed and I was ready to apply for my WAS award. His signal was strong . . . his fist was great . . . and everything was deathly quiet. He acknowledged my call, gave me his name, and then started with his QTH—just as a 4-land station with a million-Watt linear started his big CQ, almost knocking my cans from my ears. I ditted a few thousand times and he stopped just as the lad in Anchorage was telling me that he had to get to work, but would answer my QSL as soon as he got it. And that ended that . . . thanks to the million-Watter in orange country.

Only this time I was ready. This had happened to me before . . . many times . . . so I was prepared. While I was listening to the KL7 QSO, I was copying his data as he sent it to the former recipient . . . and even though Florida knocked the orange juice out of my coax, I was ready with the proper address and now have my QSL merrily on its way to Anchorage with an SASE enclosed!

Why didn't I refer to the *Callbook*? Well, this lad had already said that he was too new to be in the latest edition of the *Callbook* and he had to get his QSLs in care of his dad, who was in the book! Practice may not make perfect . . . but it helps. ■

NEW MFJ Dual Tunable SSB/CW filter

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Reader Service—see page 211

H. Lawrence Laupheimer K3FDL
4110 Fields Drive
Lafayette Hill PA 19444

The Last DXpedition

—"QTH hr is Purgatory"

What the devil is going on here?

This old-timer was one-in-a-million, with a personal history dedicated to amateur radio. He was the envy of operators the world over. He held more certificates than the average ham ever knew existed, was winner of numerous contests and citations from all over the world for amateur radio services above and far beyond the call of duty, and was designer and builder of practically every type of radio equipment from the spark-gap days on up. This old-timer had just expressed his last "73" along with his final "dah-dit-dah." In simple words, he died.

He awakened, feeling no pain, and discovered he was lying on a very comfortable, elaborate bed, in a gorgeous room which was permeated by the faint odor of burning sulphur. "Oh, brother," sighed the old-timer, "I knew this would happen to me. I should have been more careful to always stay within the legal bands. I knew I was wrong in using that 'California Kilowatt' so often, and I should not have worked those guys with the HS, XU, XV, 3W8, and 8F calls. Yes, I'm confined to eternal damnation!"

"Just a minute there, my friend. Don't be upset about what happened to you." Jumping from his bed, the old-timer found himself face-to-face with a man who was reddish of face and the epitome of sartorial splendor in his superbly tailored suit, bright red socks, and foot-long cigar. The old-timer could plainly see the horn-like protrusions, all polished and gleaming, near the top of the man's head, and even the shadow of a tail extended from his rear. "Allow me to introduce myself. I am lovingly called Satan by my many admirers and I welcome you to Purgatory. Now, don't get yourself all uptight about things you heard concerning me and my home from those narrow-minded people up there where you used to live. I've been given a bad press all my life, and I honestly don't feel I deserve such humiliating treatment. They don't like me up there for some reason, and they sure paint a black picture of Hell. Now, don't misunderstand me—it's Hell down here alright, but we still have plenty going for us, as you'll soon discover. Here, have a glass of 20-year-old bourbon, a fine cigar, and pull up a chair. Tell me all about yourself, you lucky man!"

Before the old-timer had time to collect his thoughts, Satan started in again. "Look, pal, I'm going to try to make you like it down here. Sure it's Hell, but just for openers, tell me what you like the best. Do you want a dozen or so beautiful, sexy gals—or maybe you'd like to become a millionaire? Is it just hunting, fishing, and yachting you like? Tell me what 'turns you on' and it's yours, absolutely free of charge, with no strings attached."

"Well, Mr. Satan," replied the old-timer, "up there I was one hell, oh, pardon me, of a ham radio operator, and I thought just maybe you'd have . . ."

"A ham radio operator!" screamed Satan. "Why the hell didn't you say so in the first place! Quickly, come with me." Satan then rushed the old-timer outside to a warehouse, unlocked the door, and said, "We'll start with your tower. Here's a nice medium height one of about 500 feet, OK?"

"Wow!" yelled the old-timer. "These are built better than the commercial towers up there. You sure there's no catch to this?"

"Aw, come on, pal," replied Satan. "Would I fool you when you're going to be my guest for quite some time? Why shouldn't I try to please you with the best of everything just to make you happy? Sure, it's Hell down here, as I said before, but we still have much more to offer a nice guy like you. Now, let's get some antennas up. How's this—a simple Christmas tree of rotary beams, simple 10-element beams for every band? I'll have them erected immediately."

"Yes, but what am I going to do for a transmitter and receiver?" queried the skeptical old-timer.

"Never fear, friend, Satan is here. Take a look and pick up any of these." Here was a room filled with every late model transmitter and receiver, all in sealed cartons. The old-timer was dumbfounded, as he had never owned any equipment that wasn't "home brewed."

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"Wait a minute, friend," said Satan. "Pick up a good linear while you are at it. And by the way," he whispered, edging over to the old-timer, "how about one of my special 'Satanic Kilowatts' that makes those 'California Kilowatts' up there sound like peanut whistles? Here's a great new 10 kW job.

"Sure, this is Hell, but answer me truthfully, did anyone up there ever offer a nice guy like you so much for free with absolutely no strings attached?"

The old-timer was absolutely at a loss for words. Having scrounged all his life for every dime to buy used parts to build anything he ever operated, he never dreamed he would be so fortunate as to have such magnificent appliances to operate for all eternity. "Let's get this set up!" yelled the old-timer. "I just can't wait to get on the air!"

"Certainly," said Satan. With a wave of his smoking hand, there was a loud clap of thunder and a puff of sulphur-ridden smoke, and the old-timer found himself in a shack fit for a king, with everything properly set up.

"Great, great, absolutely beyond belief!" cried the old-timer. I just don't know how to thank you enough. I'm going on the air to tell everybody up there the true story of you and your kindness, Mr. Satan. I'll tell them the absolute truth about the goodies you have to offer everyone. By the way, where do I plug in this magnificent equipment?"

"Well, my friend," replied Satan as he hastily headed for the door, "that's the hell of it—we have no electricity!"■

Randy Hoffman WB6WQN
991 42nd Street
Sarasota FL 33580

An Audio Morse Memory

—got a tape recorder?

Listen to your own fist—and learn.

The tape recorder decoder (Fig. 1) can be very useful and is easy to duplicate. It converts an audio signal to dc to key a relay. Code can be recorded on a tape recorder, then played back through the decoder, thus keying a transmitter, monitor, or both. Works just dandy for a "CQ" tape or a "CQ field day" tape. CW can also be recorded from a receiver and then played back to key your transmitter, letting a fellow amateur hear his own fist! A delayed test-transmission with a timer can also be arranged, allowing you to check signal quality from a friend's shack.

Parts List for Tape Recorder Decoder

Q1—For maximum sensitivity, a high-gain transistor such as a 2N447A (gain of 200) should be used. But any transistor of reasonable gain is OK (2N338, 2N3641, 2N3843, etc.). A PNP transistor can be used as easily by reversing the polarity at the battery and C3 (2N1307, 2N404, 2N408, 2N1025 with a gain of 100).

C1—.001 to .005 uF rf bypass.

C2—.1 to .25 uF disc ceramic, mylar, or electrolytic (6 V).

L1 — .5 H choke. A toroid is best because of its small size and low losses. The value is not critical and can be replaced with a 68- to 100-Ohm resistor, though performance is degraded slightly when demodulating low frequencies.

C3—1 uF to 2 uF, 3 V electrolytic.

T1—miniature transistor audio output transformer with primary of 8 Ohms (to match tape recorder output) and a secondary of 500 to 1000 Ohms.

D1-D4—1N34 or equivalent. Just about any small-signal, germanium diode will work.

K1—reed relay with 3- to 6-volt coil. A 10-Watt reed relay with coil can be bought at Lafayette Radio, or a range of relays, with and without coils, can be obtained at suppliers.

B—battery, 3 to 6 V.

None of the part values are critical. The volume control setting on playback and record will have to be adjusted to obtain the best results. Playback volume should be as low as possible to prevent background noise from causing odd clicks, or overloading from causing mushy characters.■

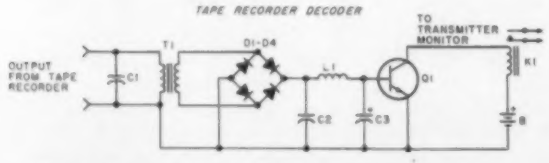

Fig. 1. Tape recorder decoder schematic diagram.

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Michael Black VE2BVW
16 Anwoth Road
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The Amazing Active Attenuator

— can you find a use for it?

The op amp is the answer.

I'm sure, by now, you have heard of many uses for op amps. But did you know that they can be used as attenuators? For some uses, they are better than attenuators consisting of only resistors. While the principle is very simple, I have not seen much mention of it in the various electronic magazines.

In an inverting op amp amplifier, as shown in Fig. 1, the gain can be varied from the open loop gain down to a gain of one. This gain is determined by the equation R_f/R_{in}, where R_f is the resistor from the output to the input and R_{in} is the resistor from the driving source to the input of the op amp (Fig. 1). Now, what happens if R_{in} becomes greater than R_f? To save you the trouble of running this experiment, the answer is that there is a loss from input to output and the circuit becomes what I call an active attenuator.

There are, unfortunately, some disadvantages to this attenuator. The first problem is that an active component, along with its associated power supply, is required. Also, frequency response is restricted to the bandwidth of this active component. Next, you must remember that this circuit inverts, so if you are using it for dc, you will get a negative voltage out if you feed in a positive voltage and vice versa.

Now, for the advantages. The output of this active attenuator, as in any op amp amplifier, is a low impedance (independent of resistor values). This means that any loading (within reason) c
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a non-inverting op amp amplifier has a minimum gain of one no matter what. Second, the input impedance is equal to R_{in}. So, when calculating the resistor values, choose R_{in} first, so that it is equal to the desired input impedance. Then choose R_f for the desired attenuation. Using this procedure, the resistor equation can be rearranged as $R_f = R_{in} \div$ desired attenuation. Also, make sure that the op amp is still useful at the desired frequency of operation. One thing that I am in-

response drops, so with an active attenuator, does the frequency response increase?

Well, I hope that you can put this information to use. I have not given too many details because most of the information required can be found in many magazine articles and books dealing with using op amps. I have found the *IC Op-Amp Cookbook* by Walter G. Jung (Howard W. Sams & Co.) especially useful. If you come up with some new data or uses for the active attenuator,

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INSTRUCTIONS

1. To adjust, remove a screw on each side and remove the cover. As viewed from the rear, left to right, there are 6 switches as follows:

#1 (Red toggle)	Set hours/month
#2 (Green toggle)	Set minutes/day
#3 Slide switch	Inhibit/run
#4 Slide switch	Spare
#5 Slide switch	Alarm select—UP alarm #2, DOWN alarm #1
#6 Slide switch	Display format—UP 24 hours, DOWN 12 hours

Note: In 12-hour mode, pm is indicated when 3 bars appear in the first digit position.

2. On initial light-off, all time functions will read 0:00, colon on or off, date will indicate 12 31, and seconds 00. To start the clock, momentarily place switch #2 (green toggle) in the advance position; seconds will start counting and the colon will flash. (Minutes may be set at this time if desired.)

3. To synchronize (to WWV or a time-tick), place switch #3 in its up position, stopping the clock as indicated by the absence of a colon and 00 seconds. At the instant of the "00 seconds" pulse from WWV or other time source, depress switch #3, restarting the clock.

Note: Step #2 must be performed first, after initial light-off.

4. Place function switch on LOCAL and set time:
   (a) To set hours, use switch #1 (red toggle)—UP advances; DOWN decrements; and MID-POSITION is the normal run position.
   (b) To set minutes, use switch #2 (green toggle) as in (a) above.

5. Place function switch on zone, alarm 1, or alarm 2, and set the desired time as in step 4(a) and (b). Repeat for each desired function.

6. Place function switch on DATE and set the desired date, using the #1 toggle for month and #2 toggle for the day.

Note: After the seconds have been initially synchronized, any and all times (and/or dates) may be changed at will. No further synchronization is required unless the timebase is gaining or losing time—or the clock is accidentally stopped when changing power sources.

7. To use the alarm(s), select the desired alarm with switch #5, and then place the front panel alarm switch to ON. When the alarm energizes, it may be stopped for 10 minutes by pressing SNOOZE, or by momentarily turning off the alarm switch. (A momentary turn-off rearms the alarm to energize at the designated time 24 hours later.)

Notes: SNOOZE inhibits the alarm for 10 minutes from the time it is pressed (not from the time entered), e.g., if the alarm is set for 06:00 and is "snoozed" at 06:03, it re-energizes at 06:13. This may be repeated indefinitely and makes the feature amenable for use as a 10-minute timer during long-winded QSOs. Also, if the display is blanked, the alarm feature will activate but will not sound off until the display is unblanked, if done within 1 hour of the time set. (Unless the snooze button is pressed, the alarm operates for an hour and then resets itself should the alarm circuit be on but the clock unattended.)

8. On the right side of the front panel are two slide switches which control the illumination level of the LEDs. The first blanks or unblanks the display; in the blank position, the alarm output is also made inoperative (see step 7, above). The second (outboard) switch controls the display illumination level: HI for daytime viewing and LO for nighttime viewing.

OPERATION

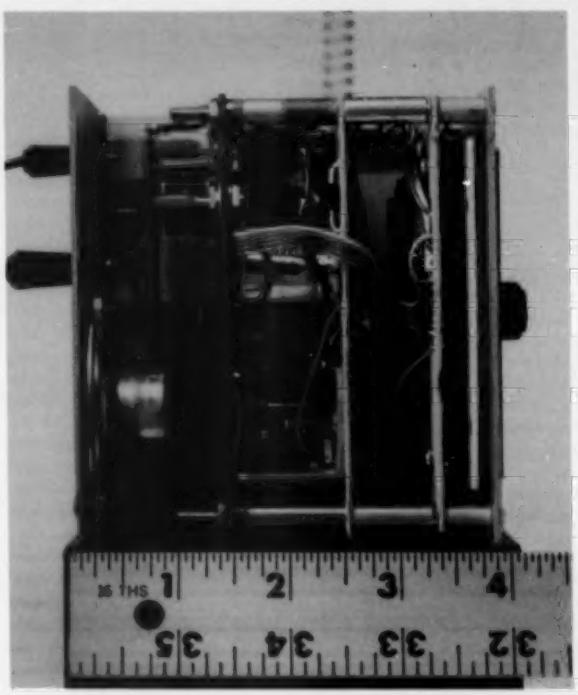
1. This clock is designed to operate from a number of power sources, 9 to 13 V dc or 6 to 9 V ac at the power input jack, without regard for polarity, or on a 9-volt transistor battery internally mounted. A small earphone-type jack is in parallel with the internal battery and may be used to (a) parallel the internal battery with an external battery while exchanging the internal battery, (b) provide a convenient test point for measuring the internal battery voltage condition, or (c) if necessary, be used as a recharge point for the internal battery.

2. The input to the power supply is a bridge rectifier which will accept ac or dc voltages of either polarity. A -5-volt regulator (7905) provides the LED voltage and a regulated 5-volt source for the internal crystal timebase. All circuits have been isolated from the case; therefore, it is safe to use this instrument in a car, using its battery connected to the power jack without regard to polarity. Caution: The shaft of the function switch is at circuit ground (+) and *must* have a plastic knob. Use of a metallic knob will invalidate the preceding statement.

3. The crystal timebase adjustment capacitor has been paralleled with a small piston-type capacitor to provide a "fine" adjustment, and is accessible via a small hole in the back skirt below the alarm speaker.

4. In operation, this unit draws current from the power source as follows:

7 mA — Illumination blanked
26 mA — Illumination LO
160 mA — Illumination HI



Battery version, top view.

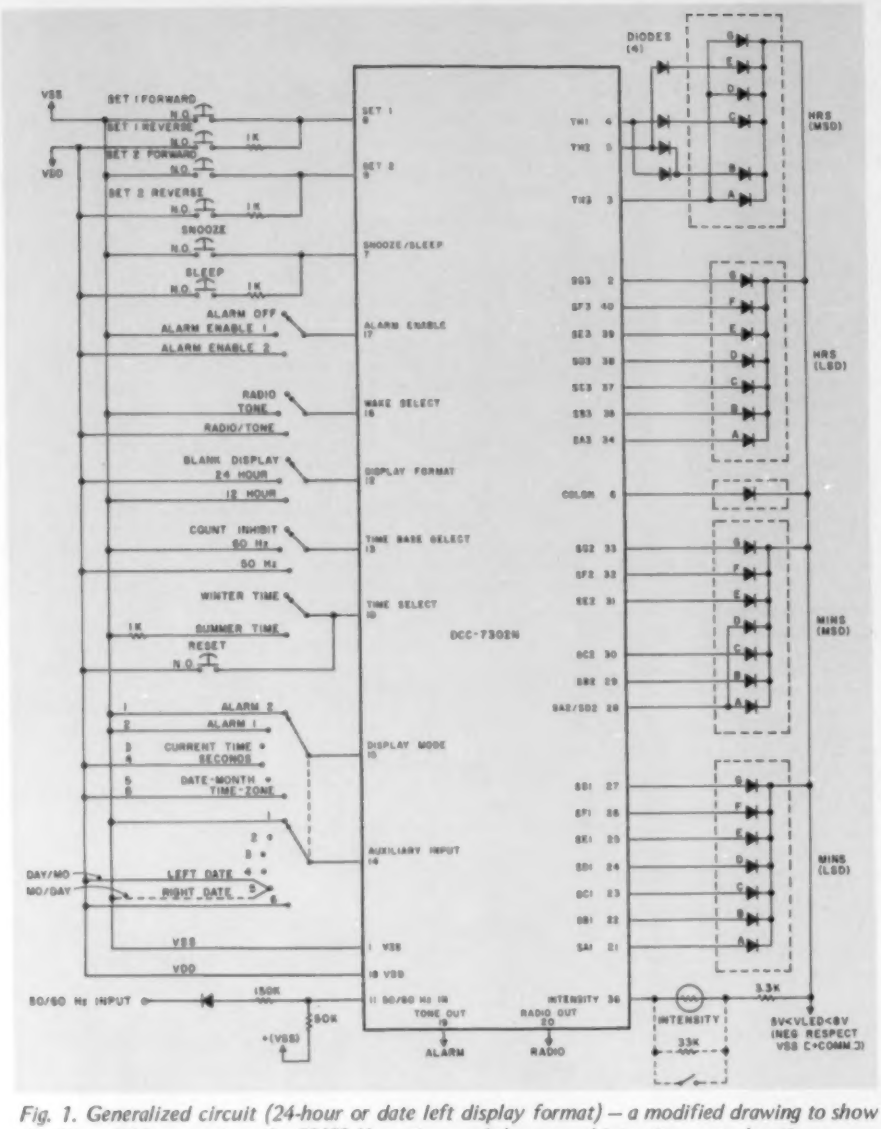


Fig. 1. Generalized circuit (24-hour or date left display format) – a modified drawing to show the 12- or 24-hour option, the 50/60 Hz option, and the manual intensity control option.

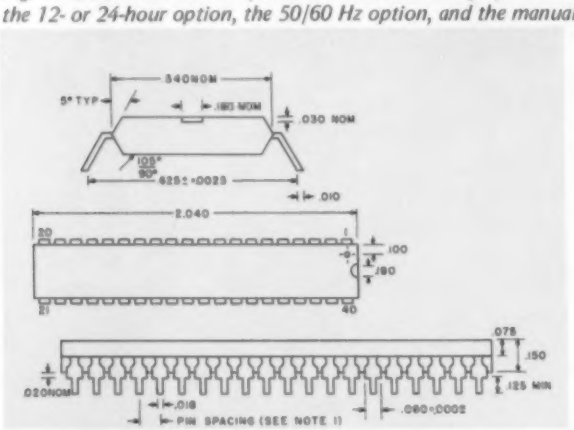


Fig. 2. The pin spacing is 0.100 between centerlines. Each pin centerline is located within ±.0010 of its true longitudinal position relative to pins 1 and 40.

or in foreign countries when you travel on 230/115 V, 50 or 60 Hz?

If you desire a clock with the above listed features, the DCC-7302N clock chip comes in a kit, available with fluorescent display, for about $30. In order to add options, read on. The chips are available for about $6.00 and an LED 4-digit display for about $10, or you can fabricate your own display from individual LED readouts.

I have produced 2 clocks around the 7302N chip. One is designed to operate from 115/230 V, 50/60 Hz power lines and includes many of the published chip options. The second is designed to be operated from either a battery source or a filament transformer – in this, a bonus was obtained when it was discovered that the clock will function nicely on 9 V or less, and the battery drain may be minimized by using low illumination or a blanked display as much as possible. Blanked, the total current is 7 mA; at minimum illumination, it is 26 mA, and, at maximum illumination, 160 mA (using a 9 V source).

The 115/230-volt version uses the power lines as a timebase and has most of my desired options, as indicated in the drawings.

The battery-operated version uses a crystal timebase sold by S. D. Sales, and several options were deleted to conserve on space and the number of switches required. A 7905 negative regulator IC chip is used in this unit to provide 5 V regulated for the timebase and the supply voltage for the LEDs.

Caution: Although these chips use a positive ground

Summer/winter time switch for Daylight Savings Time
Brownout indication
Four-year calendar
One time zone register

Would you like to use it independently of power lines, as well – possibly in your car

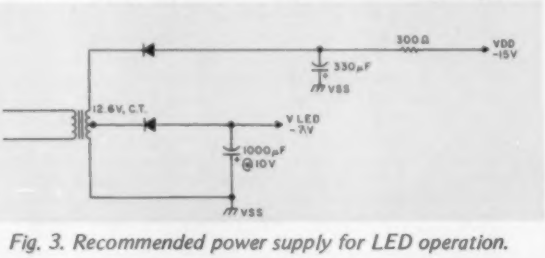


Fig. 3. Recommended power supply for LED operation.

(common), the LED display must be of the common cathode configuration.

PC Board Preparation

Lay out the circuits on graph paper, full scale, 10 lines to the inch, making a template. The template is then taped to the copper side of the PC board stock and each hole point lightly punched through the template. Remove the template and clean the copper with scouring powder and/or a steel wool soap pad, rinsing

Input function	V_{SS}	Open	V_{DD}	Aux input
Display mode	alarm 1	current time	seconds	open
Display mode	alarm 2	month-date		V_{SS}
Display mode		date-month	time zone	V_{DD}
Set 1	forward		reverse	N.A.
Set 2	forward		reverse	N.A.
Timebase select	60 Hz	count inhibit	50 Hz	N.A.
Display format	12 hour	blank	24 hour	N.A.
Wake select	tone	radio	Radio and tone	N.A.
Alarm enable	enable 1	off	enable 2	N.A.
Snooze/sleep	snooze		sleep	N.A.
Time select	summer	winter	reset	N.A.

Table 1. Input selection table.

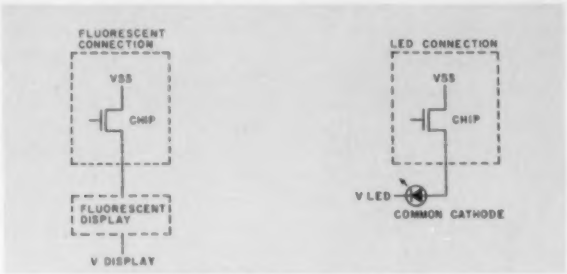


Fig. 4. Display connections.

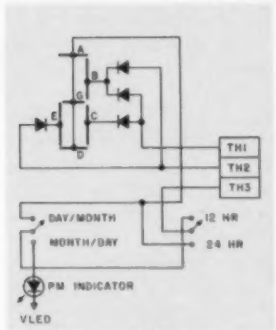


Fig. 5. Selectable 12-hour or 24-hour display.

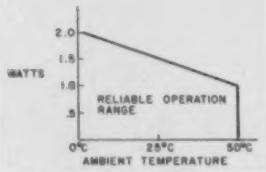


Fig. 6. Total chip power dissipation.

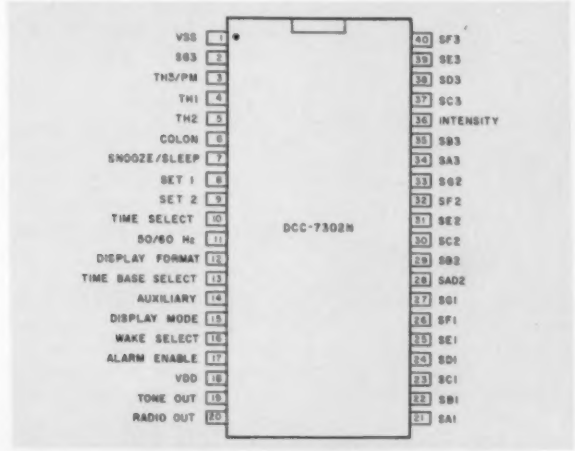
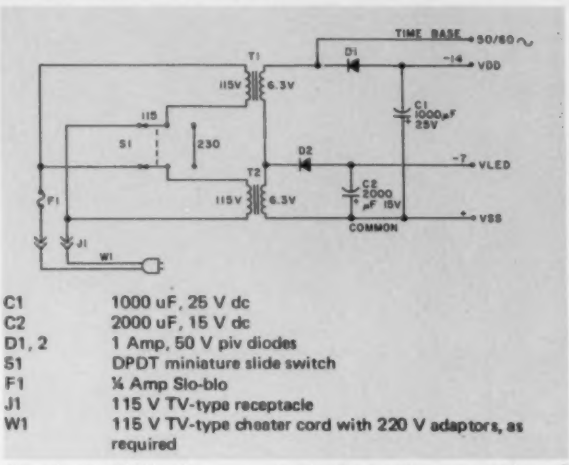
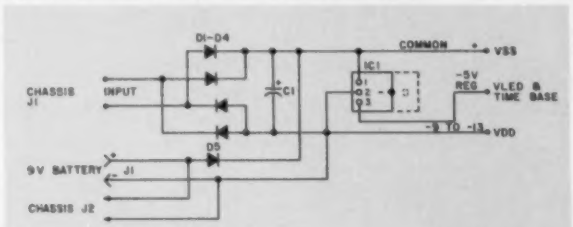


Fig. 7. Pin connections.



C1	1000 uF, 25 V dc
C2	2000 uF, 15 V dc
D1, 2	1 Amp, 50 V piv diodes
S1	DPDT miniature slide switch
F1	¼ Amp Slo-blo
J1	115 V TV-type receptacle
W1	115 V TV-type cheater cord with 220 V adaptors, as required

Fig. 8. 115/230-volt power supply. Note: there are at least 3 types of 230-volt receptacles in use in Europe.



C1	1000 uF, 15 V dc
D1-5	1 Amp, 50 V piv diodes
IC1	7905 -5 V regulator
J1	9 V transistor battery connector
Chassis J1	input jack, insulated from chassis
Chassis J2	input for auxiliary battery and small earphone jack, center positive and insulated from chassis

Fig 9. Less than 2 inches must separate the capacitor and the chip, or a second capacitor will be required across the chip input.

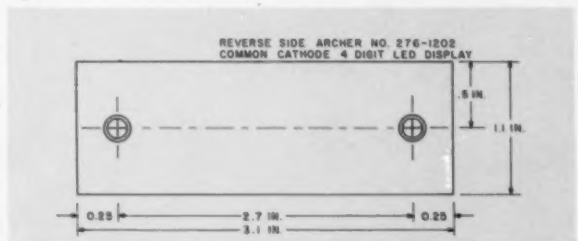


Fig. 10. Glue two spacers, 3/16" diameter x 1/4", i.d. tapped for #4-40 screws, to the two places shown. These spacers must align with the 2 holes in the main board.

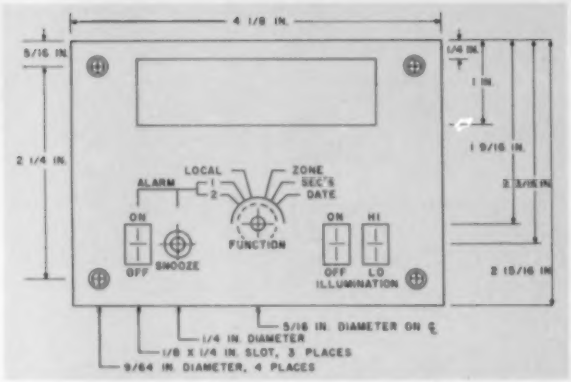


Fig. 11. Front panel dimensions and markings — battery version.

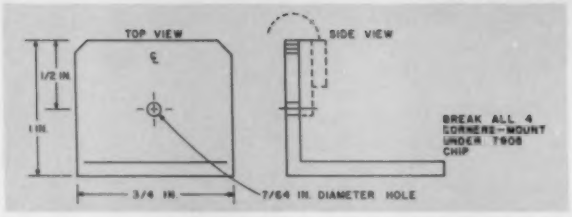


Fig. 12. Heat sink detail. Use 1" x 1" x 1/16" aluminum angle cut ¾" wide or fabricate it from aluminum or copper stock.

and drying each PC board thoroughly.

After the PC board is dry, use a wide-tip permanent marking pen and draw a wide line (about ¼") through all close-spaced contact points (20 on each side of the chip and others). Then, using a straightedge and a scribe, remove about 1/64" of the ink from between each of the contact points. Using a narrow etch-resist pen, draw a circle around the individual contact points (those separated by more than 0.1"), and connect the various contact points as indicated on the template. Use care not to soil the copper during this process. After all contact points have been correctly and properly connected, use the wide marker pen and fill in as much of the unused copper as possible to reduce the amount of copper that has to be etched off. This will speed up the etching and prolong the life of the etchant. In the battery version, remove the copper around the corner holes and the function switch mounting hole.

Etch the PC boards with your favorite etchant.

Note: There are several permanent marking pens on the market that will satisfactorily perform as etch-resist pens: EI Marko™ and Marks-a-lot™ are examples that have been used here. If in doubt, try your favorite on a scrap of PC board. These pens are much less expensive than the etch-resist pens available from your friendly Radio Shack or other dealer.

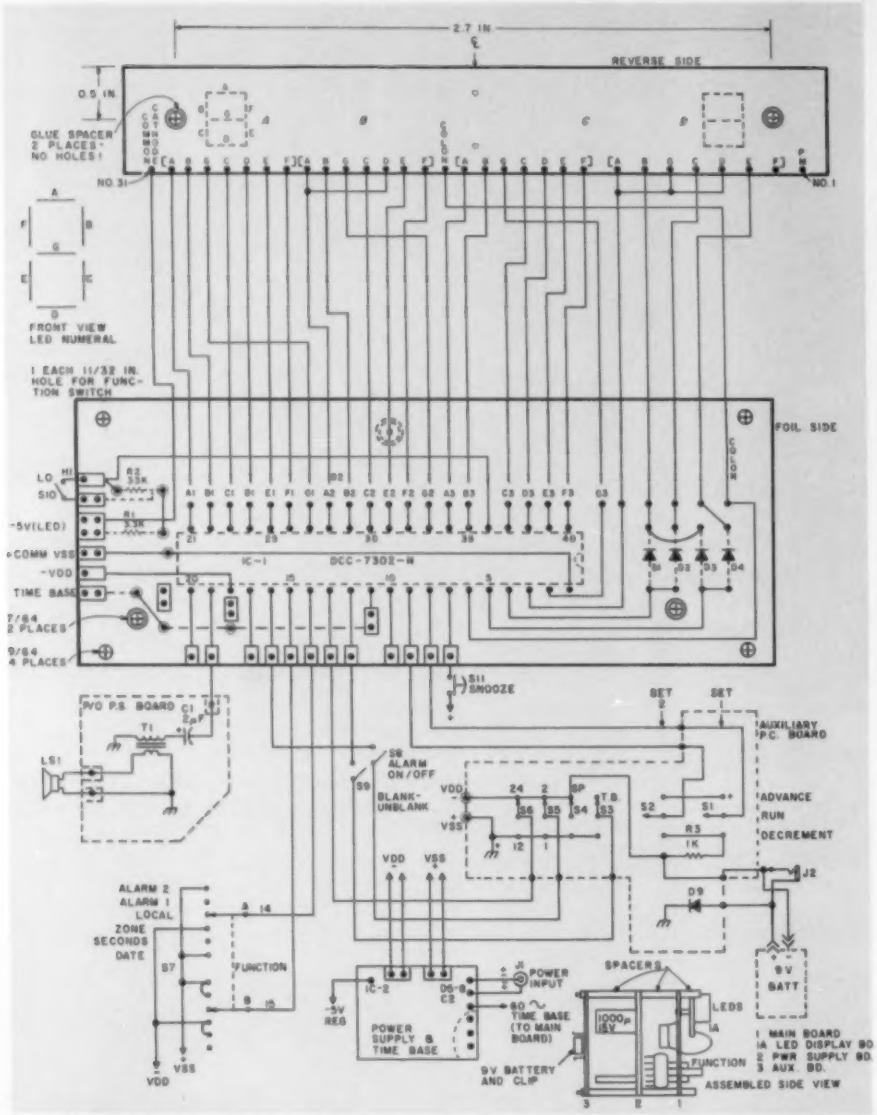


Fig. 13. Wiring arrangement used for the battery version. J1 and J2 must be isolated from the cabinet chassis.

Construction

All PC boards should be the same size for mounting ease, unless you wish to mount the programming board separately, as in the case of the 115/230 V version.

Check over the features

and decide which ones you need and which ones you can live without. Then determine how many switches you need. Time can be set with push-buttons, but, to conserve space, use SPDT miniature toggle switches with center-off. For economy, use single-pole slide switches where possible. Minimize the number of front panel switches. In the 115/230 V version, I used 6 push-button switches, 5 SPDT center-off toggle switches, 2 SPST slide switches, and 1 DPDT slide switch. In the battery version, it came out 2 SPDT center-off toggles, 1 push-button, and 7 SPDT slide switches, of which one is a spare and 4 are used in SPST functions.

Two problems were encountered in the timebase inputs. In the 115/230 V version, the chip would not initially clock. A copy of the kit schematic was obtained, and it indicated that pin 11 was biased back to common via a 150k Ohm resistor. This cured the clock problem but created another – the chip was clocking at 2 pulses per second rather than one pulse per second. A diode cured that. In the battery version, I found that pin 11 would drive directly off the output of the timebase without a diode, an isolation capacitor, or isolation resistor. However, I found that if the filter capacitor and the 7905 chip were not adjacent on the PC board, it would be necessary to place about 0.1 uF across the input to that chip to stabilize the output of the timebase.

A socket for the 7302N chip is recommended but not necessary. When drilling the PC board, use care, and, if possible, use special drills* for glass epoxy boards. Use nothing larger than a #65 drill, except at the edge points where wire connections are made, where a #60 drill is more correct. Of course, the hardware holes must be of the correct sizes to accommodate the screw sizes used. If a drill press is not available, be very careful with a hand drill or it will drift or make slanted holes, and aligning 40 pins of a chip or socket is no fun under those conditions (experience speaketh).

*Special drills are available from: Ford Cutting Tools, M.A. Ford Mfg. Co., Inc., Davenport IA, or Tools & Metals, 301 N. Johnson, El Cajon CA 92020.

The 2-pole 6-position non-shorting function switch may be mounted on the same PC board as the chip. The LED display and the chip PC are mounted back to back with a ¼" spacer between them (see drawings for details). Locate the positions on the back of the display that correspond to the positions on the template for the main board (with the chip). Thread the spacers for #4-40 screws, and use Super Glue™ (or its equivalent) to bond them in position.

I also used Super Glue to secure all slide switches in position, and, in the battery version, the battery clip was secured similarly. If done right, a good bonding is affected; if done wrong, try, try again (it took 3 passes for the battery clip to hang in there).

6-32 x 3" screws were used to mount the PC boards into the cabinets, using spacers and the front panel for support. If necessary, ¼" Plexiglas™ tubing may be used to fabricate the desired spacers. The i.d. is slightly smaller than a 6-32 thread and can be either tapped or drilled out – for ease of assembly and disassembly, unthreaded spacers are recommended.

Use care in locating the 4 mounting holes for the 6-32 x 3" screws, the openings for the display, and the shaft of the function switch on the front panel. In the battery version, provide an insulated mounting for the switch or insulate the shaft with shrink tubing, and be sure there is no contact between the shaft and the case (this has been

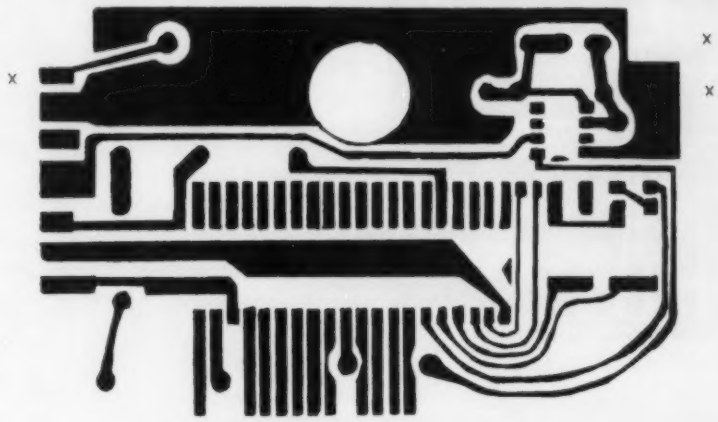


Fig 14(a). Main circuit board – PC board.

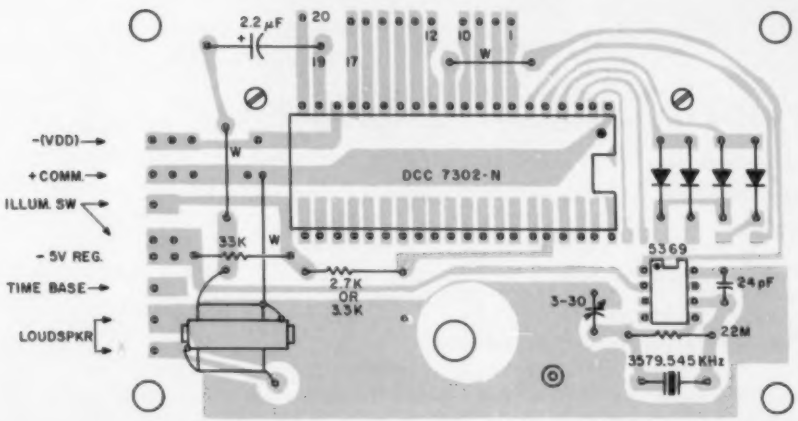


Fig. 14(b). Main circuit board – component layout.

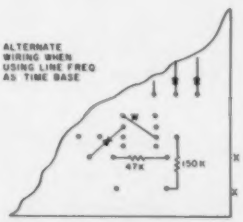
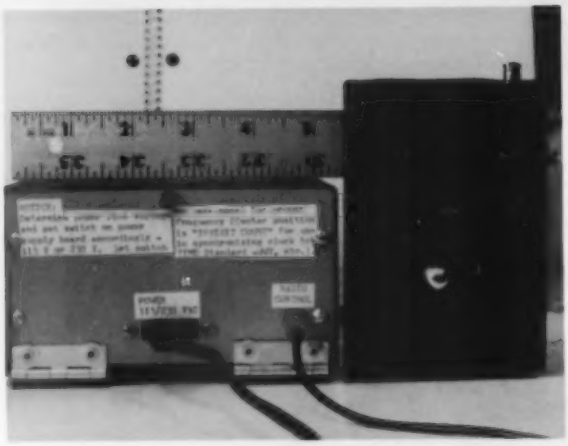


Fig. 14(c). Alternate wiring when using line frequency as timebase.



Ac operated version, rear view.

corrected in the included template drawing).

The illumination control is a 33k Ohm resistor with an SPST switch in parallel to add or subtract the 33k to or from the circuit. If desired, the switch and resistor may be replaced with either a 30k Ohm variable resistor or a photocell control of about 30k Ohms maximum resistance.

At this writing, it has been determined that the battery-operated unit is hard on 9 V transistor batteries, in spite of its low drain in the "low" or "blanked" conditions. A Duracell™ only lasted about 20 hours under a 26 mA load; a regular carbon-zinc battery lasted about 18 hours (both new batteries). Although the clock works satisfactorily on a 9 V battery charger, I learned that the circuit "loads" the charger to about 7.8 volts, and a new battery inside the unit will supply power to the clock, in parallel, until it is at or below the input voltage from the charger.

When the clock is on the internal battery, it will continue to function (blanked or low) at terminal voltages below 7.0 volts, but disturbing the input power (paralleling the battery or applying an external supply) can and does cause glitches, if not done carefully. When glitches are introduced, the displays become random – like showing 65 seconds, or a 3 in the tens-of-hours column, or beeping the alarm tone when the alarm is turned off. Under these conditions, the best cure is to remove power completely and restore the correct voltage level; the clock needed resetting anyway.

If it is desired to use the pm indicator in the 12-hour mode (rather than display 3 bars), the 12/24-hour selector will have to be a DPDT (center-off) switch, and the date format will have to be the American style (month/day). Similarly, if only the 12-hour option is desired, the month/day format must be used in order to access the pm indicator, as the 3-bar output required for a 2 or a 3 is also the pm indicator in the 12-hour mode, and no digit greater than a "1" can be

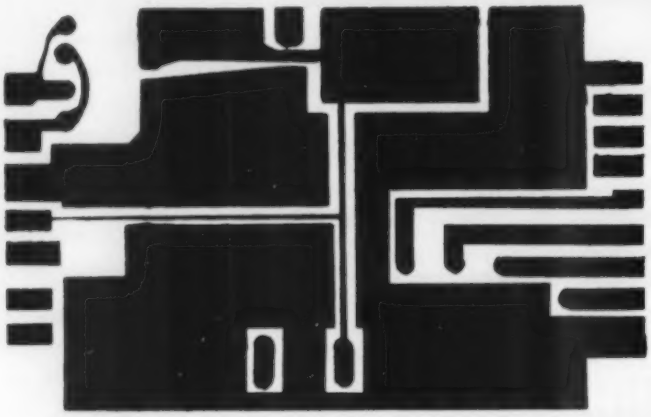


Fig. 15(a). Auxiliary board – battery version – PC board.

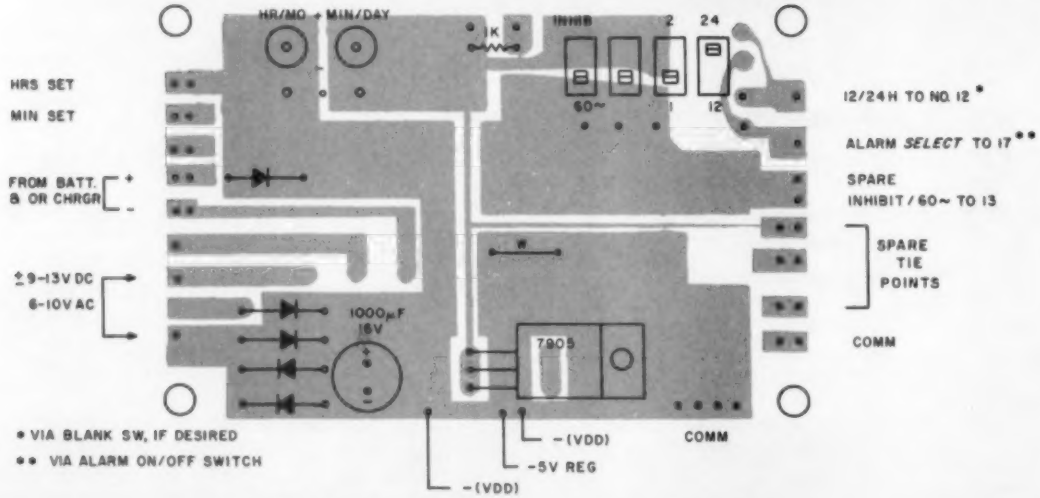


Fig. 15(b). Auxiliary board – battery version – component layout.

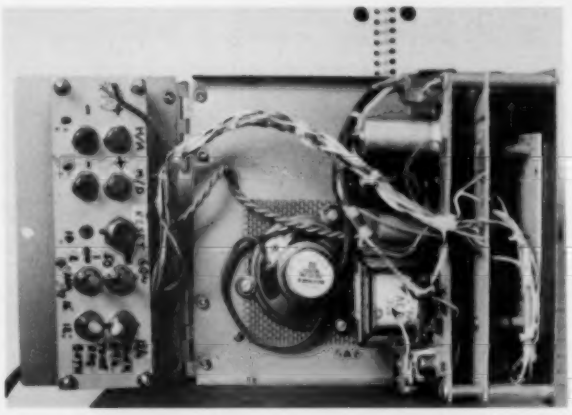
Parts List

Quantity	Description	115/220 V version	Battery version	Both	Price
1	7302N clock chip, Integrated Circuits Unlimited			x	6.00+
1	40-pin IC socket, ICU or IC Elex.			x	.50
1	LED display, four ½" digits + colon + pm indicator, Archer #276-1202			x	
5	Diodes, 1N277 or equivalent	x			
4	Diodes, 1N277 or equivalent		x		
2	Diodes, rectifier, 1N4001 or equivalent	x			
5	Diodes, rectifier, 1N4001 or equivalent		x		
1	7905-5 V regulator chip, ICU or IC Elex.		x		
2	Transformer, 115 V pri., 6.3 V 300 mA sec., Radio Shack	x			1.69 ea.
1	Transformer, output, 1200Ω pri., 8Ω sec., Calectro D1-724			x	
1	Capacitor, 1000 uF, 15 V			x	
1	Capacitor, 2000 uF, 15 V	x			
1	Capacitor, 2.2 uF, 15 V			x	
1	Resistor, 33k, ¼ W		x		
1	Resistor, 3.3k, ¼ W		x		
1	Resistor, 1k, ¼ W			x	
1	Resistor, 330Ω ¼ W	x			
1	Resistor, 4.7k	x			
1	Resistor, 5.6k	x			
1	Resistor, 27k	x			
1	Resistor, 47k	x			
1	Resistor, 150k	x			
1	Speaker, 8Ω 0.12 W, 2", Calectro S2-202 or equivalent			x	
1	Relay, 6 V 5kΩ (SPST n.o. only used)	x			
2	Switch, SPDT center-off toggle MS167		x		
4	Switch, SPDT center-off toggle MS167	x			
1	Switch, push-button, n.o. Electrocraft 35.414		x		
6	Switch, push-button, n.o.	x			
1	Switch, slide, DPDT	x			
2	Switch, slide, SPST Electrocraft 35-202	x			
1	Switch, rotary, 2 pole 6 posit. miniature, Archer 275-1384 (nonshorting type)			x	1.70
2	Switch, slide, SPDT		x		
4	Switch, slide, SPST		x		
1	Timebase kit, S.D. Sales		x		5.95
3	PC board 4" x 2½"		x		
2	PC board 5" x 2½"	x			
1	PC board 5" x 1½"	x			
1	Mini phone jack			x	
1	Jack, power input and matching plug set		x		
1	115 V power conn. TV type	x			
1	115 V TV cheater cord	x			
1	Cabinet 4¼"W x 3"H x 4-3/16"D, Ten-Tec TG 34		x		
1	Cabinet 5¼"W x 3"H x 5-7/8"D	x			
1	Transistor, 2N2219 or equivalent	x			
2	Hinge, brass 1½" x ½"	x			
4	6-32 x 3" screws, cut to size as required			x	
1	Mounting clip for NEDA1604 transistor 9 V battery		x		
1	Battery connection for NEDA1604 transistor 9 V battery		x		
	Assorted hardware and spacers				

tolerated in the tens-of-hours digit when the pm indicator is desired.

The clocks were mounted in small utility boxes. The 115/230-volt version was installed in a box 3" H x 5¼" W x 6" D. The chassis was U-shaped, but the back panel (skirt) was sawed off at the bend, dressed up to allow for hinging, and hinges were installed. The programming board is mounted on this, and, when it is desired to set the clock or change the program, one thumb screw is removed and the back drops down, disclosing the programming switches. The battery version is mounted in a Ten-Tec TG34 box which is 3" H x 4¼" W x 4¼" D. It is of a double "U" construction, and the top/sides piece is removed by removing one screw on each side, exposing the interior and making the set and program switches available.

An attempt to operate the battery clock off the cigar lighter outlet in the car met with failure, causing a glitch when the car was started. A filter is proposed, consisting of a small resistor and two 12 V zener diodes back to back to act as shorts for any transients. ■



Ac operated version, top view with the rear skirt opened to disclose "program" switches.

Car Battery Charger

—junk-box special

This is the safe way.

David E. Roscoe W1DWZ
49 Cedar Street, RFD #2
East Bridgewater MA 02333

One of the most useful pieces of "junk" that can be found in any self-respecting ham's junk box is an old, but serviceable, 12-volt automotive battery. They can be very useful for bench testing, field day operation, running that mobile rig at the home QTH, jump-starting the wife's car, etc. To be maintained at the peak of their usefulness, they do require occasional recharging. After getting along for a number of years with a haphazard (and dangerous) collection of hay wire and diodes, we decided to remedy the situation. Most of the commercially available chargers did not seem to meet the requirements we wanted, so we set out to fabricate our own. We wanted one that had the capacity to put out 15 Amperes or so if needed, yet have the capability of being adjustable to 1 or 2 Amperes for a trickle charge, or to some value in between.

After experimenting briefly with series resistors and series-regulating pass transistors, these ideas were discarded as we found it difficult to dissipate such large quantities of power (and heat). While thumbing through some manufacturers' applications literature, we came upon one describing the triac and decided that this would be a really neat way to do it (Fig. 1).

A triac is basically two SCRs connected in parallel in opposite directions so that conduction is permitted during both halves of the ac sine wave. By controlling the phase and amplitude of the signal to the gate, the firing point of the triac can be controlled and, thus, the conduction angle can be varied to regulate the input power to a transformer primary. A bilateral thyristor (D1, a diac) is used in the gate circuit to provide a threshold level for firing the triac. C3 and R4 provide a transient suppression network to protect the triac from damage when the power is switched off to the transformer primary.

R1, R2, R3, C1, and C2 provide a phase-shift network for the signal being applied to the gate. R1 is selected to limit the maximum charging current at full rotation of the control pot to stay within the ratings of the rectifiers, transformer, etc., of the specific components chosen by the builder. As is true of most ham projects, we tried to use what parts we had available. Readers wishing to build this unit could substitute whatever they might have in their junk boxes for the bridge and the transformer and their unit would only be limited by the voltage and current ratings of these components.■

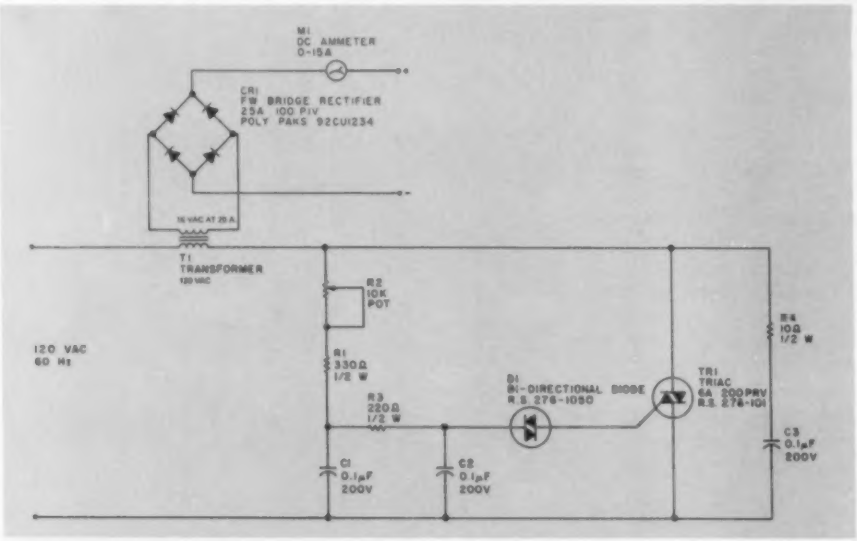


Fig. 1. Battery charger schematic diagram.

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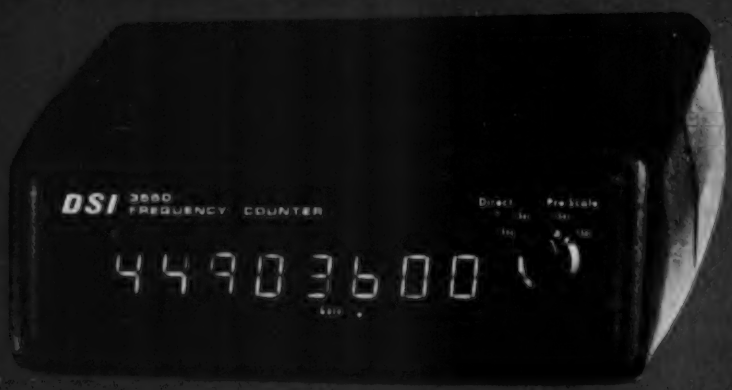

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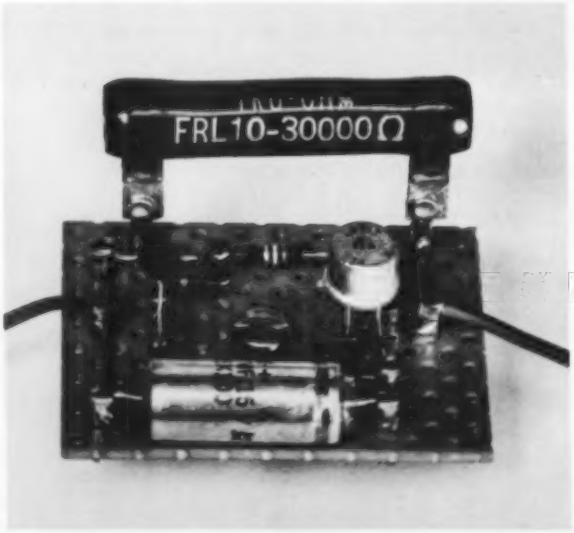
The solid state circuit shown in Fig. 1 is a simple but effective 60-second B+ delay. Q1 is any SCR able to block unloaded B+ voltage and pass the required load current. Using an RCA S-2061M, this circuit will perform in power supplies up to 600 volts and 4 Amperes.

This circuit is not a perfect switch. It has a voltage drop when on of about 1 volt and a "leakage" current when off equal to (Volts$_B$ unloaded /30 in mA. This "leakage" current of a few milliamperes limits plate voltages in most applications to only a few volts. The 10-Watt resistor is operated at full rating with a B+ of 600 volts, but only for 60 seconds at each turn-on.

Wire the B-delay into the power supply as shown in Fig. 2. The + end of the switch is connected to the input filter capacitor. All other wires except the one from the rectifier(s) must be removed from this capacitor and connected to the − end of the switch.

The B-delay may be installed in all types of vacuum tube equipment including receivers, transmitters, instruments, and TV receivers. Note: In a color TV receiver, the automatic degaussing may be visible on the screen for a few seconds after B+ is switched. The original B-delay used an RCA 40812 SCR. It has been operating in my black and white TV for 6 years, during which not a single tube has been replaced.■



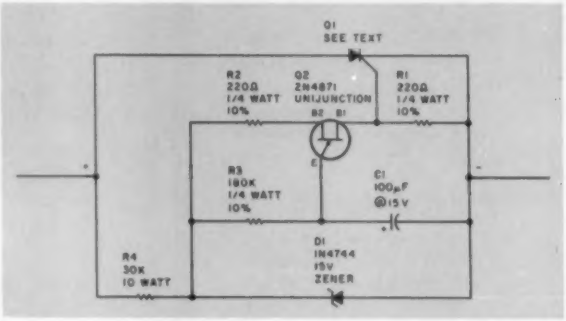


Fig. 1. Schematic.

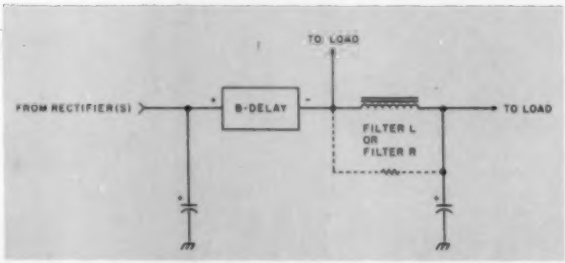


Fig. 2. Connection of B-delay in a power supply.

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The Hot Mugger X1

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There is no such thing as a cold drink.

Ever since Wayne Green's editorial in the July, 1977, issue of *73*, I have been thinking about a coffee warmer. He gave some ideas on how to make one and also said that it should be a real money-maker. I, too, hate cold coffee with a passion and usually end up with such every time I bring a cup out to the shack. So, with his idea and my junk box of parts, I put together the Hot Mugger, destined to become the most popular piece of gear in the ham shack.

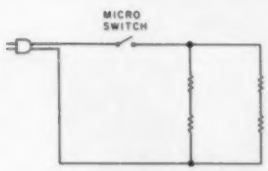

Fig. 1. Schematic.

I have used the Hot Mugger for several months now, and it works very well. But I have left a lot of room for improvement and would be interested to see other ideas for a coffee warmer. I am surprised that no one has written one up yet, as it is a very practical item for the ham shack. I hope this will set the wheels in motion and we will see many improvements and innovations.

The Hot Mugger does not require much in the way of parts. My junk box yielded all that were needed. There are four 550-Ohm, 15-Watt power resistors in series parallel, which gives 26 Watts of power dissipation. The 26 Watts does a good job of keeping a cup of coffee warm. I don't know how much lower you can go in power dissipation and still keep your cup warm, but you might try whatever you have on hand. I don't recommend exceeding 26 Watts, as this wattage will cause ¼ cup of coffee to become quite hot.

The cup should be a flat-bottomed one without any recess. I chose my cup before making the top for the coffee warmer so that I could cut the hole to the right size. The microswitch has a long actuator so that the cup will sit down on it and turn on the heating element (resistors). The base and housing were made out of printed circuit board, soldered and screwed together with an opening cut out of the top for the cup.

That's just about it except for painting. I used Rust-oleum® primer, which I don't recommend because it gave off a fishy smell for a long time afterward. Probably a good auto engine paint would be a better choice. A nameplate could be added so that your friends will know what it is.

As I type this, the Hot Mugger X1 is on the job keeping my coffee warm to the last drop. What is there left to say except, "Try it; you will like it." ■

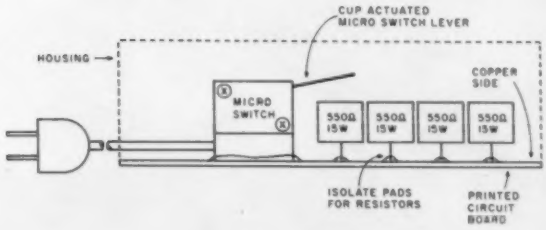

Fig. 2. Construction.

Side view of the finished Hot Mugger.

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The Circuit

Referring to Fig. 1, the plus 5 V and ground connections are made to the circuit under test, and the probe is touched to the pin under test. If the pin is open, Q2 will conduct slightly because of the bias introduced by R1. This will cause the yellow LED to light at about half brightness. If the pin under test is ground, both Q1 and Q2 are off so neither LED will light. If the pin is high, the red LED will blink once because Q1 puts a high signal into the one-shot, and the yellow LED will light at full brightness because Q2 is turned on. If only the yellow LED were used, it would be difficult to differentiate between an open and an oscillating condition. This is where the one-shot goes to work. It gives a relatively long (.5 seconds or so) pulse anytime the probe goes high—even if for a very short duration. So if the probe contacts an oscillating pin, it will blink continuously.

Unless pulses of very high frequency are to be detected, there is nothing critical about the layout except for space economy so that the board can be slipped into the case.

So there, in a nutshell (plastic one), is a way to know what's happening inside that digital monster's mind.■

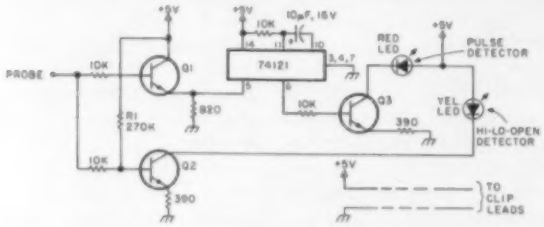
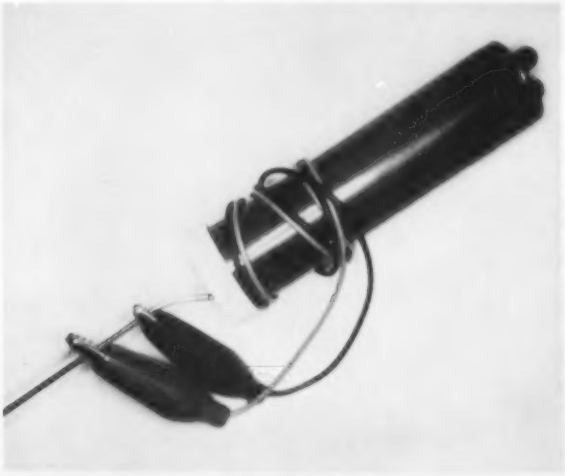


Fig. 1. Logic probe schematic diagram. Resistors ¼ Watt, 10%. Transistors ECG 123A or equivalent. LEDs as desired.



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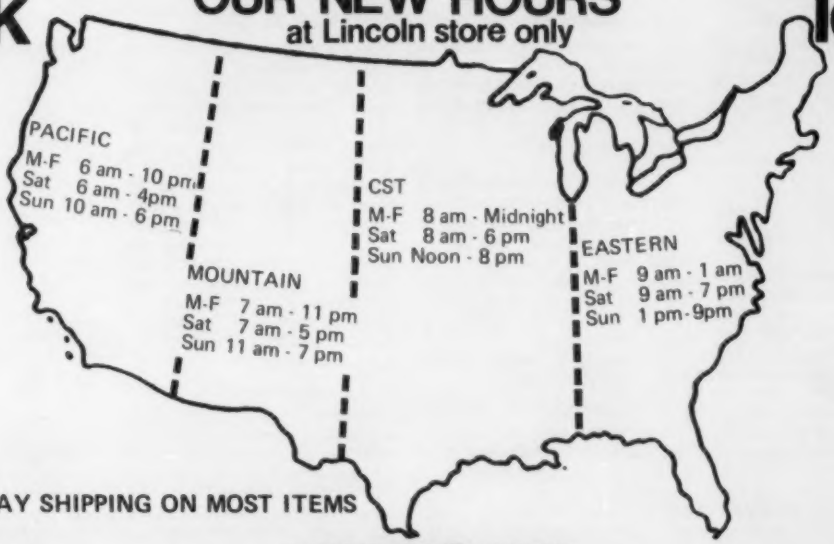
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editorial by Wayne Green

from page 4

interested in the same end . . . a better world, helped along a whole lot by amateur radio. Hamming can only provide these benefits to the world if it is fun, so let's all try to do what we can to make amateur radio fun . . . for everyone. I don't ask *you* to speak out against those who are lousing things up, whether by intention or stupidity—I just ask that you look into these things with an open mind and vote with your conscience.

ALSO AT ATLANTA

In addition to laying it on the line about amateur radio . . . and I expect the usual goon squad . . . I'll be talking about microcomputers. I'll be talking about them primarily in terms which may be of particular interest to you . . . how to make money in microcomputing. I'd talk about how to make money in amateur radio, but I don't know anyone who has figured it out yet. Perhaps those who are pushing for the Communicator Class license on 220 have the answer.

The opportunities in microcomputing are still as good as ever for making a bundle. The industry has grown some since I got involved. Sales in 1975 were about $5M. This went up to about $25M in 1976 . . . $100M in 1977 . . . and passed $300M in 1978. With Atari and Texas Instruments now hitting the market with microcomputers, 1979 is still an unknown quantity. Radio Shack has a very big lead and may just be able to hold it, what with about 10,000 of their stores selling the TRS-80.

I'll be talking about hardware which is needed and which can be marketed easily to make money. I'll be putting software into perspective. Mostly, I'll try to answer as many questions as I can. I may even talk a bit about the whole philosophy of making money . . . what the secrets of success are and how to achieve success if you want it. Most people have blundered into the trap of the good old American system . . . guaranteed to keep you poor for life and with no real hope of spectacular success. Is there anything to do about this? I think so . . . and the first step is to become aware of the system and how it can be beaten.

Will I be seeing you at Atlanta June 16-17th? I hope so. What about Dayton? I don't know . . . I skipped it last year, but haven't decided about this year yet. With two or three new magazines in various stages of getting started, Instant Software really getting going, and some other projects, I don't really have time to go most of the places where they want me, much less where they don't.

MEET ME IN ST. LOUIS

Yes, Wayne Green is coming to St. Louis . . . for the big hamfest on March 31st. I'll be talking about amateur radio . . . the good things and the bad. I'll be answering questions on just about anything. In addition to that, as at Atlanta, I'll be talking to microcomputer hobbyists about the many ways of making money in this new field. I'll try to give some perspective on what has happened and what I see as coming in both fields.

This will be my first trip to St. Louis, so I'm looking forward to it. I'll be getting in a day early, so I'll have a chance to get on the local radio and television stations and promote the hamfest.

If you're a Wayne Green fan, be sure to come to the show . . . at the new convention center. If you're anti-Green, it's even more important for you to come and make sure you are right in your assessment. Is it possible that you are more a part of the problem than a part of the solution? Find out at the St. Louis hamfest.

There will be a raft of exhibits and other talks . . . with manufacturers showing their latest ham gear and dealers doing their best to cut their own throats. They're lining up some fantastic speakers and forums (in addition to my talks), so you'll have a great time.

I'm looking forward to seeing you . . . please come.

THAT LONNNG ARRL PIECE

One of the problems is that I'm spread a lot thinner than I should be. Instant Software is demanding . . . as is *Kilobaud MICROCOMPUTING* . . . and with two or three more magazines in the planning stages, when do I sleep? This came to a head last month with my endless editorial about the League.

Normally, when I write an editorial, I sit down and write with smoke coming out of my typewriter. Then I find the heat abated a bit and write a second draft which is a bit less fiery. If I don't like the first two drafts, I try a third time. In December, *all* of the drafts of my editorial managed to reach print, end to end. I'm supposed to get a chance to review my editorial before it goes to the printer . . . but they skipped me last month. Rats.

Oh, I get annoyed at a lot of the crap I get from the League, but I'm not as upset about it as most people think. You'll perhaps get better perspective on this at St. Louis or Atlanta if you come and say hello and get into one of my talks.

ARTICLES NEEDED

Our increased use of color in *73* permits us to run some color photographs of interesting DX-peditions. The time was when we had to run all those pictures of gorgeous places in black and white. We're looking for colorful DXpedition pictures accompanied by interesting articles. An article will not only help pay some of the freight for the trip, but could also encourage others to help out a bit when they send for your QSL card. DX-ing is one of the most exciting aspects of amateur radio, so let's see more of the DXing fun in articles for *73*.

If I can get my new tower up, I'll be back in there scrapping with you for the rare ones. I'm a tough one to beat, so watch out! I racked up over 300 confirmed countries (all on 20m phone) in one year a while ago . . . and even managed 100 countries on 20m phone one weekend, just to prove to myself that I could do it. I didn't get much sleep.

It appears that we are up to here in antenna, keyer, and counter articles, but really in need of articles on transmitters, receivers, and transceivers. Surely someone out there has built a rig which will get thousands of hams hot to follow suit. Let's see more construction projects on ham gear.

It is my conviction that the tens of thousands of hams who have bought microcomputers should be using them in place of Teletype™ equipment. Let's have more articles on RTTY using microcomputers.

SLEP WRITES

A letter from Bill Slep (Slep Electronics) mentions that his ads have been selling stuff right and left. That's always nice to hear. Bill says that there has been a recent run on microwave equipment which hams are using to receive the TV satellites direct. I've been reading a lot about this recently and would like to encourage those who have been successful in getting something inexpensive together to do the job to write for us about it.

Why bother to get TV direct from a satellite? Well, right off the top there is the challenge. It isn't easy. Once you get set up, you'll be getting network program feeds. This means that you'll be able to get, for example, Johnny Carson before the salty language is bleeped out. You'll get a lot of programs which are not being broadcast in your area. You'll get the Home Box Office stuff . . . late movies.

I've been corresponding with Bob Cooper K6EDX/5, who publishes a magazine for the CATV field and is deeply into this direct satellite TV reception. I may be able to get him to either write an article for us or at least get him to get someone else to prepare such an article. Using commercial gear for the effort would run you into the thousands of dollars. Heck, just a receiver for 4 GHz costs thousands. Then they want you to buy a ten-foot dish and a special preamplifier. Some experimenters have been getting the stuff with a lot less expense and trouble. If you're one, write to me about it.

NEW COVER PRICE

The new cover price shouldn't come as much of a surprise to anyone. A big part of it is inflation, which has been running about 10% of late. It's been two years since there has been an increase in cover price. If inflation keeps up like it has (if you continue to let your congressman spend money on more and more government), the price increases will have to come more often. How'd you like to find a different price every month? Keep it up, Congress!

We see the inflation in many ways. Postage has gone up beyond belief . . . made even worse by the great big, thick, heavy issues of *73*. Paper costs have doubled in the last couple of years, and no end is in sight. Wages all around have been going up in step with inflation. Our advertising rates, once under $100 per page, are now over $1,500 for a page!

Obviously, the way to beat the cover price is to subscribe. I've been hinting gently at that for a long time. At $2.50 per issue, this comes to $30 per year. The subscription rate is $18 for one year and $36 for three years. That means you can get three years of *73* for just a little bit more than buying one year on the newsstand. Convinced? Remember when a life subscription was going for $37?

Of course, those early issues of *73* were much smaller (about one half the size of this page) and thinner. You're getting eight times as much material for about six times the price . . .

so it is a good deal. Fifty-seven feature articles in the November issue! That's more than all the other magazines combined, isn't it?

THE 10 GHZ SAGA

Chuck Martin WA1KPS started off going great guns (Gunns, that is) on 10 GHz with contacts with New Hampshire from Massachusetts, Vermont, Maine, and even the Granite State itself (106 miles between Pack Monadnock in southern New Hampshire and Mt. Washington, up north). From there on, the situation got more difficult.

A couple of tries from hills in Rhode Island didn't make it. The paths were even difficult on 220 MHz, so the failure on 10 GHz wasn't very surprising, even if it was disappointing.

Chuck got the two transceivers together and found little things to do which supposedly improved their action. He also borrowed a two-foot dish to perk up his end of the signal, just in case this would help. It might push a signal through some trees, but it wouldn't boost it over any mountains.

On November 19th, I braved icy winds gusting to over 80 mph up in the superstructure of a tower on the Pack, while Chuck relaxed up in the branches of a tree on a hill in Rhode Island. Well, he was perhaps only partly relaxed, considering that he was trying to hold on to the tree while he aimed the dish and tuned the transceiver . . . and gradually froze.

Perhaps it was worth it all. We did manage some short contacts as the two transceivers drifted in frequency about 16 MHz as they cooled down to the subarctic temperatures. The AFC system is pretty good, but definitely not equipped to handle that kind of drift. And tuning the little buggers is about like trying to tie an appendix with boxing gloves on. You have to turn the tuning knob about a thousandth of an inch to tune in a signal. This is interesting to do when you are being blown almost out of a tree or a tower by gusts of very cold wind . . . shivering . . . and your hands are turning blue as frostbite creeps up towards your armpits.

That makes five states on 10 GHz, with all contacts being over 50 miles. Anyone done better than that, or should we send it to the book of world records? Our laurels will not be crushed. Chuck has some ideas on pepping up the transceivers, and if we put the darned things outside so they can come to a steady temperature, we should avoid the drift miseries. The next stop obviously is Connecticut for state number six . . . if we can get organized before the snow hits.

Those little Microwave Associates Gunnplexers sure are good fun. They put out enough of a signal so that you should not have to have any additional antenna for a contact over any line-of-sight path. Our contact of over a hundred miles was plenty strong.

Sherry has been itching to get a hot air balloon ever since we went down to Florida and made the balloon cover for *73* a couple of years ago. If we get one, I understand that contacts from the balloon count for New Hampshire as long as the balloon is tethered. I wonder if a 5,000-foot kite string counts as a tether?

OCTOBER WINNER

Our readers have selected "Antenna Design: Something New!" as the best article in our October issue, so Harry A. Mills W4FD and Gene Brizendine W4ATE will be sharing our $100 Most Popular Article prize. Remember, your ballot is your Reader Service card.

DX

from page 14

from Greenland to South America out of our home base, Wright-Patterson AFB, on a two-week "worldwide" communications test of an experimental airborne satellite terminal. Among the crew of 25 men, we had four hams: Sandy Cole K1SC, Tom Walilko K8NOQ, Bob Beach W8LCZ, and Wayne Beeson K8WB.

After landing (on Ascension Island) on Saturday night, we immediately searched for the acting base commander, Captain Lord, and finally found him in a barracks card game. Captain Lord informed us that the required forms and the British Islands Administrator's signature needed to obtain our own ZD8 calls would not be available until Monday morning. Meanwhile, he authorized the use of your call, ZD8KG, for us as guest operators. He presumed your kind permission since you were not then on the island.

The authorization seemed adequate, as we had the word of the *Lord*, so we rushed over to barracks 14 and set up our FT-101E and 18-foot vertical antenna. Our first QSO took place just after midnight on September 17th with W7PFZ on 20 meter SSB.

We then proceeded to have the time of our lives working our first pileup from the fun (rare) end of the QSO. An awesome and enjoyable experience almost every DXer has dreamed of was coming true. All four of us took turns as noted in the enclosed log copy.

We worked 10, 15, and 20 meter CW and SSB. Conditions on 10 were great, so we used that band a lot in racking up 230 contacts from ZD8KG in about 36 hours.

On Monday, we filled out the required forms, got the necessary signatures, and finally received our own calls. Sandy got ZD8SC, Robert got ZD8RB, Wayne got ZD8WB, and I got ZD8TW. We still had some operating time left, so we returned to the rig and ran off 105 more contacts in the four hours before our plane took off for Brazil.

We totaled five continents, fifty countries, and 325 contacts, of which 101 were with stateside stations. We earned no awards but we had a terrific time.

During some hurried and confused packing, we yanked our antenna off the barracks roof in the middle of our last QSO with WB0TXV on ten meter SSB. A sudden end to our DXpedition. We all had a ball and can't wait to do it again. Our plane will return to Ascension Island in March, 1979, and again in the summer of 1980. We plan to bring multiple rigs next time and to use our newfound experience to cut through the pileups faster. Meanwhile, we left our aircraft number and 73 written with six-foot high rocks on the side of West Bay Hill near the barracks.

We requested everyone we worked to QSL direct to our home calls, but if you or your QSL manager, K4KBL, receive any cards for contacts we made, you can forward them to me. Again, thanks for the use of your call and we hope to see you on a future trip to the island.

Tom Walilko K8NOQ/ZD8TW
712 Sykes Circle
Wright-Patterson AFB OH 45433

BITS AND PIECES

As of this writing, no documentation has reached the ARRL for the HZ1BS/8Z4 neutral zone operation. No documentation, no recognition.

If you still haven't worked KV4, there is really no excuse. KV4AA recently made his 38,000th QSO. Most are CW.

That W0DX who operated from Desecheo recently is Bob Denniston, former president of the ARRL. He runs the Smuggler's Cove Hotel on the north side of the island group.

4U1ITU in Geneva reports that they are receiving QSL requests for 4U1UN in NYC. The correct QSL route for 4U1UN is UN Staff Radio Club, United Nations, Box 20, NYC NY 10017. SASE, of course.

For those who are still confused by the FCC callsign allocations in areas outside the continental U.S., the following should be of some help. The

George Lindley WA5HKW erecting his home-brew three-element beam. George built it from plans in Bill Orr's Beam Antenna Handbook *for about one-third the cost of a commercial beam. He says it works great.*

digit is the key. Alaska stations sign AL7, KL7, NL7, and WL7. The rest are as follows.

Atlantic: 1—Navassa Island; 2—Virgin Islands; 3—Serrana Bank; 4—Puerto Rico. Prefixes are KP, NP, and WP.

Pacific: 1—Baker, Canton, Howland Islands; 2—Guam; 3—Johnston Island; 4—Midway Island; 5—Kingman Reef (K suffix); 5—Palmyra, Jarvis; 6—Hawaii; 7—Kure Island; 8—American Samoa; 9—Wake Island; 0—Northern Mariana Islands. Prefixes are AH, KH, NH, and WH.

All the foreign nationals have been assigned YS9 prefixes in El Salvador. YS1WPE is now YS9YSS.

The operator at HF0POL, the Polish base in the South Shetlands, left and the new crew contains no amateurs. QSLs have been printed, but there is a holdup in getting them filled out and mailed.

The ARRL is planning to take the FCC ten meter linear ban to court. As noted before, the innocent hams were the only ones to suffer from this ban. The manufacturers of illegal CB linears either went underground or switched to manufacturing high-powered "amateur transmitters." CBers just plug in their transceiver as a vfo. Passing laws to make it illegal for lawbreakers to break the law has never made much sense to us.

Those working toward WAZ should bear in mind that UA0YAE, heard often on 15 meter CW, is located in Tana Tuva, which is in Zone 23. In fact, any UA0Y is in Zone 23.

Gary Yarus WB0MSZ puts out a directory of stateside QSL managers that contains over 1300 managers. This is almost a necessity for the serious DXer and at only $1.00, it's a great bargain. The address is: Gary Yarus, 921 N. Clay Avenue, St. Louis MO 63122, and the list is updated weekly.

UV0BB claims to be the first and only YL operator in Siberia.

SV1IT is considering a possible Mt. Athos effort this summer. Nothing definite as yet, but if you run across him, you might ask for the latest word.

Amateur radio continues to experience rapid growth. Amateur licenses in the U.S. are expected to top 366,000 by early this year. There were some 28,000 new licenses issued during 1978. The total number of licensed amateurs in the U.S. has increased better than 100,000 since 1975. CB licenses, on the other hand, dropped below 100,000 per month last summer for the first time in several years. Look for several of the larger CB equipment manufacturers to jump into the amateur market.

QSL manager ON5TO notes that the true-blue 9U5CA has not been active since 1971. The one showing in '76-'77 was a pirate. Only 9U5CB, 9U5DS, and 9U5CR are legit at present.

The U.S. and Surinam, PZ, completed a reciprocal operating agreement on October 12. Amateurs of either country wishing to operate in the other country can do so upon application to the proper authorities. Information on this or any other reciprocal operating agreement can be obtained by sending an SASE to the ARRL. Reports indicate a reciprocal agreement with Spain is now in the works.

A note from K5OVC straightens out the Argentine-Antarctic callsign designations. LU-ZA, ZG, and ZM are South Orkneys. LU-ZY is South Sandwich. LU-ZC, ZI, ZO, SZ, and ZT are South Shetlands. Others are Antarctica.

Jim Henderson, who spent several months signing ZM7AH from the Tokelaus a few years back, wants to clean up any remaining need for ZM7AH cards and seal the logs permanently. Anyone still needing a card can reach Jim at 13490 Mt. Hood, Reno NV 89506.

The Mellish Reef operation, VK9ZR, managed some 16,000 contacts despite being plagued by generator problems that limited their output.

K4OD notes that he still has all logs from his previous overseas assignments and will be glad to confirm any contacts. Anyone needing a card from OA4DX ('68-'71), HP1XOD ('70-'71), PY1ZAL ('71-'73), EP2OD ('75-'77), or 9D5B ('76-'77) can reach Carl at PO Box 135, Front Royal VA 22630. SASE, of course.

EI8H is a legitimate station, but any EI8H/xx you hear is a definite phony. Pat has been getting loads of QSLs for these operations, but all are going into the trash and he requests that no more be sent.

ZD9GG can often be found on a list operation run by WA7ZTL on 14245 kHz around 1445Z. An Asahi newspaper recently took some aerial photos of Okino Torishima. The outlines of the barrier reef are quite distinct and the foundation of the never-built weather station can be seen in the center. Only two rocks are visible at high tide. One is five feet tall. It is difficult to imagine another operation taking place from here for quite some time.

The DX gathering on 14225 kHz after 1500Z is a great hunting ground. Check it out.

The first DXCC for 160 meter operation was issued on November 15, 1976. Since that time, twelve have been issued. #1 went to W1BB, of course, #2 to W1HT, #3 to W8LRL and KV4FZ (two were issued), #5 to K1PBW, #6 to W4BRB, #7 to W2QD, #8 to W2DEO, #9 to W4QCW, #10 to W4YWX, #11 to K4CIA, and #12 to W9NFC. The east coast pretty well has a lock on this award.

8J1JCI was a special station on from the Japanese Chamber of Commerce and Industry Centennial Exhibition.

QSL INFORMATION

In the November column, a typo snuck in directing QSLs for GU5CIA, GU4EON, and GU3YIZ to K5YY. This was an error and San says no more, please. The correct route is to N6MA, whose address is listed below.

3D6BA to WA4HNL
3Y0BZ to VE7ZQ
3Y5DQ/3Y1VC to LA5NM
4079WARC to YU2DX
4N0D to YU2CQ
4N2EC to YU1JAS
7P8BH to WB9ZZK
8J3ITU to JH3DPB
9J2JN to WB2IZN
9K2FX to W4KA
GU5CIA to N6MA, 3800 J Street, Oxnard CA 93030
A7XAH to DJ9ZB
EX9A to Box 88, Moscow
H5RAC to WA4HNL
HH2DX to George Werner, 1045 Le Brun, Jacksonville FL 32205
HZ1AB to K8PYD
J28AZ to I8JN
JY3ZH to DJ9ZB
KA1MI to WB1GXU
KA1NC to K4JEX
KG4KG to YASME
LU3ZY to SARA, Malabia 3029, 1425 CF, Buenos Aires
N0TG/KP1 to Randy Rowe, 3237 Connecticut Drive, St. Charles MO 63301
S8GEH to WA4HNL
TF0DF to K4SAK
ZL3HI/C to N2CW, 207 West Fifth Street, Ship Bottom NJ 08008

Thanks to *The West Coast DX Bulletin*, the Long Island DX Association *Newsletter*, and *Worldradio Magazine* for much of the preceding information.

AMATEUR RADIO IN IRAQ

During a business trip to

Ever wonder what the shack of a rare DX station looks like? Here's the operating position of the much-sought-after YI1BGD, the only station currently active in Iraq. Pictured are ops Majid (seated) and Saad, along with their Atlas transceiver. Can you spot your QSL on the wall? Thanks to Jack Winterbourne VE3ITO and the CARF News Service for the photo.

Baghdad in September, 1978, I contacted Majid Abdulhamid, Chief Operator of the Radio Club of Baghdad, amateur radio station YI1BGD.

Majid gave me telephone directions to find the club premises, now located in the building of the General Directorate of Scientific Welfare in the Azamia district of Baghdad. This building also houses other scientific clubs.

I was met by Majid and another club operator, Saad Al Tai, both of whom accorded me a very courteous welcome.

On being informed of the general interest of North American amateurs in the situation of ham radio in Iraq, they explained their present status.

YI1BGD is the only legal ham station in Iraq at present. Majid is holder of the license, which is limited to the 20 meter band and 100-Watt input.

The club hopes to be permitted soon to operate on other bands and with higher power.

The present membership, besides Majid, consists of seven operators, including two YLs. Majid expects the club to grow as their activities become more widely known.

The whole operation was made possible through a radio course given by YU1NFV, who has since left Iraq.

The club station commenced operation on April 14, 1978, and has logged a respectable number of countries and QSOs since that time.

The present station is equipped with an Atlas 210 and a two-element quad which is operated manually. Recently, they received a donation from Japan of a Yaesu FT-101, which is awaiting clearance at customs pending the revised station license.

YI1BGD's operating schedule is Monday and Wednesday on 14210 MHz, and on Friday from 2000 UTC until 0100 UTC, their beam is directed at North America. At that time they have regular skeds with VO1CU (Gordon) and 12CBM (Bert) who act as control stations on their behalf. The Friday frequency is 14310 MHz.

When I enquired if they had any QSLs for VE3-land which I could carry back, they showed me the station log which indicated almost 100 percent QSL response from them. Those hams who have sent QSLs are quite certain to receive confirmation, but it will take time. It does not appear that the club takes long to respond, but the distance and conditions really slow things down.

The club has received some publicity in the Long Island DX Association bulletin, one of the British magazines, and locally in an Arabic publication.

My friends were kind enough to let me take a few pictures of them and their station (I hope the film survives the security checks on the return trip), and also gave me a small black and white print of four of the operators in the shack—Kamal, Majid, Mohammed, and Dhia.

Judging by the enthusiasm of these two men, the DX hounds will continue making regular contact with YI1BGD, but it is doubtful that there will be any other YI stations for some time. This information came to us courtesy of Jack Winterbourne VE3ITO, and was first published in the Burlington, Ontario ARC bulletin.—Ed.

FCC

Reprinted from the Federal Register.

ADMINISTRATION OF TELEGRAPHY EXAMINATIONS TO HANDICAPPED APPLICANTS FOR OPERATOR LICENSES IN THE AMATEUR RADIO SERVICE

Order extending time for filing comments and reply comments

AGENCY: Federal Communications Commission.

ACTION: Order Extending Time to File Comments.

SUMMARY: The FCC is inquiring into the administration of its telegraphy examinations to handicapped persons who apply for amateur radio licenses. The comment period ends November 30, 1978. Mr. Norman Kaplan has petitioned to extend the comment period. The comment period is being extended to encourage as wide a participation in the proceeding as possible.

DATES: The comment period is extended to March 30, 1979. The reply comment period is extended to April 30, 1979.

ADDRESSES: Send comments to: The Secretary, FCC, 1919 "M" Street NW., Washington, D.C. 20554.

FOR FURTHER INFORMATION CONTACT:

Mr. Robert Cassler, Personal Radio Division, Safety and Special Radio Services Bureau, 202-634-8620.

SUPPLEMENTARY INFORMATION: See attached document.

Adopted: November 21, 1978.

Released: November 24, 1978.

In the matter of the administration of telegraphy examinations to handicapped applicants for operator licenses in the Amateur Radio Service, Gen Docket No. 78-250.[1]

1. On August 24, 1978, the Commission released a Notice of Inquiry into the administration of telegraphy examinations to handicapped appticants for operator licenses in the Amateur Radio Service. Cummenta were due no later than November 30, 1978. Reply comments were due no later than December 29, 1978.

2. A petition to extend the comment period to March 30, 1979 was submitted by Mr. Norman Kaplan of the Disabled American Veterans, North Miami Beach, Florida. Mr. Kaplan cites the need for as many handicapped persons to participate in the proceeding as possible. Because of the special nature of this proceeding, we agree with petitioner.

3. Accordingly, the Commission, by the Chief, Safety and Special Radio Services Bureau, pursuant to delegated authority granted to him by § 0.331 orders that the comment period and the reply comment period in General Docket No. 78-250 are extended to March 30, 1979, and April 30, 1979, respectively.

CARLOS V. ROBERTS,
Chief, Safety and Special Radio Services Bureau.

OSCAR Orbits

Courtesy of AMSAT

FINDING OSCAR

The listed data tells you the time and place that OSCAR 7 and OSCAR 8 cross the equator in an ascending orbit for the first time each day. To calculate successive OSCAR 7 orbits, make a list of the first orbit number and the next twelve orbits for that day. List the time of the first orbit. Each successive orbit is 115 minutes later (two hours less five minutes). The chart gives the longitude of the day's first ascending (northbound) equatorial crossing. Add 29° for each succeeding orbit. When OSCAR is ascending on the other side of the world from you, it will descend over you. To find the equatorial descending longitude, subtract 166° from the ascending longitude. To find the time OSCAR 7 passes the North Pole, add 29 minutes to the time it passes the equator. You should be able to hear OSCAR 7 when it is within 45 degrees of you. The easiest way to determine if OSCAR is above the horizon (and thus within range) at your location is to take a globe and draw a circle with a radius of 2450 miles (4000 kilometers) from your QTH. If OSCAR passes above that circle, you should be able to hear it. If it passes right overhead, you should hear it for about 24 minutes total. OSCAR 7 will pass an imaginary line drawn from San Francisco to Norfolk about 12 minutes after passing the equator. Add about a minute for each 200 miles that you live north of this line. If OSCAR passes 15° east or west of you, add another minute; at 30°, three minutes; at 45°, ten minutes. Mode A: 145.85-.95 MHz uplink, 29.4-29.5 MHz downlink, beacon at 29.502 MHz. Mode B: 432.125-.175 MHz uplink, 145.975-.925 MHz downlink, beacon at 145.972 MHz.

OSCAR 8 calculations are similar to those for OSCAR 7, with some important exceptions. Instead of making 13 orbits each day, OSCAR 8 makes 14 orbits during each 24-hour period. The orbital period of OSCAR 8 is therefore somewhat shorter: 103 minutes.

To calculate successive OSCAR 8 orbits, make a list of the first orbit number (from the OSCAR 8 chart) and the next thirteen orbits for that day. List the time of the first orbit. Each successive orbit is then 103 minutes later. The chart gives the longitude of the day's first ascending equatorial crossing. Add 26° for each succeeding orbit. To find the time OSCAR 8 passes the North Pole, add 26 minutes to the time it crosses the equator. OSCAR 8 will cross the imaginary San Francisco-to-Norfolk line about 11 minutes after crossing the equator. Mode A: 145.85-.95 MHz uplink, 29.4-29.50 MHz downlink, beacon at 29.40 MHz. Mode J: 145.90-146.00 MHz uplink, 435.20-435.10 MHz downlink, beacon on 435.090 MHz.

Oscar 7 Orbital Information

Orbit	Date (Feb)	Time (GMT)	Longitude of Eq. Crossing °W
19272	1	0040:17	71.4
19285	2	0134:34	85.0
19297	3	0033:54	69.8
19310	4	0128:11	83.4
19322qrp	5	0027:31	68.3
19335	6	0121:48	81.8
19347X	7	0021:09	66.7
19360	8	0115:26	80.3
19372	9	0014:46	65.1
19385	10	0109:03	78.7
19397	11	0008:23	63.6
19410qrp	12	0102:40	77.2
19422	13	0002:01	62.0
19435X	14	0056:16	75.6
19448	15	0150:35	89.2
19460	16	0049:55	74.0
19473	17	0144:12	87.6
19485	18	0043:32	72.5
19498qrp	19	0137:49	86.1
19510	20	0037:10	70.9
19523X	21	0131:27	84.5
19535	22	0030:47	69.4
19548	23	0125:04	82.9
19560	24	0024:24	67.8
19573	25	0118:41	81.4
19585qrp	26	0018:01	66.2
19598	27	0112:18	79.8
19610X	28	0011:39	64.7

Oscar 8 Orbital Information

Orbit	Date (Feb)	Time (GMT)	Longitude of Eq. Crossing °W
4636Abn	1	0133:06	66.9
4650Abn	2	0138:19	67.2
4663Jbn	3	0000:17	42.7
4677Abn	4	0005:29	44.0
4691Abn	5	0010:42	45.4
4705Abn	6	0015:54	46.7
4719X	7	0021:06	48.0
4733Abn	8	0026:18	49.3
4747Abn	9	0031:30	50.6
4761Jbn	10	0036:43	51.9
4775Jbn	11	0041:55	53.3
4789Abn	12	0047:07	54.6
4803Abn	13	0052:19	55.9
4817X	14	0057:31	57.2
4831Abn	15	0102:43	58.5
4845Abn	16	0107:55	59.8
4859Jbn	17	0113:07	61.1
4873Jbn	18	0118:20	62.5
4887Abn	19	0123:32	63.8
4901Abn	20	0128:44	65.1
4915X	21	0133:56	66.4
4929Abn	22	0139:08	67.7
4942Abn	23	0001:06	43.2
4956Jbn	24	0006:18	44.5
4970Jbn	25	0011:30	45.9
4984Abn	26	0016:42	47.2
4998Abn	27	0021:54	48.5
5012X	28	0027:06	49.8

New Products

from page 26

ing. The peak reading feature is a must for SSB transmitters. The MP1 also will display swr. Swr is measured directly, without having to use extra charts or graphs.

For ease of installation, the MP1 has a removable coupling unit which may be placed up to 4 feet from the meter.

The MP1 is portable. It contains the latest in low-power ICs and is powered by a 9-volt battery. For long-term nonportable operation, an optional ac adapter is available.

A low-battery-voltage indicator has been built into the wattmeter to indicate when the battery needs changing.

The MP1 will provide all the functions and features needed to maintain an efficient, well-operating HF amateur station.

For more information, please contact your local dealer or *Mirage Communication, PO Box 1393, Gilroy CA 95020; (408)-847-1857.* Reader Service number M75.

NEW MURA VOM MULTITESTER OFFERS DUAL-RANGE SENSITIVITY

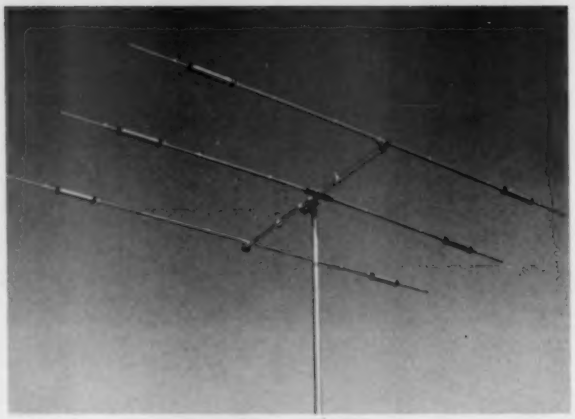
Mura Corporation, manufacturer of home entertainment products, CB accessories, and electronic parts and components, has introduced a new precision VOM multitester with extremely high dual-range sensitivity.

Designated Model 85-M, the new VOM multitester is ideal for use where measurements must not appreciably disturb a particular circuit being tested. It features high 50,000-Ohms/volt dc and 10,000-Ohms/volt ac sensitivities on one set of voltage ranges, and 25,000-Ohms/volt dc and 5,000-Ohms/volt ac on a second group of voltage ranges.

In conjunction with a power supply, the 85-M can be used to measure capacitance and inductance. Special circuitry has been included to protect the meter movement against accidental overload, and a mirror arc has been provided to help eliminate parallel error from readings. In addition, a convenient carrying handle, attached to the unit's high-impact casing, can be positioned for easy meter reading.

The new 85-M measures 6¾" x 5" x 2" and weighs 1 lb., 5 oz., with batteries. *Mura Corporation, 177 Cantiague Rock Road, Westbury NY 11590; (516)-935-3640.* Reader Service number M79.

The Mura Model 85-M VOM multitester.



Wilson's "System Three."

"SYSTEM THREE" BY WILSON

Wilson Electronics is proud to announce the latest in tri-band antennas for 10-15-20 meters. The "System Three" features lightweight design, heavy-duty materials, low swr across all three bands, a boom length of 14' x 4", wind survival of 100 mph, direct feed with 52-Ohm coax or with a balun, and a capability of 2000 Watts.

For more information on the "System Three," see your favorite dealer or contact *Wilson Electronics, Consumer Products Division, PO Box 19000, Las Vegas NV 89119.* Reader Service number W2.

YAESU'S FT-202R

"The Handie," a new miniaturized two meter handheld transceiver (Model FT-202R), has now been added to the Yaesu line of amateur radio equipment.

Measuring only 67 x 49 x 171 mm, the one-Watt-output, six-channel hand-held should please the most critical user with its excellent receiver performance and high-quality F3 transmitted signal.

The receiver is double-conversion, with a sensitivity measurement of 0.32 mV for 20-dB quieting. "The Handie" covers the entire two meter band and includes a flexible rubber ducky antenna and attractive carrying case. Crystals are supplied for three channels.

Other features include a combination "S"-meter and tuning meter, tone burst or subaudible squelch (optional), built-in speaker, and condenser microphone. Batteries required (not supplied) may be AA-size or nicads to provide 9.6 V dc (not to exceed 12 V dc).

For complete details on this new hand-held transceiver, see your Yaesu dealer or write to *Yaesu Electronics Corporation, PO Box 498, Paramount CA 90723.* Reader Service number Y1.

NEW CUSHCRAFT HF VERTICALS

Many hams are convinced that to work meaningful DX they need a couple of thousand Watts and a monster antenna array. While that undoubtedly helps, where is it written that the ham suffering a money or space cramp can't compete for his day in the DXCC sun?

Three new Cushcraft verticals, the ATV-3, ATV-4, and ATV-5, provide a commonsense solution to a commonplace problem. Specifically designed for the DXer, these antennas provide the low angle of radiation necessary for long-haul DX communicaiton, along with the performance and quality long associated with the Cushcraft name. The ATV-3, ATV-4, and ATV-5 operate over the 10, 15, and 20 meter amateur bands, with the ATV-4 having built-in 40 meter coverage and the ATV-5 all set for complete 5-band operation.

All antennas feature a built-in PL-259 coax connector and stainless steel hardware for all electrical connections, and are matched to 50 Ohms and rated for a full 2000 Watts PEP. Factory-marked tubing and plain English instructions make assembly a snap.

Built to withstand the severest weather, the ATVs feature specially-designed high-Q traps employing large-diameter enameled copper wire and solid aluminum air-dielectric capacitors. The trap forms are manufactured from filament-wound fiberglass for minumum dielectric loss and high structure strength. Durable 6063-T832 aluminum tubing with 0.058" (1.5 mm) walls used for the vertical radiator and the heavy-duty phenolic base insulator ensure long life and durability. All this adds up to an antenna line that comes through winter after winter a winner!

For more information and a

The new Mizuho SX-59 preselector from Gilfer.

full-color catalog highlighting the entire Cushcraft HF, VHF, and UHF antenna line, write to *Cushcraft, PO Box 4680, Manchester NH 03108.* Reader Service number C67.

GILFER INTRODUCES VERSATILE NEW RF PRESELECTOR/ PREAMPLIFIER WITH AUTOMATIC ANTENNA SWITCHING

If you are missing out on those weak DX signals because your receiver needs more sensitivity, here's a low-cost way to hype it up: Add the new Mizuho SX-59 preselector/preamp from Gilfer.

The SX-59 adds 20 dB of gain (3 or 4 S-units) with low noise. Tunable in 3 switched bands from 3 to 30 MHz, the unit is completely automatic in antenna switching—turn it on and it connects itself to the antenna, turn it off and the antenna is reconnected to the receiver. No manual bypass is needed.

Beautifully styled in a solidly-made beige-colored cabinet, the SX-59 has a built-in, switchable, 20-dB rf attenuator to cope with excessively strong signals, plus a range switch, rf gain control, tuning dial, LED "on" indicator, input and output coax (SO-239 and phono plug) antenna connectors, "remote" terminals, and a built-in power supply for 117 V ac.

It's easy to use. Just select the band and tweak the tuning dial for the maximum signal. You'll be surprised at what you're missing. And if you've an old single-conversion receiver, the SX-59 will also reduce those images by 4 or 5 S-units.

Staco's new RPS-8 power supply.

For complete information, write *Gilfer, Box 239, Park Ridge NJ 07656.* Reader Service number G6.

NEW STACO REGULATED 8-AMP POWER SUPPLY

A new regulated 8-Amp power supply from Staco, Incorporated, is built to operate amateur, commercial, and industrial transceivers, as well as other 12-volt dc equipment, from 120 volts ac.

The solid-state Staco RPS-8 is ideally suited for fixed output power. A unique current foldback circuit and internal circuit breaker provide automatic dual overload and short-circuit protection. In the event of component failure, an automatic crowbar circuit protects equipment from high voltage. The RPS-8 features a surge current of 8.0 Amps, a continuous current of 6.0 Amps, and a full 13.8-volt dc output. Ventilated steel housing is clad with black and white vinyl to prevent scratches or mars. Each unit is complete with input power cord, switch, pilot light, and operating instructions. Output connections are easily made to the terminal board on the rear of the unit. The RPS-8 measures 3-5/8 inches x 5 inches x 8 inches, and is backed by a 90-day limited warranty.

For more information, contact *Staco, Incorporated, 301 Gaddis Boulevard, Dayton OH 45403.* Reader Service number S78.

Corrections

I would like to offer a reed relay update to my October, 1978, article ("Happiness Is A Smart Scanner"). This information is from Allied's catalogue #790 (page 180). The following relays may be used: stock no. 929-377 (mfr. type MRR1ADS), stock no. 850-1552 (mfr. type W107DIP-3), or stock no. 703-2012 (mfr. type AMP2012). Also, please note my new address.

John P. Skubick K8JS
791 106th Ave. N.
Naples FL 33940

I just had a letter from Harold Drennon W0FSC who was nice enough to point out an error that he found in my OSCAR turnstile antenna article in the November, 1977, issue, page 63, Fig. 3. In the 2m driving harness, the wording below coaxial line 2 read λ/RG-62A/U, but should be λ/4 RG-62A/U. This is the first notice of a problem I have had, and I am sorry it was not caught by me in the proofs. The original was okay, but the proofs are still my responsibility. I thoroughly checked the entire article again, while I was at it, and, sure enough, I found one of my own errors. Fig. 1 caption should be: "Vertical mast is 10' ± 5'..." Surely the builders caught that one or they got strange looks when they went shopping!

Dave Brown W9CGI
Noblesville IN

Eric Corbett WD8PYE and others have pointed out a few errors in the wiring diagram and description of the Novice keyer on page 44 of the March, 1978, *73 Magazine.* The following should be noted:

Fig. 1: IC1 pin 7 should be pin 4. C2 should be reversed (negative side grounded).
Fig. 2: D2 should be connected to R6 at the crossover point.
Table 1: With power applied but key not contacting, IC2 pin 5 should be low (not high as indicated).

Several hams have written with these difficulties, along with shorted diodes, etc. None of them has written to me a second time, so hopefully I have been able to explain enough to them to get their keyers working. If you are having any difficulties, and will describe any voltages differing from those in the article (with above corrections), I'll help you out.

Michael Windolph W0OGX
Chaska MN

Ham Help

I need information on how to update or increase the usability of a Hammarlund Super-Pro or BC-779 shortwave receiver. Any info would be appreciated.

Bill Koczon W2HWQ
85 Lakeland Dr.
Bricktown NJ 08723

I would like to convert a Johnson Canadian model Messenger 352 mobile SSB/AM solid-state 23-channel CB transceiver into a 10 meter mobile transceiver. I would greatly appreciate receiving information regarding this conversion.

Raymond Boivin VE2BOL
282 Boul Monaco
Duberger, Quebec
Canada G1P 3H4

Contests

from page 24

other ZS1 stations. All modes or combination of modes permitted. All bands or combination of bands permitted. Closing date for the award is July, 1979. No QSL cards are required. Send a copy of your log verified by 2 local amateurs. Fee: US $1 or 10 IRCs; ZS R1.00. Send applications to: The Award Manager, ZS1MO, PO Box 5100, Cape Town 8000, Republic of South Africa. A special indication is given for VHF contacts.

SECOND ANNUAL INTERNATIONAL SSTV CONTEST

The contest is sponsored by R. Brooks Kendall W1JKF and David Ingram K4TWJ.

CONTEST RULES:

Contest is held annually on the second full weekend of March from 1500 to 2200 GMT, Saturday and Sunday, 3/10/79 and 3/11/79. All amateur bands between 3.5 and 29.7 MHz may be used.

EXCHANGE:

Exchange of pictures should include callsigns, RST report, and contest number. FCC rules require verbal exchange of callsigns for U.S. stations. Do not include contact number.

CREDITS:

1 point for each station worked. A station may be worked once on each band for credit. 1 point for each state or province worked. 5 points for each country worked. 5 points for each continent worked. Total score is the sum of all the credits. Excessive discrepancies in the contest entry may cause disqualification. Entries become the property of the contest committee. The decisions of the contest committee are final.

ENTRIES:

Activity sheets should show station worked, state or province, country, and band (80, 40, 20, 15, 10). Summary sheets should show number of stations worked, number of states or provinces worked, number of countries worked, number of continents worked, and total score. Contest entries should be postmarked no later than 4/10/79. Top scorer will be awarded a certificate and a year's subscription to the magazine of his or her choice. Certificates will also be awarded to the top scorer for the most countries and most continents worked.

Send entries to either: R. Brooks Kendall W1JKF, 10 Stocker Street, Saugus MA 01906, or David Ingram K4TWJ, Eastwood Village, No. 1201 South, Rt. 11, Box 499, Birmingham AL 35210.

THE WORKED ALL WEST AUSTRALIAN SHIRES AWARD AND THE WORKED ALL WEST AUSTRALIAN POST CODES AWARD

To become eligible for these awards, it is necessary for overseas amateurs to work 40 shires and 50 post codes, respectively, with proof of the QSOs to be forwarded to the Contest Committee, c/o PO Box 6250, Hay Street, Perth 6000, Western Australia, along with 10 IRCs or equivalent for the initial award. Subsequent stickers will be issued free, although return postage will be appreciated.

A map of West Australia showing all shires is available from the above address for $2 Australian.

Ham Help

I am with the Canadians in Lahr, West Germany. My problem is this: The D.A.R.C. over here has a large number of QSL cards that belong to DA call holders. I am in the position of trying to locate amateurs and pass on the cards. I am *not* a QSL bureau, just a locating service.

At the time of writing, I find myself with over 5000 cards, DA1, DA2, DA4, and DJ (foreign civilians), all of which the D.A.R.C. is unable to locate. So, for some time now, I have been trying to locate same, with little or no luck. Most of the U.S. Army DA call holders are moving around all the time, including going back home, so a lot of amateurs are without their QSL cards. If you are missing some QSLs, let me know.

Michael R. Jackson
VE3KQI/DA1UO
Postfach 1771
7630 Lahr
West Germany

In the October, 1978, issue of *73 Magazine*, in Ham Help, I asked for a simple modification for the popular Kenwood TR-7400A in order to receive the Civil Air Patrol frequency of 148.15 MHz. A reader (Gerald Gray WA0IKA of Topeka) came up with the mod, and I would like to pass it along for use by other 7400 owners. The only components needed are a small switch and a diode. Connect as follows: With the top cover of the radio removed, install an SPST switch with one lug grounded to the cover. Locate the switch directly behind the CT1 terminal. Connect the cathode of a 1N914 diode to the other switch lug. Add a 2" piece of wire to the anode, and slip shrink tubing over switch lug, diode, and wire. Strip the other end of the wire approximately ½" and wrap it around terminal CT1 on PD board X50 1380 10 (refer to Kenwood manual); no solder is required. Install the cover. Label the switch "Receive, + 600." With this switch in the closed position, I can receive the CAP frequency of 148.15 by setting the display dial of my transceiver on 147.550, and, with the TX offset of +600, I can simplex on the frequency. No change is required to transmit on this frequency, and just turn the switch off to receive the frequency displayed. My thanks to Gerald and *73 Magazine*.

George E. Taylor WA4GUW
Muscle Shoals AL

I need to get in touch with other amateurs, faculty members on the college or university level, who teach biomedical electronics and instrumentation. I'm on the faculty of the University of Texas School of Allied Health Science in Houston.

MDs interested in the subject are also very welcome. However, I am seeking resources on at least the postgraduate level in Health Related Science. In addition, those interested should be "teaching oriented."

Jim McClure WB5MHA
801 S. Braeswood, Apt. 1313
Houston TX 77031

We recently obtained a multimeter, ME-26 D/U, serial no. 7747 (similar to HP-410B), manufactured by Sentinel Electronics, Inc. The company is not listed in the *Electronics Buyer's Guide*, and may be out of business. We need the operator's manual and schematic. Thanks for any assistance.

Heritage Christian School
Warren Pettit
Box 50002
6401 East 75th St.
Indianapolis IN 46250

I need the manual for a Heathkit Model V-6 vacuum tube voltmeter. I will gladly reimburse reasonable duplicating and mailing expenses, or I will duplicate on receipt and send back by return mail. Thanks.

V.F. Smith VE1BEA
46 Beaconsfield St.
Fredericton, New Brunswick
Canada E3B 5H2

I would like to hear from people who are using the FCC experimental band and learn where I can get plans for transceivers, transmitters, and receivers.

Rick Todd KA8AKL/N
14470 Bassiake Road
Newbury OH 44065

I need a photocopy of *Surplus Schematic Handbook* (red and black, with white schematic on cover, part of *CQ* series, 8½ x 11 inches). Also need photocopy of Wolf's *Motorola Schematic Digest* and photocopy of manual or diagram for National NC-200 receiver.

Finally, I need Knight Signal Tracer and any data, and rigs for two meters in any condition.

John C. White WB6BLV
560 North Indiana
Porterville CA 93257

I would like to obtain a copy of the manual, or at least the schematic, for the Heathkit Model VF-1 vfo. I'll be happy to pay postage and copy costs. Thanks!

Mark F. Allen WD6GZJ
11401 Snowdrop Ave.
Fountain Valley CA 92708

I have an old Hallicrafters S-85 receiver and would like to modify and utilize it for DX work as the receiver is extremely sensitive. I am in need of a schematic and operator's manual. Thanks.

Charles Bott DL-579/WW
PSC Box 56
APO NY 09123

I am in need of an operations manual and schematic for a Dumont Labs type 350-R oscilloscope. I will pay for copies, or whatever arrangement we can come up with.

James G. Brown
15 New Ocean St.
Lynn MA 01902

I need a manual or complete schematic for a Motorola 41 V dispatcher (high band, 110/12 volts). It is needed for a club project.

Chuck Bennett WB8GQW
17060 Paver-Barnes Rd.
Marysville OH 43040

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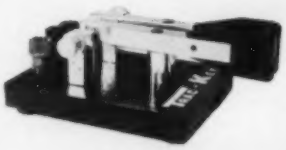

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✓ Reader Service—see page 211

Social Events

MADISON WI
FEB 8-11

The 1979 Spirit of Ballooning Fiesta will be held on February 8-11, 1979, in Madison, Wisconsin. This is a national convention of hot-air balloonists. On the 8th and 9th, 10 balloons will take off each afternoon. On the 10th and 11th, eighty balloons are scheduled to lift off. Amateurs interested in providing communications should contact Clyde Downing W9HSY, PO Box 3403, Madison WI 53704, (608)-244-4744, or contact him on the Madison 16/76 two meter machine. Please provide days and type of equipment available (base, mobile, HT, etc.). K9BIL or K9VAL may also be contacted.

TRAVERSE CITY MI
FEB 10

The Cherryland Amateur Radio Club will hold its annual Swap & Shop on February 10, 1979, from 9:00 am to 4:00 pm, at Northwestern Michigan College Technical Center, Front St., Traverse City, Michigan. For information, please contact Greg North, Box 115, Lake Leelanau MI 49653.

MANCHESTER NH
FEB 10

The Interstate Repeater Society will hold its 3rd annual auction and hamfest on February 10, 1979, beginning at 9:00 am, at the Manchester Armory, across the Amoskeag Bridge from I-93, in Manchester, New Hampshire. There will be commercial exhibits, and the auction will be held rain or shine. Admission and parking are free. Talk-in on 146.52, 146.25/.85, and 224.86/223.46. For information, contact Gary A. Delong WB7NOH/KA1BCA, Interstate Repeater Society, PO Box 94, Nashua NH 03061.

MANSFIELD OH
FEB 11

The Mansfield midwinter hamfest/auction will be held on February 11, 1979, in a heated building at the Richland County Fairgrounds in Mansfield, Ohio. There will be prizes and a flea market. Doors will open to the public at 8:00 am. Talk-in on 146.34/.94. Advance tickets are $1.50; $2.00 at the door. For information, contact Harry Frietchen K8HF, 120 Homewood,

SST ACCESSORIES

SST T-3

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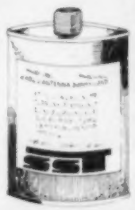
The SST DL-1 is a unique non-corrosive chemical dummy load which has been developed and tested by K4RLJ for 12 years. There is no other dummy load like it. Unlike messy oil filled dummy loads, the DL-1 will not leak. It is sealed and ready to use.

A dummy load is a must for any ham station. High input to small size ratio makes the DL-1 ideal for portable, base station, and work bench operation for hams and commercial users. Accurate readings will result when used with SWR and power meters.

Specifications:
Max. power: 1000 watts PEP for 15 seconds.
SWR: less than 1.5:1 1 MHz - 225 MHz.
Size: 3-1/8" X 4-3/8"



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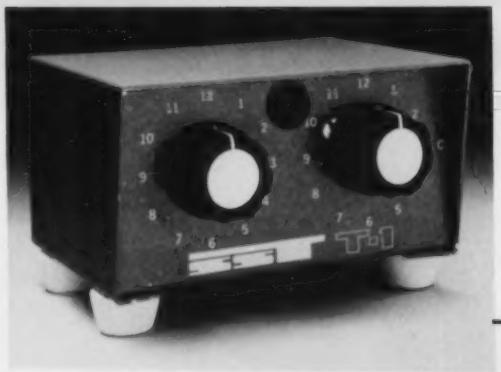
SST T-1 RANDOM WIRE ANTENNA TUNER



All band operation (160-10 meters) with any random length of wire. 200 watt output power capability - will work with virtually any transceiver. Ideal for portable or home operation. Great for apartments and hotel rooms—simply run a wire inside, out a window, or anyplace available. Efficient toroid inductor for small size: 4-¼" x 2-⅜" x 3", and negligible loss. Built-in neon tune-up indicator. SO-239 connector. Attractive bronze finished enclosure.

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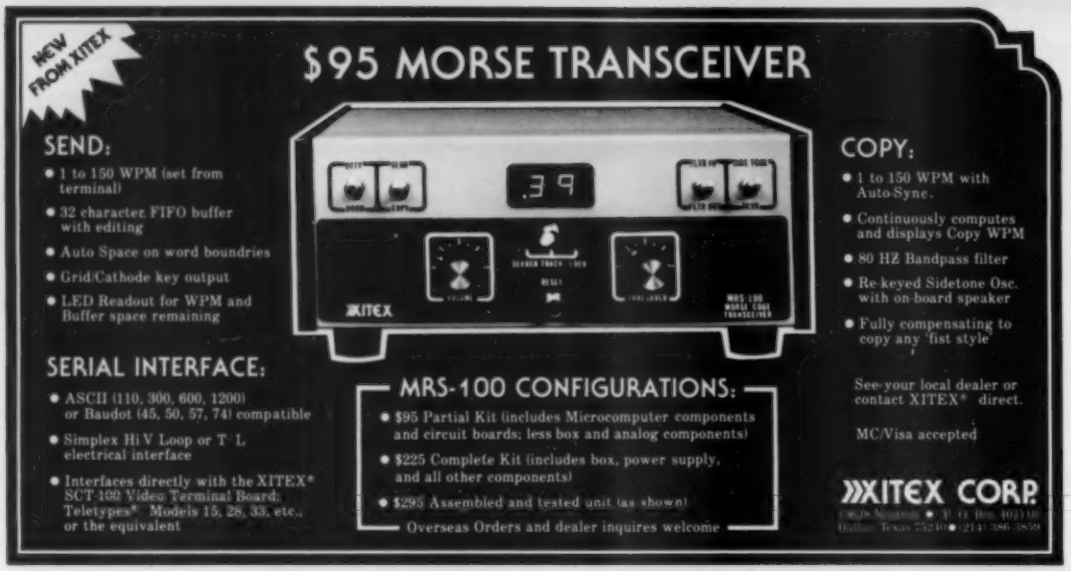
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LANCASTER PA
FEB 18

The 7th annual Lancaster hamfest will be held on Sunday, February 18, 1979, at the Guernsey Sales Pavilion, US Rt. 30 & PA Rt. 896, Lancaster, Pennsylvania. Doors will open at 8:00 am and there will be a prize drawing at 2:00 pm. Admission is $3.00, and table reservations are $2.00 in advance. There is a new, larger indoor flea market area. Food and soft drinks will be available. Talk-in on 146.01/.61. For further information, contact SERCOM, PO Box 6082, Rohrerstown PA 17603.

MARLBORO MA
FEB 24

The Algonquin Amateur Radio Club will hold its annual electronic flea market on Saturday, February 24, 1979, from 10:00 am to 4:00 pm, at St. Mary's School Hall on Broad Street in Marlboro, Massachusetts. There is easy access to the Hall from I-495 via Rt. 20 east. Seller setup is from 9:00 am to 10:00 am. Talk-in on .52. Sellers should contact Charlie W1BK at (617)-562-5622.

VIENNA VA
FEB 25

The Vienna Wireless Society will hold its annual Winterfest on Sunday, February 25, 1979, at the Vienna Community Center, Vienna, Virginia. There will be tables, sales, prizes, food, and frostbite tailgating. Doors open at 6:30 am for vendors and 8:00 am for the general public. Admission is $3.00, including one prize ticket; $2.00 for an extra prize ticket, and $1.00 for frostbite tailgaiting. Preteens with parents are free. Tables range from $2.00 to $5.00, depending on the quantity. Reservations close on February 15, 1979. For reservations, contact Carroll N. Guin, 7533 Oak Glen Court, Falls Church VA 22042. For information, contact the Vienna Wireless Society, PO Box 418, Vienna VA 22180.

LIVONIA MI
FEB 25

The Livonia Amateur Radio Club would like to announce that the 9th annual LARC Swap 'n Shop will be held on Sunday, February 25, 1979, from 8:00 am to 4:00 pm, at the new location of Churchill High School in Livonia MI. Tables, door prizes, refreshments, and free parking will be available. Talk-in on 146.52 simplex. Reserved table space of 12-foot minimum is available. For further information, send an SASE to Neil Coffin WA8GWL, c/o Livonia Amateur Radio Club, PO Box 2111, Livonia MI 48151.

LAPORTE IN
FEB 25

The LaPorte Amateur Radio Club will hold its winter hamfest on Sunday, February 25, 1979, at the LaPorte Civic Auditorium, LaPorte, Indiana. There is a $1.00 table charge. Donation is $2.00 at the gate. Talk-in on .01/.61 and .52. For more information, contact LARC, Box 30, LaPorte IN 46350.

AKRON OH
FEB 25

The Cuyahoga Falls Amateur Radio Club will hold its annual electronic equipment auction and flea market on Sunday, February 25, 1979, at North High School, Akron, Ohio, from 9:00 am to 4:00 pm. Tickets are $2.00. You may bring your own tables, and there will be some available for $2.00 each. There will be refreshments, prizes, and a grand prize of a Triton IV. There is easy access to the high school on the Tallmadge Avenue off-ramp and the North Expressway (Rt. 8). Talk-in on 146.52 and 146.04/.64. For details, write CFARC, PO Box 6, Cuyahoga Falls OH 44222, or phone Bill Sovinsky K8JSL at (216)-923-3830.

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DAVENPORT IA
FEB 25

The Davenport Radio Amateur Club will hold its hamfest on February 25, 1979, at the Masonic Temple in Davenport, Iowa. Admission is $2.00 in advance, $2.50 at the door. Refreshments and tables will be available. Talk-in on .28/.88 and .52. For further information, send an SASE to John S. Birmingham WB0QCC, 2022 Brown St., Davenport IA 52804.

CIRCLEVILLE OH
MAR 4

The King of the Pumpkin Ham Fiesta, sponsored by the Teays Amateur Radio Club, will be held from 9:00 am to 5:00 pm

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on Sunday, March 4, 1979, at the fairgrounds coliseum, Circleville, Ohio. There will be an indoor flea market, new and used equipment, door prizes, refreshments, and free parking. Table spaces are available at $3.00 each. Advance admission is $1.00; $2.00 at the door. For advanced reservations and information, contact Dan Grant W8UCF, 22150 Smith Hulse Road, Circleville OH 43113; (614)-474-6305.

STERLING IL
MAR 4

Sterling Rock Falls Amateur Radio Society will hold its annual hamfest on March 4, 1979, at the Sterling High School Fieldhouse, 1608 4th Avenue, Sterling, Illinois. Tickets are $1.50 in advance; $2.00 at the door. A large indoor flea market is restricted to radio and electronic items only. There is plenty of free parking available, including an area to accommodate campers and mobile trailers. There will be no advance sale of tables. We will take reservations for commercial enterprises only. There will be bargains, miscellaneous prizes, and food. Talk-in on 146.94. For tickets, write Don VanSant WA9PBS, 1104 5th Avenue, Rock Falls IL 61071. Make checks payable to Sterling Rock Falls Amateur Radio Society. Please include an SASE.

FLEMINGTON NJ
MAR 17

The Cherryville Repeater Association will hold its annual hamfest on March 17, 1979, from 10:00 am to 5:00 pm, at the Field House of Hunterdon Central High School, just north of Flemington, New Jersey, on

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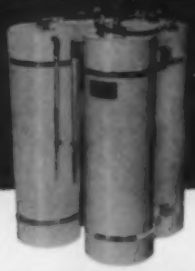

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VERO BEACH FL
MAR 17-18

The Treasure Coast Hamfest will be held on March 17-18, 1979, at the Vero Beach Community Center, Vero Beach, Florida. Activities will include prizes, drawings, and a QCWA luncheon. Admission is $3.00 per family. Talk-in on 146.13/.73, 146.52/.52, and 222.34/223.94. For information, write PO Box 3088, Vero Beach FL 32960.

JEFFERSON WI
MAR 18

The Tri County ARC Hamfest will be held on March 18, 1979, at the Jefferson County Fair Grounds, Jefferson, Wisconsin. Advance tickets are $1.50. Reserved 6-foot tables are $2.00 in advance, while 6-foot space is $1.00. For information, send an SASE to Glenn Eisenbrandt WA9VYL, 711 East Street, Fort Atkinson WI 53538.

LAWTON OK
MAR 23-25

The Lawton Fort Sill Amateur Radio Club, Inc., will hold its 33rd annual hamfest at the Montego Bay Motel Complex at Lawton, Oklahoma, the weekend of March 23-25, 1979. There will be the usual large flea market, ARRL officials, technical programs, QCWA breakfast, and activities for the ladies.

EAST RUTHERFORD NJ
MAR 24

The Knight Raiders VHF Club, Inc., will hold its world-famous flea market at St. Joseph's Church, East Rutherford, New Jersey, on Saturday, March 24, 1979. Doors open at 10:00 am. There will be free admission and free parking. Refreshments will be available. Flea market tables are available for: $5.00/full table or $3.00/half table, in advance; $6.00/full table or $3.50/half table, at the door. Talk-in on 146.52 and 144.65/145.25. For further information, call Bob Kovaleski at (201)-473-7113 or Jack Mandelberger at (201)-857-0016 (evenings only). Send reservations to: R. Wetzel, 419 Union Ave., Rutherford NJ 07070, and make checks payable to: Knight Raiders VHF Club, Inc.

WAUKEGAN IL
MAR 25

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lein Amateur Radio Society will hold its second annual Lamarsfest on Sunday, March 25, 1979, at the J. M. Club, 708 Greenwood Ave., Waukegan, Illinois. Doors will open at 7:00 am. There will be plenty of free parking, door prizes, and a large indoor flea market for radio and electronic items. Tables will be available at $4.00 each. Advance tickets are $1.50; $2.00 at the gate, with children under 10 free. Hot lunch will be available and there will be plenty of commercial exhibits and demonstrations. Talk-in on 146.94. For further information, write LAMARS (include SASE, please) at 1226 Deer Trail Lane, Libertyville IL 60048, or call (312)-367-1599.

MUSKEGON MI
MAR 30-31

The Muskegon Area Amateur Radio Council is sponsoring the ARRL Great Lakes Division Convention and Hamfest at the Muskegon Community College in Muskegon, Michigan, on March 30-31, 1979. This event will feature manufacturers' exhibits, technical forums, and a large swap shop. Ample parking and dining facilities are available. Friday evening at the Muskegon Ramada Inn, there will be a "Ham Hospitality" with libation courtesy of the MAARC and a Wouf Hong initiation. For additional information, contact MAARC, PO Box 691, Muskegon MI 49443, or H. Riekels WA8GVK, (616)-722-1378/9.

COLUMBUS GA
MAR 31-APR1

The Columbus Amateur Radio Club will hold first annual hamfest from March 31-April 1, 1979, at the Columbus Municipal Auditorium, US 27 & 280, Columbus, Georgia. Donation is $1.00 at the door. There will be plenty of free parking and overnight free RV space. Exhibitors and flea market will be inside, with a free flea market outside. Talk-in on 28/88. For advance registration and details, write Bob Glasgow N4BGN, 1503 Layard Drive, Columbus GA 31907; (404)-561-7746.

WILLIAMSPORT PA
APR 29

The West Branch Amateur Radio Association will hold its 15th annual Penn Central Hamfest on Sunday, April 29, 1979, from 11:00 am to 5:00 pm at the Woodward Township Fire Hall, Rt. 220 south from Williamsport. For more information, write Richard Sheasley K3QDA, RD 1, Box 454, Linden PA 17744, or call Tony at (717)-322-6017.

NEENAH WI
MAY 5

The 3-F Amateur Radio Club will hold its annual swapfest on Saturday, May 5, 1979, from 8:00 am to 3:00 pm, at the Neenah Labor Temple, 157 S. Green Bay Road, Neenah, Wisconsin, just off Highway 41 at the Highway 114 or 150 exit. Facilities include a large parking area and a large indoor swap area with a free auction at the end of the day. Food and beverage will be available. Advance admission for tickets and tables is $1.50; $2.00 at the door. Talk-in on 52/52. For reservations, write to Mark Michel W9OP, 339 Naymut Street, Menasha WI 54952.

SALINE MI
MAY 13

The ARROW Repeater Association will hold its annual Swap and Shop on Sunday, May 13, 1979, at the Saline, Michigan, fairgrounds. Admission, including parking on the fairgrounds, is $1.50 in advance and $2.00 at the door. There will be food, prizes, and a covered area for trunk sales, as well as indoor tables. Because of Mother's Day, wives will be given free admission. Talk-in on 146.37/97, 223.18/224.78, and 448.5/443.5 MHz. For additional details, write ARROW, PO Box 1572, Ann Arbor MI 48106, or call George Raub AD8X at (313)-485-3562.

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Lin Hamilton WB6PAV
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Hopefully, your Ham Help column can help me find the information I want. I would like to get in touch with anyone who is still using an old Galaxy V transceiver on the air today and find out what their opinions are of it.

Rick Todd KA8AKL/N
14470 Basslake Road
Newbury OH 44065

I would very much appreciate help from anyone in finding a circuit diagram of the McMurdo Silver Masterpiece VI.

Reg Trickey G3DRB
31 Pensby Ave.
Chester, England

I would like to obtain a copy of the original owner's manual for a Viking "Courier" linear amplifier.

John I. Nelson AA7W
19025 73rd Avenue N.E.
Bothell WA 98011

I need a schematic for a Johnson Model 122 vfo. Any help in obtaining this will be greatly appreciated.

Bill Richmond WD4CPQ
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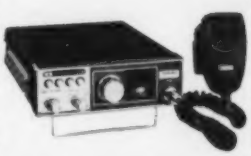

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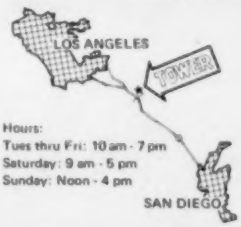

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106	.80	179	5.69	229	1.06	298	1.13
107	.79	180	5.68	230	3.60	299	2.02
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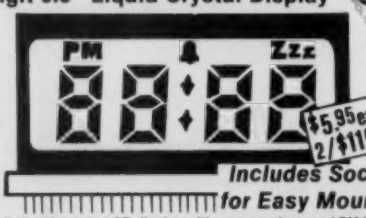

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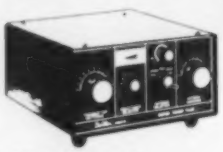

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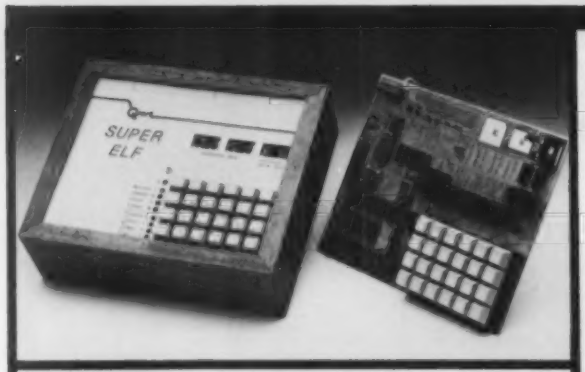

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Compare features before you decide to buy any other computer. There is no other computer on the market today that has all the desirable benefits of the **Super Elf** for so little money. The Super Elf is a small single board computer that does many **big** things. It is an excellent computer for training and for learning programming with its machine language and yet it is easily **expanded with additional memory, Tiny Basic, ASCII Keyboards, video character generation, etc.**

The **Super Elf** includes a **ROM** monitor for program loading, editing and execution with **SINGLE STEP for program debugging** which is not included in others at the same price. With **SINGLE STEP** you can see the microprocessor chip operating with the **unique Quest** address and data bus displays **before, during** and **after** executing instructions. Also, CPU mode and instruction cycle are shown on several LED indicator lamps.

An RCA 1861 **video graphics** chip allows you to connect to your own TV with an inexpensive video modulator to do graphics and games. There is a **speaker system** included for writing your own music or using many music programs already written. The speaker amplifier may also be used to drive relays for control purposes.

A 24 key **HEX keyboard** includes 16 HEX keys plus **load, reset, run, input, memory protect, memory select, monitor select** and **single step**. Large, on board displays provide output and optional **high and low address**. There is a 44 pin standard connector for PC cards and a 50 pin connector for the **Quest Super Expansion Board**. Power supply and sockets for **all** IC's are included in the price plus a detailed 90 page instruction manual.

Many schools and universities are using the Super Elf as a course of study. OEM's use it for training and research and development.

Remember, other computers only offer Super Elf features at additional cost or not at all. **Compare before you buy. Super Elf Kit $106.95, High address option $8.95, Low address option $9.95. Custom Hardwood Cabinet** with drilled and labelled front panel **$24.95. NiCad Battery Backup Kit $4.95.** All kits and options also come completely assembled and tested.

Questdata, a 12 page monthly software publication for 1802 computer users is available by subscription for $12.00 per year. New 100 page software manual Vol.1 $4.95.

Tiny Basic for ANY 1802 System

Cassette $10.00. On ROM Monitor $30.00. Super Elf owners, 30% off. **Object code listing or paper tape with manual $5.50. Original ELF Kit Board $14.95.**

Super Expansion Board with Cassette Interface $89.95

This is truly an astounding value! This board has been designed to allow **you** to decide how you want it optioned. **The Super Expansion Board comes with 4K of low power RAM** fully addressable anywhere in 64K with built-in memory protect and a **cassette interface**. Provisions have been made for all other options on the same board and it fits neatly into the hardwood cabinet alongside the **Super Elf**. The board includes slots for up to 6K of **EPROM** (2708, 2758, 2716 or TI 2716) and is **fully socketed** ($12.00 value). EPROM can be used for the monitor and Tiny Basic or other purposes.

A 1K Super ROM Monitor $19.95 is available as an on board option in 2708 EPROM which has been preprogrammed with a program loader/editor and error checking multi file cassette read/write software, (relocatible cassette file) another exclusive from Quest. It includes register save and readout, block move capability, and video graphics driver with blinking cursor. The Super Monitor is written with subroutines allowing users to take advantage of monitor functions simply by calling them up. Improvements and revisions are easily done with the monitor. If you have the **Super Expansion Board** and **Super Monitor** the monitor is up and running at the push of a button.

Other on board options include **Parallel Input and Output Ports** with **full handshake**. They allow easy connection of an ASCII keyboard to the input port. **RS 232 and 20 ma Current Loop** for teletype or other device are on board and if you need more memory there are two **S-100** slots for static RAM or video boards. A Godbout 8K RAM board is available for $135.00. **Parallel I/O Ports $9.85, RS 232 $4.50, TTY 20 ma I/F $1.95, S-100 $4.50. A 50 pin connector set** with ribbon cable is available at $12.50 for easy connection between the **Super Elf** and the **Super Expansion Board.**

The **Power Supply** for the Super Expansion Board is a 5 amp supply with + 8v ± 1By + 12v – 5v. Regulated voltages are ±5v & +12v $29.95, –12 volt optional. Deluxe version includes the case at $39.95.

INTEGRATED CIRCUITS

7400TTL							
7400N	17	LM340T-18	1.10	CD4011	.54	6212	2.90
7401N	17	LM340T-20	1.10	CD4015	2.50	6214	6.90
7402N	17	LM340K	4.50	CD4016	1.10	6216	2.90
7404N	19	LM370	1.15	CD4518	1.02	6224	2.90
7408N	23	LM377	4.50	CD4520	1.52	6228	5.55
7410N	17	LM379	5.00	CD4527	1.51	6251	6.50
7411N	62	LM380N	1.00	CD4528	.79	6253	10.00
7420N	17	LM381	1.60	CD4553	5.75	6255	9.25
7427N	1.20	LM382	1.60	CD4566	2.25	6257	19.50
7430N	39	LM703H	.40	CD4583	4.50	6259	19.50
7442N	39	LM709H	.29	CD4585	1.10	CDP1802CD	19.95
7445N	69	LM723H/N	.50	CD40192	3.00	CDP18020	25.00
7447N	60	LM7339	.67	74C00	.29	CDP1861	12.95
7448N	60	LM741CH	.35	74C04	.33	6800	9.95
7450N	17	LM741N	.25	74C10	.29	6810	12.95
7470N	20	LM747HN	.60	74C14	2.50	6820	12.50
7472N	20	LM7486	.75	74C20	.29		
7486N	.89	LM1303N	.80	74C30	.29		
7427N	2.09	LM1304	1.10	74C42	1.05		
7430N	.49	LM1310	1.27	74C74	.70		
7460N	.49	LM1337	3.99	74C76	1.49		
7472N	.43	LM1310	3.75	74C86	1.15		
7495N	.99	LM1458	.47	74C93	1.40		
74100N	.99	LM1800	1.75	74C154	3.00		
74107N	.33	LM1811	7.00	74C160	1.44		
74121N	.34	LM1889	3.00	74C175	1.35		
74123N	.59	LM2111	1.75	74C192	1.60		
74145N	.69	LM2900N	.69	74C221	2.25		
74151N	.69	M2002	1.75	74C905	3.00		
74153N	.69	M2003	1.75	74C906			
74157N	.69	MC3999N	.61	74HC914	1.85		
74174N	1.09	MC1456N	.50	74HC922	5.00		
74175N	.69	MS408L	2.00	74HC923	5.95		
74181N	.67	NE555N	.40	74HC925	6.95		
74182N	.67	NE556N	.63	74HC926	6.95		
74190N	.87	NE558V	.79	74HC927	6.95		
74191N	.87	NE566A	1.00				
74192N	.69	NE568V	1.50	**MEMORIES**			
74193N	1.15	NE567V	1.00	2101	.85		
74197N	.67	NE570N	5.00	2102	.60		
74198N	.89	NE571N	5.00	2111	.85		
74221N	.69			2112	.85		
74232N	.69			2114	3.00		
74367N	.99			2147	17.95		
		7545ION	.33	6810	3.75		
74LS00 TTL		7546ION	.55	6813	3.95		
74LS00N	.23	7549HON	.69	6815	3.00		
74LS02N	.23			6816	1.69		
74LS03N	.23	**A to D CONVERTERS**		6820	2.75		
74LS04N	.23	0804LCN	4.99	6821	2.00		
74LS08N	.23	0808CJ	13.95	6830	1.69		
74LS10N	.23	0816CN	22.00	6834	1.69		
74LS13N	.49	0756CJ	13.95	6850	1.69		
74LS14N	.99	LD130	9.95				
74LS20N	.23	0480CJ/CP	7.40	**MICROMEMORY RAM**			
74LS22N	.25	ICL7103	9.50	2101-1	3.95		
74LS26N	.41	ICL7107	14.25	2102-1	.95		
74LS30N	.25			2102L-4	1.20		
74LS33N	.39	**CMOS**		2102L-4	1.60		
74LS38N	.35	CD4001 Per	.50	2111-1	3.95		
74LS74N	.35	CD4000	.16	2112-2	3.95		
74LS75N	.47	CD4001	.21	2114	8.50		
74LS86N	.51	CD4002	.21	2147	17.95		
74LS93N	.51	CD4006	1.10	2513B	6.30		
74LS95N	1.89	CD4007	.21	2LG2-1	1.29		
74LS107N	.35	CD4008	.40	MM5262	.95		
74LS112N	.35	CD4009	.39	MM5280	3.00		
74LS113N	.35	CD4010	.39	MM5320	9.85		
74LS132N	.79	CD4011	.21	MM5330	5.95		
74LS138N	.59	CD4012	.21	P04110-3	4.69		
74LS151N	.67	CD4013	.36	P04110-4	5.00		
74LS155N	.67	CD4014	.65	P5101L	13.95		
74LS157N	.67	CD4015	.65	4200A	9.95		
74LS158N	.67	CD4016	.36	MM5290	2.95		
74LS163N	.91	CD4017	.64	91L02A	1.75		
74LS174N	.95	CD4018	.64	HD0165-5	6.50		
74LS190N	1.05	CD4019	.21	MM57100	7.50		
74LS221N	1.95	CD4020	1.02	GIAY38500-1	9.95		
74LS259N	.67	CD4021	.65	MM5671A	12.95		
74LS367N	.89	CD4022	.65	9368	3.50		
		CD4023	.21	4108	10.00		
LINEAR		CD4024	.70	4116	16.50		
CA3045	.00	CD4025	.21				
CA3046	.00	CD4026	1.51	**CLOCKS**			
CA3081	1.99	CD4027	.36	MM5309	5.00		
CA3082	1.99	CD4028	.79	MM5311	5.60		
CA3083	1.99	CD4029	1.02	MM5312	5.60		
LM301AN/H	.35	CD4030	.21	MM5313	5.50		
LM309H	.67	CD4031	1.02	MM5314	5.00		
LM307N	.39	CD4032	.65	MM5316	5.00		
LM308N	.59	CD4042	.71	MM5318	5.00		
LM309H	1.15	CD4043	.69	MM5369	5.00		
LM309K	.99	CD4044	.63	MM58389	2.10		
LM311N/D	.69	CD4046	1.67	MM58341	10.40		
LM317T/K	1.99	CD4047	.96	MM58365	7.95		
LM318	1.35	CD4066	.36	CT7001	5.00		
LM320H-5	1.20	CD4081	1.13	CT7002	6.00		
LM320K-5	1.20	CD4082	.21	CT7010	5.00		
LM320H-12	1.20	CD4085	.71	CT7015	7.25		
LM320K-12	1.20	CD4089	.49	MM53758A/N	2.00		
LM320T-5	1.69	CD4093	.65	MM53758A/N	2.00		
LM320T-12	1.69	CD4070	.40	7208	10.50		
LM320T-15	1.69	CD4071	.21	7207	7.50		
LM320T-15	1.69	CD4072	.21	7208	15.95		
LM324N	1.15	CD4073	.21	7206	4.95		
LM339N	.89	CD4075	.21	0560260N	3.75		
LM340K-5	1.10	CD4076	1.79	0560560N	3.75		
LM340K-8	1.10	CD4078	.40	MM53104	2.50		
LM340K-12	1.10	CD4081	.21				
LM340K-15	1.10	CD4082	.21	**MICROPROCESSORS**			
LM340K-18	1.10	CD4085	.67	8008	17.00		
LM340T-5	1.10	CD4449	5.00	8080	24.95		
LM340T-6	1.10	CD4027	1.00	8080A with data	9.95		
LM340T-12	1.10	CD4030	1.00	8085	27.95		
LM340T-15	1.10	CD4510	1.02	Z80A	24.50		

IC SOCKETS

Solder Tail Low Profile

PIN	WIRE WRAP	TIN	GOLD
8	15	22	30
14	18	24	32
16	20	25	42
18	27	30	58
20	29	40	52

3 level wire wrap gold
14 pin 20 ... 16 pin .27
22 and 24 pin wire wrap

WIRE WRAP LEVEL 3

PIN	PIN
8	24
14	28
16	35
18	40
22	1.25

UART/USRT

AY5-1013	5.00
AY5-1014	7.95
3341	6.95

PROM

1702A	3.50
MM5L03	2.95
MM5123	3.50
MM5126	3.75
MM5129	3.75
MM5131	3.75
MM5133	6.75
MM5137	6.75
2708	10.50
2708/27	7.95
8223	4.00
2716/1	22.50
2716 Intel	49.00

CRYSTALS

1 MHz	4.50
2 MHz	4.69
4 MHz	4.25
5 MHz	4.25
10 MHz	4.25
18 MHz	5.60
20 MHz	5.90
32 MHz	5.60
32768 MHz	4.50
1.8432 MHz	4.50
2.5795 MHz	4.50
2.0100 MHz	4.50
2.097152 MHz	4.50
2.4576 MHz	4.50
3.2768 MHz	4.50
5.0665 MHz	4.50
5.185 MHz	4.50
5.7143 MHz	4.50
6.5536 MHz	4.50
14.31818 MHz	4.50
18.432 MHz	4.50
22.1184 MHz	4.50

CONNECTORS

44 pin edge	2.00
100 pin edge	4.50
100 pin edge WW	4.50

KEYBOARD ENCODERS

AY5-2376	$4.50
AY5-3600	13.50
74C923	5.00
74C923	5.50
HD0165-5	6.95

IC Test Clips

1	19
Red .65	.47
Black .65	.47

Super 8643 14.50
comp. w/spec. sock.

TRANSISTORS

2N1893	40	1600 mtg	2000 4.50
2N2102	40	1600 mtg	400 3.50
2N2369	30	3069	90V 3.50
2N2904A	25	3069	60V 3.00
2N2907A	25	5869	40V 3.00
2N3053	40	6149	40V 3.00
2N3638	25	6199	60V 3.00
2N3643	25	7769	60V 3.50
2N3644	25	8869	90V 3.50
2N3645	25	8869	60V 3.50
2N3646	25	10869	30V 2.90
2N3702	25	10869	60V 3.50
2N4036	25	10869	90V 3.50
2N4037	25	30869	30V 5.00
2N4401	25	30869	60V 5.00
TIP31	60	30869	90V 5.00
TIP33A	1.00	160000	18V 6.00

CLOCK MODULES Complete alarm clocks ready to hook up with transformer and switches. Very compact with .56" and .86" digits.

MA1002A, C or E .56"	8.95
1002P3 Transformer	3.29
MA1016A, C or E .86"	11.95
1602P2 Transformer	3.29
Special transformer and six switches when purchased w/module	3.00
MA1002 Low module .5" green fluor. display	19.95

RESISTORS ¼ watt 5%

10 per type .03	1000 per type .012
25 per type .025	5000 per type .010
100 per type .015	5 per type 6.75

KEYBOARDS

58 key ASCII keyboard kit	$82.50
Fully assembled	72.50
53 key ASCII keyboard kit	59.00
Fully assembled 65.00 Enclosure 14.95	

LEDS

Red T01¾	.10
Green, Orange, Yellow T01¾	.20
Jumbo Red	.20
Green, Orange, Yellow Jumbo	.25
Dialight LED Mounting Clips .5/$1.25	
(specify red, amber, green, yellow, clear)	

CONTINENTAL SPECIALTIES in stock
Complete line of breadboard test equip.
MAX 100 8 digit Freq. Ctr. $139.95

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+ .2° accuracy. Comp. Assy. in compact case. Switches from F° to C°.

COMPUTER BOARD KITS

8K RAM Board Kit	$134.95
4K EPROM Kit	114.95
I/O Board Kit	44.50
Extender Board w/connector	12.50
Video Interface board kit	123.00
16K EPROM board kit w/o PROMS	74.50
16K Static RAM board kit	399.00
North Star Floppy Disc Kit	$995.00
Additional Drive Kit	475.00

SPECIAL PRODUCTS

MM5865 Stopwatch Timer	9.00
PC board	7.50
Switches Mom. Pushbutton	.77
3 pos. slide	.35
Solder HD0165-5	6.95
2 Digit Universal Counter Board Kit	
Includes: 7-.18 VAC DC to 10 MHz typ. 125° LED display	19.50
Voice activated switch	.50

Paraphernalia 100A Logic Analyzer Kit $231.00

Model 10 Trigger	
Expander Kit	$239.00
Model 100 Box	
Grabber Kit	$369.00

TRANSFORMERS

117 VAC 300 ma	3.25
12 Volt 300 ma transformer	1.25
12.6V CT 300 ma	3.75
12V 350 ma wall plug	2.95
12V CT 250 ma wall plug	3.50
24V CT 500 ma	3.95
10V 1.2 amp wall plug	4.85
12V 6 amp	12.95

DISPLAY LEDS

MAN1	CA	.270	2.90
MAN3	CC	.125	.39
MAN7274	CA/CC	.300	1.00
DL704	CC	.300	1.25
DL707/DL707R	CA	.300	1.00
DL727/728	CA/CC	.500	1.99
DL747/755	CA/CC	.600	1.99
DL759	CC	.600	1.95
FND70	CC	.300	1.25
FND500/507	CC/CA	.500	1.35
FND503/510	CC/CA	.500	.99
FND800/857	CC/CA	.800	2.20
3 digit Bubble			.60
4 digit Bubble			.60
DS8 Fluorescent			1.75
DS10 Fluorescent			1.75
4 digit 1/2 pin display			1.00
MAN80 9 digit display			.60
7520 Opto-isolator photocells			.39
TIL311 Hex			9.50

COMPUTER GRADE CAPS

1000	mfd	200V	4.50
1000	mfd	40V	2.50
3300		50V	3.50
3300		16V	2.00
5800		40V	3.00
6100		40V	3.00
8100		25V	3.00
7700		50V	3.50
8800		50V	3.50
10000		50V	3.50
16000		25V	3.50
16000		50V	5.00
22000		25V	3.50
22000		50V	5.00
33000		16V	3.00
33000		25V	3.50
33000		50V	6.00
47000		16V	3.50
47000		25V	4.00
47000		50V	6.00
100000		16V	6.00

Auto Clock Kit $15.95

DC clock with 4-.50" displays. Uses National MA-1012 module with alarm option. Includes light dimmer, crystal timebase PC boards. Fully regulated, comp. instructs. Add $3.95 for beautiful dark gray case. Best value anywhere.

RCA Cosmac VIP Kit $229.00

Video computer with games and graphics. Fully assem. and test. **$249.00**

Not a Cheap Clock Kit $14.95

Includes everything except case. 2-PC boards. 6-.50" LED Displays. 5314 clock chip, transformer, all components and full instrucs. Green and orange displays also avail. **Same kit w/.80" displays.** Red only. **$21.95** Case **$11.75**

60 Hz Crystal Time Base Kit $4.40

Converts digital clocks from AC line frequency to crystal time base. Outstanding accuracy. Kit includes: PC board, IC, crystal, resistors, capacitors and trimmer.

Digital Temperature Meter Kit

Indoor and outdoor. Switches back and forth. Beautiful, 50" LED readouts. Nothing like it available. Needs no additional parts for complete, full operation. Will measure –100° to +200°F, tenths of a degree, air or liquid. Very accurate. **$39.95**
Beautiful woodgrain case w/bezel **$11.75**

NiCad Battery Fixer/Charger Kit

Opens shorted cells that won't hold a charge and then charges them up, all in one kit w/full parts and instructions. **$7.25**

PROM Eraser

Ultraviolet, assembled **$34.50**

Clock Calendar Kit $23.95

CT7015 direct drive chip displays date and time on .6" LEDS with AM-PM indicator. Alarm/dozs feature includes buzzer. Complete with all parts, power supply and instructions, less case.

Sinclair 3½ Digit Multimeter

Batt./AC oper. 1mV and .1NA resolution. Resistance to 20 meg. 1% accuracy. Small, portable, completely assem. in case. 1 yr. guarantee. Best value ever! **$59.95**

Video Modulator Kit $8.95

Convert your TV set into a high quality monitor without affecting normal usage. Complete kit with full instructions.

2.5 MHz Frequency Counter Kit

Complete kit less case **$37.50**

30 MHz Frequency Counter Kit

Complete kit less case **$47.75**
Prescaler kit to 350 MHz **$19.95**

1978 IC Update Master Manual

1978 IC Update Master Manual **$19.50.** Complete IC data selector, 2175 pg. Master reference guide. Over 42,000 cross references. Free update service through 1978. Domestic postage **$3.50.** Foreign **$5.00.** 1979 IC Update available late Jan. **$30.00.**

Stopwatch Kit $26.95

Full six digit battery operated. 2–.5 volts. 3.2768 MHz crystal accuracy. Times to 59 min., 59 sec., 99 1/100 sec. Times std., split and Taylor. 7205 chip, all components minus case. Full instructions.

D Connectors RS232

25 Pin Subminiatures

DB25P	2.95	DE9P	1.50
DB25S	3.95	DE9S	1.95
Cover	1.50	DA15P	2.10
RS232 Complete Set	6.50	DA15S	3.10

S-100 Computer Boards

8K Static RAM Kit	$127.00
16K Static RAM Kit	265.00
24K Static RAM Kit	423.00
32K Dynamic RAM Kit	449.00
64K Dynamic RAM Kit	945.00
8K/16K Eprom Kit (less PROMS)	**$89.00**
Video Interface Kit	**$139.00**
Motherboard **$39.**	Extender Board **$8.99**

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H31

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(714) 560-4900
Highway 163 & Clairemont Mesa Blvd.

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999 Howard Avenue
(415) 342-5757
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HAM RADIO OUTLET™

OVER THE COUNTER (Mon. thru Sat. 10 AM to 5:30 PM)
MAIL ORDER, Phone, Write.

Reader Service—see page 211

SAVE $25.00

Model 8100 Frequency Counter Kit

- Range: 20Hz to 100MHz
- High Sensitivity
- Resolution to 0.1Hz

Now you can forget about price/performance trade-offs when you select a frequency counter. In Sabtronics' Model 8100 kit you get all the characteristics of superior performance at a low, affordable price.

This frequency counter, employing LSI technology, has the performance and input characteristics you demand: guaranteed frequency range of 20Hz to 100MHz (10 Hz to 120MHz typical); selectable hi/lo impedance; superior sensitivity; selectable resolution and selectable attenuation. Plus an accurate time base with excellent stability.

An 8-digit LED display features gate activity indicator, leading zero suppression and overflow indicator. You would expect to find all these features only on high-priced instruments — or from Sabtronics' advanced digital technology.

BRIEF SPECIFICATONS:
• Frequency Range: 20Hz to 100MHz guaranteed. (10Hz to 120MHz typical) • Sensitivity: 15mV RMS, 20Hz to 50MHz (10mV typical); 25mV RMS, 50MHz to 100MHz (20mV typical) • Selectable Impedance: 1MΩ /25pF or 50Ω • Attenuation: X1, X10 or X100 • Accuracy: ±1Hz plus time base accuracy • Aging Rate: ±5ppm/yr. • Temperature Stability: ±10ppm, 0°C to 40°C • Resolution: 0.1Hz, 1Hz, 10Hz selectable • Display: 8-digit LED, overflow indicator, gate activity indicator • Overload Protection • Power Requirement: 9–15 VDC @ 330mA

Model 2000, 3½ Digit DMM Kit

- 5 Functions, 28 Ranges
- Basic DCV Accuracy: 0.1% ±1 Digit

The amazing Sabtronics 2000 is the choice of both professionals and hobbyists. It's the only portable/bench DMM that offers so much performance for such an astonishing low price.

You get basic DCV accuracy of 0.1% ±1 digit; 5 functions giving 28 ranges; readings to ±1999 with 100% overrange; overrange indication; input overload protection; automatic polarity; and automatic zeroing.

The all-solid-state Model 2000 incorporates a single LSI circuit and high-quality components. Our clear, step-by-step manual simplifies assembly. Complete kit includes a rugged high-impact case ideal for both test-bench and field use.

BRIEF SPECIFICATIONS:
• DC volts in 5 ranges: 100 μV to 1kV • AC volts in 5 ranges: 100 μV to 1kV • DC current in 6 ranges: 100 nA to 2A • AC current in 6 ranges: 100 nA to 2A • Resistance: 0.1Ω to 20MΩ in 6 ranges • AC frequency response: 40 Hz to 50kHz • Display: 0.36" (9.1mm) 7-segment LED • Input Impedance: 10MΩ • Size: 8"W × 6.5"D × 3"H (203 × 165 × 76 mm) • Power requirement: 4.5-6.5 VDC-4 "C" cells (not included).

SPECIAL OFFER EXPIRES FEB. 15, 1979

Special Offer! Save $25.00*

If you order both the frequency counter and DMM kits now, you pay only $144.90 including shipping and handling. *You save $25.00* off the combined regular low price of $169.90. Order both kits now. This special offer good for a limited time only.

*Special offer good in USA only.

Making performance affordable.

S27

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Sabtronics International Inc. 13426 Floyd Circle Dallas Tx 75243 **"73-2"**

☐ **Yes, I want to take advantage of your special $25.00-off offer.***

Please send _____ Model 8100 *and* Model 2000 kit(s) for only $144.90 total including shipping and handling . . . . . $_____

Please send _____ Model 8100 Frequency Counter kit(s) @ $89.95 ea. $_____
Shipping and handling $ 5.00/unit* $_____

Please send _____ Model 2000 DMM kit(s) @ $69.95 ea. $_____
Shipping and handling $ 5.00/unit* $_____

Texas residents add sales tax . . . . . $_____
Total enclosed . . . . . $_____

☐ Check ☐ Money Order ☐ Charge my Master Charge_____ Visa_____
Acc. No. _____ Exp. Dt._____

Name _____

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City_____ State_____ Zip_____

*USA only. CANADA: $6.50. FOREIGN: $19.00 AIRMAIL.

NEW! NEW! NEW!

KDK

FM2016A

All Solid State-CMOS PL digital synthesized - No Crystals to Buy! 5KHz steps - 144-149 MHz-HUGE ⅜" LED digital readout PLUS MARS-CAP and MULTIPLE OFFSET BUILT IN. ● 5 MHz Band Coverage - 1000 Channels (instead of the usual 2 MHz to 4 MHz-400 to 800 Channels) ● 4 CHANNEL RAM IC MEMORY WITH SCANNING AND AUTO TRANSMIT ● MULTIPLE FREQUENCY OFFSETS ● ELECTRONIC AUTO TUNING - TRANSMIT AND RECEIVE ● INTERNAL MULTIPURPOSE TONE OSCILLATOR ● RIT ● RF ATT ● DISCRIMINATOR METER - 16 Watts Output-Unequaled Receiver Sensitivity and Selectivity - 15 POLE FILER, MONOLITHIC CRYSTAL FILTER AND AUTOMATIC TUNED RECEIVER FRONT END, COMPARE! ● Superb Engineering and Superior Commercial Avionics Grade Quality and Construction Second to None at ANY PRICE.

INTRODUCTORY PRICE

$359.00

Regulated AC/PS
Model FMPS-4R . . . $39.95

SHOWN WITH OPTIONAL μP-800 MICRO-PROGRAMMER*

FMMC-1* Microphone with Built-in Touch Tone Pad.

WHY BUY LESS? THE FMMC-1 HAS IT *ALL!*

- New! Auto key up
- Snap-Action Keyboard
- Adj. level and tone balance
- Use with any transceiver
- Only 3¼" x 2" **$39.95**

- **FREQUENCY RANGE**: Receive and Transmit: 144.00 to 148.995 MHz, 5 Khz steps (1000 channels) + MARS-CAP and MULTIPLE OFFSET BUILT IN.
- **HUGE ⅜" LED DIGITAL READOUT.**
- **4 CHANNEL RAM SCANNER WITH IC MEMORY AND AUTO TRANSMIT**: Program any 4 frequencies and reprogram at any time using the front panel controls—search for occupied (closed) channel or vacant (open) channels. Internal Ni-Cad included to retain memory (no diode matrix to wire or change).
- **MULTIPLE FREQUENCY OFFSETS: NO CRYSTALS TO BUY - EVER** - Any offset any split! "Odd Ball" splits accomplished by digital programming. Never any need for crystals!
- **INTERNAL MULTIPURPOSE TONE OSCILLATOR BUILT IN**: Sine Wave 1750 Hz tone burst for "whistle on operation" and sub-audible tone operation. Internal 2 position switch for automatic and manual operation, tone burst or sub audible tone PL - adjustable 60-203 Hz (100 Hz Pre-Set).
- **AIRCRAFT TYPE FREQUENCY SELECTOR**: Large and small coaxially mounted knobs select 100KHz and 10KHz steps respectively. Switches click-stopped with a home position facilitate frequency changing without need to view LED's while driving and provides the sightless amateur with full Frequency Selection as standard equipment.
- **FULL AUTOMATIC TUNING OF RECEIVER FRONT END AND TRANSMITTER CIRCUITS**: DC output of PLL fed to varactor diodes in all front end RF tuned circuits provides full sensitivity and optimum intermodulation rejection over the entire band. APC (AUTO POWER CONTROL) - Keeps RF output constant from band edge to band edge. NO OTHER AMATEUR UNIT AT ANY PRICE has these features which are found in only the most sophisticated and expensive aircraft and commercial transceivers.
- **TRUE FM**: Not phase modulation - for superb emphasized hi-fi audio quality second to none.
- **RIT CONTROL**: Used to improve clarity when contacting stations with off frequency carrier.
- **MONITOR LAMPS**: 2 LED's on front panel indicate (1) incoming signal-channel busy, and (2) Transmit.
- **FULLY REGULATED INTEGRAL POWER SUPPLY**: Operating voltage for all 9v circuits independently regulated. Massive Commercial Hash Filter.
- **MODULAR COMMERCIAL GRADE CONSTRUCTION**: 3 Unitized modules eliminate stray coupling and facilitate ease of maintenance.
- **ACCESSORY SOCKET**: Fully wired for touch tone, phone patch, and other accessories. Internal switch connects receiver output to internal speaker when connector is not in use.
- **MULTI-PURPOSE METER**: Triple Function Meter Provides Discriminator Meter, "S" Reading on receive and Power Out on Transmit.
- **RECEIVE**: Better than .25uv sensitivity, 15 POLE FILTER as well as monolithic crystal filter and AUTOMATIC TUNED LC circuits provide superior skirt selectivity - COMPARE!
- **HIGH/LOW POWER OUTPUT**: 16 watts and 1 watt, switch selected. Low power may be adjusted anywhere between 1 and 16 watts. Fully protected - short or open SWR.
- **RF ATT**: Live right next to King Kong Repeater and can't operate? With the 2016A You Can - Just flick the RF ATT switch. Only the 2016A has this feature.
- **OTHER FEATURES**: Dynamic Microphone, built in speaker, mobile mounting bracket, external 5 pin accessory jack, speaker jack, and much, much more. Size 2½ x 7 x 7½. All cords, plugs, fuses, microphone hanger, etc. included. Weight 5 lbs.

Manufactured by one of the world's most distinguished Avionics manufacturers, Kyokuto Denshi Keisha, Ltd.
First in the world with an all solid state 2 meter FM transceiver.

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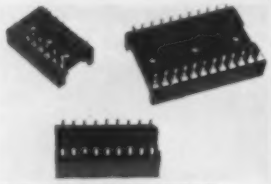
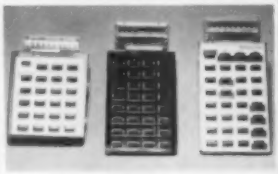
GALLIUM PHOSPHIDE L.E.D.
Provides Higher Intensity Than Regular LED's; T1-3/4 Dome (Red Diffused) AND Part #114R 1-99 . . 22¢ 100 + . . . 20¢
We stock the full line of AND L.E.D.'s



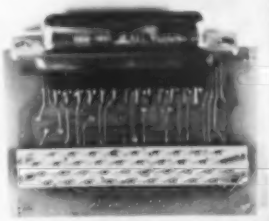
DIP SOCKET SPECIALS

	1-49	50 +
16 Pin Low Profile Solder Tab	20¢	15¢
18 Pin Standard Heighth Solder Tab	25¢	20¢
24 Pin Low Profile Solder Tab GOLD	60¢	55¢



CALCULATOR GUTS Experimenter's delight. Each keyboad includes a monolithic calculator chip and a display. These are rejects. It might be something simple to repair or it could be very nasty. At this price, who cares! 9 volt. **$1.50 ea. 3/$3.00.**

HOBBY BAGS An assortment of misc. electronic parts. A genuine value and savings. **Only $2.99.**



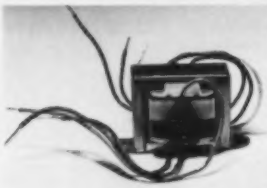
DB-25 FEMALE CONNECTOR
A unique assembly originally adapting the RS232 Type Connector to flat cable. **$1.50 each or 2/$2.50.**

INSTRUMENT/CLOCK CASE KIT Perfect for your opto projects. Solid aluminum construction with real walnut sides. O.D. 5-3/8" by 5-3/8" by 2". $6.95 ea.

EDGE CARD CONNECTOR
Cinch Jones 10/20 Pins .156 Spacing PC Mount **85¢**. Burndy 22/44 Pins, .156 spacing PC Mount, **$1.40 each.**

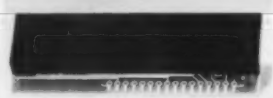
LINE PRINTER HAMMER DRIVER BOARD Each board contains approx. 130 each #MJE800 (Silicon Darlington NPN hfe 750, 1.5A). About $130.00 worth, over 100 1N4001 diodes, plus support chips. The whole package is yours for only **$14.95.**
HURRY, WE DON'T EXPECT THESE TO LAST VERY LONG!

EUROPEAN 220V LINE CORD
Building something for export? Then you might need this. **40¢ ea. 10/$3.00.**

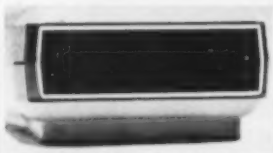


TRANSFORMER Pri. 110 VAC Sec. 11.2 and 5 VCT @ 1 amp. **95¢ ea.**

TRANSFORMER P-C mount. pri. 110 VAC Sec. 12.6 @ 1 amp. **$1.25 ea.**



CLOCK DISPLAY National Semi. 6 Digit Multiplexed Display; .33" Characters (Common Cathode).
A REAL BUY AT JUST $1.00.



INSTRUMENT CLOCK CASE KIT A real jewel for those smaller projects. Hinged top door allows you to hide your control area. O.D. 4½" x 4" x 1¾" **$1.99 each.**

SMITH 5-WAY BINDING POSTS. 69c each

FAIRCHILD #78H05 Pos. 5V 5 Amp Regulator (TO-3) NET $11.00; Your Cost $1.95 or 2/$3.00

FLAT CABLE CONNECTOR
Female 34 Pin Socket **50¢ each**

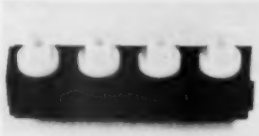
PLASTIC PARTS BOX A nice little hinged-top box for storing all your small parts. O.d. 6¼" by 3¼" by 2". **75¢ ea. 10/$5.00.**

COMPUTER POWER SUPPLY TRANSFORMER PRI. 110/220 Vac; **SEC.** 12.1 V @ 9 A, 44.0 V @ 2.5 A, 12.9 V @ 2.0 A, 12.9 V @ s 3.2 A. **Only $14.95 ea.**

EDGE METER 100-0-100 ua 1/2" by 11/16". Compare with other meters costing $6.00. **ONLY $2.00 ea.** Why pay more?

CALCULATOR BUBBLE DISPLAY BRAND NEW pocket calculator displays. Ranging from 6-9 digit. Your luck **$1.25 ea. 3/$3.00**

KEYBOARD HOBBY BAG Compare, then really save with our calculator hobby bag assortment. Each one contains 3 calculator keyboards. All this for **only $1.75.**

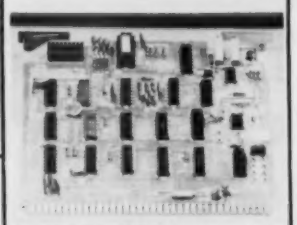


KEYBOARD SWITCH ASSEMBLIES Spring contact type **6/$2.00** (Which enables you to re-assemble 3 complete groups of 4 switches.)

REPEAT OF A SELL-OUT A complete 12 hour digital clock. Some are manufacture line rejects, some are returns, and some are just scratched. Features: hours- minutes- alarm- snooze alarm. Parts value alone would equal $20.00, you pay **only $6.00 ea.**

DEFECTIVE CALCULATORS
Well, some are and some are not. We can't afford the time to test them. **$2.50 ea.** Batteries not included. **2/$4.00**

#30 KYNAR Blk., Brn., Red., Or., Yel., Grn., Blu., Vio., Gry., Wh.
We will do our best to ship the color you specify. To ensure prompt delivery of your order we will substitute colors should we be temp. out, unless you specify otherwise. **$2.36 per hundred foot spool; $14.16 per thousand foot spool; Multiples of 100' only.**
Call us for quotes on larger quantities.



PARTS BOARDS A great way to buy parts on a budget. We guarantee your money's worth. **ONLY $1.00 ea.**

CAPACITORS

Capacitance	Voltage	Style	Price
1000uf	25 VDC	P-C	25¢
220uf	25 VDC	P-C	25¢
2000uf	25 VDC	AXIAL	50¢
40/40	150 VDC	AXIAL	45¢
1uf	15 VDC	AXIAL	19¢
.018	100 V	MYLAR	25¢
.001	100 V	MICA	11¢
.01		DISC	7¢
.02		DISC	6¢
.1		DISC	9¢

CLAIREX PHOTO CELLS These have a real USEFUL range to them. Any project involving control from ambient light levels will utilize this photo cell. Light resistance 1K. Fast response. .156 Diameter. **75¢ each or 2/$1.00.**

ROTRON WHISPER FAN #WR2H1 3 Blade 4" Diameter 75CFM 115VAC. NET $17.00 **YOUR PRICE $9.95**
Wait now, these are not pull-outs or something like that, these are new!

10 STATION PUSH BUTTON SWITCH ASSEMBLY 4 Push-On/Push-Off, 6 Ganged Push-On/Push-Off DPDT **$2.50 Each.**

SELECTED VALUES
These items are chosen from our vast inventory of industrial quality components:

Extruded heat sink 10 7/8" by 2 1/4" by 5/8"	$1.40
500 Ohm P-C mount trimmer	20¢
Line cord #18 ga 6'	25¢
74LS175 Quad D flip-flop	50¢
S.P.D.T. sub-min slide switch	40¢
S.P.S.T. P-C SWITCH	20¢
ACID BRUSH	10¢
SMITH #8523 SPACER .5 by #8 hole	5¢
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14 PIN DIP HEADER	35¢

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MK-05 MINI MOBILE CLOCK

The smallest and best priced mobile clock kit on the market. Designed to be a mobile clock from the ground up. There has been no compromise on quality.

FEATURES:

- Quartz crystal timebase
- Toroid & zener noise & overvoltage protection
- Magnified 15" 6 digit LED readout
- Complete with presettable 24 hr. alarm
- 9-14 VDC @ 40 to 50 ma.
- Readouts can be suppressed
- EASY, QUICK ASSEMBLY
- All components required included (you supply the speaker)
- Top quality drilled and plated PC boards. Clock board: 2.6" x 2". Readout board: 2 3/8" x .75"

12.95

UNIVERSAL SOUND EFFECTS BOARD

New!

HAVE YOU EVER WISHED YOU COULD DUPLICATE THE SOUND OF A STEAM TRAIN OR A PHASOR GUN? HOW ABOUT GUNSHOTS, WHISTLES, SIRENS, BARKING DOGS AND OTHER SOUND EFFECTS? NOW YOU CAN WITH OUR PROGRAMMABLE SOUND EFFECTS KIT. IT USES THE NEW 28 PIN T.I. SOUND SYNTHESYZER CHIP, SN76477 AND SUPPORT CIRCUITRY. 5 TO 12VDC IS REQUIRED TO GIVE APPROX. 1/4 WATT OF AUDIO OUTPUT. WE PROVIDE THE P.C. BOARD, PARTS AND INSTRUCTIONS ALONG WITH A CHART TO PROGRAM SOME COMMON SOUNDS. USE YOUR IMAGINATION TO CREATE ORIGINAL SOUND EFFECTS. ORDER: SE-01 **16.95**(Less Spkr.)

YOU'VE SEEN IT ON QUALITY STEREO GEAR

SUPER DEAL!

BLACK INSERT

BRUSHED CHROME

7/8" hole to hole

DPDT Toggle ALCO CST-202 3A @ 125V

.49

MC1468R POSITIVE VOLTAGE REGULATOR

1 AMP. COMPLETE SPECS AND APPLICATIONS SHOW HOW TO BUILD FIXED OR VARIABLE POWER SUPPLIES FROM 3 TO 30VDC (DRIVE EXTERNAL SERIES PASS FOR CURRENT TO 20 AMPS)

1.25 EA. 10/10.00

HOUSE #

25A 100V SCR 1.95

Perfect for battery chargers, switching supplies, crowbars, etc.

739 FAIRCHILD

DUAL LOW NOISE AUDIO PRE-AMPLIFIER

89¢ 2/1.69

HOUSE # PNP POWER

TO-3

100 WATTS 60 VOLTS 10 AMPS

IDENTICAL TO 2N3792 1.00

MPF131 N-CHANNEL DUAL GATE MOSFET

50¢

DESIGNED FOR AMPLIFIER AND MIXER APPLICATIONS TO 200 MHZ. PLASTIC CASE UNITS ARE HOUSE NUMBERED WITH SPECS.

MJ900 - MJ1000

COMPLIMENTARY PNP/NPN DARLINGTON POWER TRANSISTORS. 8 AMPS. WE SUPPLY A SCHEMATIC TO BUILD A HIGH POWER (250W) LOW DISTORTION AUDIO AMP WITH ONLY ONE ADDITIONAL TRANSISTOR AND A DOZEN INEXPENSIVE COMPONENTS! TO-3 CASE STYLE. BUY A PAIR FOR

$3.00!

FANTASTIC SOUND EFFECTS CHIP

THIS 28 PIN MARVEL CONTAINS A LOW FREQUENCY OSCILLATOR, VCO, NOISE OSCILLATOR, ONE SHOT, MIXER AND ENVELOPE CONTROL, WITH 6 PAGE MANUAL. 5 to 9VDC

3.95

EMITTER RESISTORS

HARD TO FIND VALUES!

.1 ohm @ 5W

.25 ohm @ 5W

YOUR CHOICE... 7/1.00

LM3900 QUAD NORTON AMP

HOUSE #

WE BOUGHT A LARGE QUANTITY OF THESE HOUSE NUMBERED PARTS AT A BARGAIN PRICE THAT ALLOWS US TO SELL THEM AT A LOW LOW 39¢

IL-1 OPTO ISOLATORS

BY LITRONIX 6 PIN DIP. STANDARD PINOUT. LED/TRANSISTOR COMBINATION

50¢

WHILE THEY LAST!

WIREWRAP Wire

30 Gauge KYNAR® Insulat.

500 FT

4.50

6 DIGIT ZULU CLOCK KIT

At last a clock for HAMS. Designed with large bright LED digits to enhance your shack. The unit is a pleasure to assemble and so easy on the budget! You get top quality parts and plated PC Boards. The unique design of the board set eliminates the headaches of running wires between clock and readout board. As a bonus the unit has a switchable timer that can be reset to zero without disturbing real time. Elapsed time in minutes and seconds up to 25 minutes. Six full sized FND510 readouts and colons making viewing easy from across the room. Does NOT use the old style 5314 chip. **DUE TO A SPECIAL PURCHASE WE HAVE A LIMITED QUANTITY.**

We Promised!

COMPLETE ZULU CLOCK KIT

Includes: All components, plated, drilled PC Boards, large easy to read instructions, and AC transformer. Clock board: 2¼" X 4¼". Readout Board: 1½" X 4¼"

19.00

24 Hr. Format Only

Hand made solid hardwood case for the Zulu Clock. Includes ruby front filter and back panel.

6.95

ALL COMPONENTS 100% GUARANTEED

C4301 WIDEBAND IF AMP w/specs	50¢
2N3569 NPN EPOXY 1W	6/1.00
741 OP AMP 8 PIN DIP	5/1.00
723 VOLTAGE REG 14 PIN DIP	50¢
MPS8530 NPN HOUSE #	8/1.00
725 OP AMP LOW NOISE HOUSE #	99¢
7815 15V 1A REGULATOR HOUSE #	89¢
2N4393 P CHANNEL J FET	4/1.00
2N5111 PNP MED PWR 40W TO-220	3/1.00
2N6027 PROGRAMMABLE UNIJUNCTION w/specs	50¢
TRIAC 200V 8A UNMARKED	3/1.00

Diodes

1N4003	200V 1A	15/1.00
1N4006	600V 1A	13/1.00
1N270	Germanium Diode	8/1.00
1N38A	Germanium Diode	10/100
1N4148	Cut & Bent for PC Board Insertion	100/1.25

UNMARKED POWER DIODES with cathode bands. Guaranteed to be at least 400PIV @ 1A. 100% Good parts. Epoxy case.

25/1.00

POWER SUPPLY KIT PS-14

- Better than 200MV load and line regulation
- Foldback Current Limiting
- Short Circuit Protected
- Thermal Shutdown
- Adjustable Current Limiting
- Less than 1% ripple
- 15 amps 11.5 to 14.8V
- All parts supplied including heavy duty trans-former
- Quality plated fiberglass PC board.

Less Case, meters & jacks

UPS SHIPPING PAID!

REVIEWED IN 7/78 73 MAG.

15A CONT. 20A INT. 42.95

NEW ITEMS:

MV1624 Varicap Diode 10pfd Nom. 2:1 Tuning Range 49¢

2N5583 High Freq. Amp 1 Watt @ 1.5 GHZT TO-5 Case style, House # 19¢

MPC4000B ½ Watt Audio Amp 4 pin plastic pack 59¢

H610100 100V 2A SCR Ultra sensitive gate drives from TTL. TO-220 **65¢**

H6235S 50V 3A Triac Sensitive Gate TO-5 40¢

"WARBLE ALARM KIT

A fun EASY kit to assemble that emits an ear splitting 10 watt dual tone scream. Resembles European siren sound. Great for alarms or toys. Operates from 5-12VDC at up to 1 amp (using 12VDC-8 ohm speaker). Over five thousand have been sold. All parts including PC board, less speaker.

2.50 ORDER WB-02

FND510 60¢

COMMON ANODE READOUT 7 CHARACTER

LIMIT 20 PER CUSTOMER!

LED'S

JUMBO	RED	5/.89
	GREEN	4/.89
MEDIUM	RED	.15 ea
	GREEN	.18
	YELLOW	.18

1.5V 10-30 ma

MC1351P FM-IF AMP AND DISCRIMINATOR

USED IN FM & TV SOUND CIRCUITS. REQUIRES MINIMUM EXTERNAL COMPONENTS. 14 PIN DIP. DIRECT REPLACEMENT FOR HEPC 5002, ECG 769 and SK6007. COVERS: HOUSE # WITH SPECS 39¢

MC3301P HOUSE

4 OP AMPS IN ONE PACKAGE USES SINGLE SUPPLY. 1.4 to 28VDC. INTERNALLY COMPENSATED. SIMILAR TO MC3401 BUT HIGHER GAIN 49¢

OVERVOLTAGE PROTECTION KIT 6.95

Provides cheap insurance for your expensive equipment. Trip voltage is adjustable from 3 to 30 volts. Overvoltage instantly fires a 25A SCR and shorts the output to protect equipment. Should be used on units that are fused. Directly compatible with the PS-12 and PS-14. All electronics supplied. Drilled and plated PC board. (Order OVP-1)

CAPACITORS

SMALL SIZE!

.022	@ 100VDC Mylar	8/1.00
.22	@ 50VDC Mylar	6/1.00
1.5mfd	@ 400VDC Mylar	4/1.00
1mfd	@ 35V Tant Axial	6/1.00
47mfd	@ 35V Tant Axial	6/1.00
2.2mfd	@ 35V Tant Axial	5/1.00
22mfd	@ 35V Dip Tant	4/1.00
33mfd	@ 10V Dip Tant	4/1.00

NEVER A SWEETER METER!

Beautiful **American made** panel meters are a snap to install. Huge 3½" wide dials are easy to read. You would expect to pay more for each than we get for the pair! MATCHED SET 0-15VDC, 0-30ADC

12.95 Set

MK-03A CLOCK/TIMER KIT

Features 24 hour Zulu time and up to 24 hours of elapsed time on the same set of six digit LED readouts. Totally independent operation of both functions. Clock has presettable alarm with 10 minute snooze. Timer has reset, hold, and count functions. Full noise and overvoltage protection. 24 hour only. Readouts has dimmer feature or they can be turned off without disturbing the clock or timer. Timebase included (.01% accuracy). Because of the many options and mounting considerations the case and switches are not included. Switches are standard types. Will fit inside standard aircraft instrument case.

9-14VDC 28.95

MOBILE CLOCK CALENDAR KIT

Seems like **everybody** sells digital clock kits, however we have the only low cost **DIGITAL CLOCK / CALENDAR** for Mobile operation. We provide quality plated through hole boards and step by step instructions, parts overlays and schematics. This clock has many features and we supply all the parts but a small speaker. Fantastic for car, boat or Van.

- Enclarged Timebase (.01% ACC)
- Large 4 DIGIT LED display with AM/PM indicators
- Flashing colon on 1Hz rate
- Special noise and overvoltage protection for mobile use
- Auxiliary output will drive relay or TRIAC to control external equipment
- 45% Duty Cycle
- Built in ignition transient burns off readouts when not in use
- Presettable alarm with Snooze
- Special "Sleep Timer"

23.50 NO CASE

12 VAC XFMR for 110 VAC 1.50

24 Hour Format add 2.00

ZENER GRAB BAG

A very nice assortment of ¼, ½ & 1W zeners. Voltage ranges are from **2.7** to **30 VDC.** Most have house # but we provide a cross over list to standard numbers. A great buy for any shop. **12 different types.**

69¢

- NO COD'S
- SEND CHECK OR MONEY ORDER OR CHARGE CARD NO.
- ADD 5% FOR SHIPPING
- TEX RESIDENTS ADD 5% TAX
- FOREIGN ORDERS ADD 10%,
- ORDERS UNDER $10. ADD .75 for HANDLING

PHONE ORDERS ACCEPTED ON VISA & MC

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B8

FREQUENCY COUNTER KIT

Outstanding Performance

Incredible Price $89.95

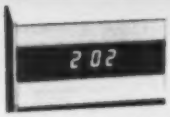
CT-50

The CT-50 is a versatile and precision frequency counter which will measure frequencies to 50 mHz and up to 600 mHz with the CT-600 option. Large Scale Integration, CMOS circuitry and solid state display technology have enabled this counter to match performance found in units selling for over three times as much. Low power consumption (typically 300-400 ma) makes the CT-50 ideal for portable battery operation. Features of the CT-50 include: large 8 digit LED display, RF shielded all metal case, easy pushbutton operation, automatic decimal point, fully socketed IC chips and input protection to 50 volts to insure against accidental burnout or overload. And, the best feature of all is the easy assembly. Clear, step by step instructions guide you to a finished unit you can rely on. **Order your today!**

SPECIFICATIONS:
Frequency range: 5 Hz to 65 mHz, 600 mHz with CT-600
Resolution: 10 Hz @ 0.1 sec gate, 1 Hz @ 1 sec gate
Readout: 8 digit, 0.4" high LED, direct readout in mHz
Accuracy: adjustable to 0.5 ppm
Stability: 2.0 ppm over 10° to 40° C. temperature compensated
Input: BNC, 1 megohm, 20 pf direct, 50 ohm with CT-600
Overload: 50VAC maximum, all modes
Sensitivity: less than 25 mv rms 5 to 65 mHz, 50-150 mv rms to 600 mHz
Power: 110 VAC, 5 Watts or 12 VDC @ 400 ma
Size: 6" x 4" x 2", high quality aluminum case, 2 lbs
IC'S: 13 units, all socketed

CT-50, 50 MHz counter kit	$89.95
CT-50WT, 50 mHz counter, wired and tested	159.95
CT-600, 600 mHz scaler, option, add	29.95
LB-1, Color TV calibration stabilizer	$14.95
DP-1, DC probe, general purpose probe	12.95
HP-1, high impedance probe, non-loader	15.95

CAR CLOCK



The UN-KIT, only 5 solder connections

Here's a super looking, rugged and accurate auto clock which is a snap to build and install. Clock movement is completely assembled—you only solder 3 wires and 2 switches, takes about 15 minutes! Display is bright green with automatic brightness control photocell—assures you of a highly readable display, day or night. Comes in a satin finish anodized aluminum case which can be attached 5 different ways using 2 sided tape. Choice of silver, black or gold case (specify).

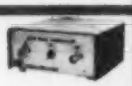
DC-3 kit, 12 hour format	$22.95
DC-3 wired and tested	$29.95
110V AC adapter	$5.95

Under dash car clock

12/24 hour clock in a beautiful plastic case features: 6 jumbo RED LEDS, high accuracy (1 min/mo.), easy 3 wire hookup, display blanks with ignition, and super instructions. Optional dimmer automatically adjusts display to ambient light level.

DC-11 clock with mtg. bracket	$27.95
DM-1 dimmer adapter	2.50

PRESCALER



Extend the range of your counter to 600 mHz. Works with any counter. Includes 2 transistor pre-amp to give super sens, typically 20 mv at 150 mHz. Specify ÷ 10 or ÷ 100 ratio.

PS-1B, 600 mHz prescaler	$59.95
PS-1BK, 600 mHz prescaler kit	49.95

OP-AMP SPECIAL

741 mini dip	12/$2.00
B1-FET mini dip, 741 type	10/$2.00

VIDEO TERMINAL

A completely self-contained, stand alone video terminal card. Requires only an ASCII keyboard and TV set to become a complete terminal unit. Two units available, common features are: single 5V supply, XTAL controlled sync and baud rates (to 9600), complete computer and keyboard control of cursor. Parity error control and display. Accepts and generates serial ASCII plus parallel keyboard input. The 3216 is 32 char. by 16 lines, 2 pages with memory dump feature. The 6416 is 64 char. by 16 lines, with scrolling, upper and lower case (optional) and has RS-232 and 20ma loop interfaces on board. Kits include sockets and complete documentation.

RE 3216, terminal card	$149.95
RE 6416, terminal card	189.95
Lower Case option, 6416 only	13.95
Power Supply Kit	14.95
Video/RF Modulator, VD-1	6.95
Assembled, tested units, add	60.00

CALENDAR ALARM CLOCK

The clock that's got it all: 6- 5" LEDs, 12/24 hour, snooze, 24 hour alarm, 4 year calendar, battery backup, and lots more. The super 7001 chip is used. Size: 5x4x2 inches.
Complete kit, less case (not available)
DC-9 $34.95

30 Watt 2 mtr PWR AMP

Simple Class C power amp features 8 times power gain. 1 W in for 8 out, 2 in for 15 out, 4 W in for 30 out. Max. output of 35 W, incredible value, complete with all parts, less case and T-R relay.

PA-1, 30 W pwr amp kit	$22.95
TR-1, RF sensed T-R relay kit	6.95

FM MINI MIKE KIT

A super high performance FM wireless mike kit! Transmits a stable signal up to 300 yards with exceptional audio quality by means of its built in electret mike. Kit includes case, mike, on-off switch, antenna, battery and super instructions. This is the finest unit available.

FM-3 kit	$12.95
FM-3 wired and tested	16.95

CLOCK KITS

our Best Seller your Best Deal

Try your hand at building the finest looking clock on the market. Its satin finish anodized aluminum case looks great anywhere, while six .4" LED digits provide a highly readable display. This is a complete kit, no extras needed, and it only takes 1-2 hours to assemble. Your choice of case colors: silver, gold, bronze, black, blue (specify).

Clock kit, 12/24 hour, DC-5	$22.95
Clock with 10 min. ID timer, 12/24 hour, DC-10	27.95
Alarm clock, 12 hour only, DC-8	24.95
12V DC car clock, DC-7	27.95

For wired and tested clocks add $10.00 to kit price.

Hard to find PARTS

LINEAR ICs	
301	$ .35
324	1.50
380	1.25
380-8	.75
555	.45
556	.85
566	1.15
567	1.25
1458	.50
3900	.50
CMOS ICs	
4011	.20
4013	.35
4046	1.85
4049	.40
4518	1.25
5369	1.75
TRANSISTORS	
2N3904 type	10/1.00
2N3906 type	10/1.00
NPN 30W Pwr	3/1.00
PNP 30W Pwr	3/1.00
2N3055	.60
UJT 2N2646 type	3/2.00
FET MPF102 type	3/2.00
UHF 2N5179 type	3/2.00
MRF-238 RF	11.95
SOCKETS	
8 pin	10/2.00
14 pin	10/2.00
16 pin	10/2.00
24 pin	4/2.00
28 pin	4/2.00
40 pin	3/2.00

REGULATORS	
78MG	$1.25
723	.50
309K	.85
7805	.85
78L05	.25
7905	1.25
7812	.85
7912	1.25
7815	.85
TTL ICs	
7400	.35
7447	.65
7475	.50
7490	.50
74196/7	1.35
SPECIAL ICs	
11C90	13.50
10116	1.25
4511	2.00
5314	2.95
5375AB	2.95
7001	6.50
4059 ÷ N	9.00
7208	17.95
LEDs	
Jumbo red	8/1.00
Jumbo green	6/1.00
Jumbo yellow	6/1.00
Mini red	8/1.00
Micro red	8/1.00
Bi-Polar	.75
FERRITE BEADS	
With mtg. specs	15/1.00
6 hole balun	5/1.00

Ramsey's famous MINI-KITS

FM WIRELESS MIKE KIT

Transmits up to 300' to any FM broadcast radio, uses any type of mike. Runs on 3 to 9V. Type FM-2 has added sensitive mike preamp stage.
FM-1 kit $2.95 FM-2 kit $4.95

COLOR ORGAN/MUSIC LIGHTS

See music come alive! 3 different lights flicker with music. One light for lows, one for the mid-range and one for the highs. Each channel individually adjustable, and drives up to 300W. Great for parties, band music, nite clubs and more.
Complete kit, ML-1 $7.95

LED BLINKY KIT

A great attention getter which alternately flashes 2 jumbo LEDs. Use for name badges, buttons, warning panel lights, anything! Runs on 3 to 15 volts.
Complete kit, BL-1 $2.95

VIDEO MODULATOR KIT

Converts any TV to video monitor. Super stable, tunable over ch. 4-6. Runs on 5-15V, accepts std. video signal. Best unit on the market!
Complete kit, VD-1 $6.95

TONE DECODER

A complete tone decoder on a single PC board. Features 400-5000 Hz adjustable range via 20 turn pot, voltage regulation, 567 IC. Useful for touch-tone decoding, tone burst detection, FSK, etc. Can also be used as a stable tone encoder. Runs on 5 to 12 volts.
Complete kit, TD-1 $5.95

WHISPER LIGHT KIT

An interesting kit, small mike picks up sounds and converts them to light. The louder the sound, the brighter the light. Completely self-contained, includes mike, runs on 110VAC, controls up to 300 watts.
Complete kit, WL-1 $6.95

SUPER SLEUTH

A super sensitive amplifier which will pick up a pin drop at 15 feet! Great for monitoring baby's room or as general purpose amplifier. Full 2 W rms output, runs on 6 to 15 volts, uses 8-45 ohm speaker.
Complete kit, BN-9 $5.95

POWER SUPPLY KIT

Complete triple regulated power supply provides variable + 6 to 18 volts at 200 ma and + 5V at 1 Amp. Excellent load regulation, good filtering and small size. Less transformers, requires 6.3V @ 1 A and 24 VCT.
Complete kit, PS-3LT $6.95

SIREN KIT

Produces upward and downward wail characteristic of a police siren. 5 W peak audio output, runs on 3-15 volts, uses 3-45 ohm speaker.
Complete kit, SM-3 $2.95

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TERMS: Satisfaction guaranteed or money refunded. COD, add $1.50. Minimum order $6.00. Orders under $10.00, add $.75. Add 5% for postage, insurance, handling. Overseas, add 15%. NY residents, add 7% tax.

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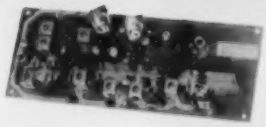
hamtronics, inc.

H16 OSCAR HEADQUARTERS

★ Quality VHF & UHF Kits At Affordable Prices

SSB TRANSMITTING CONVERTERS



FEATURES:
- Linear Converter for SSB, CW, FM, etc.
- A fraction of the price of other units
- 2W p.e.p. output with 1 MW of drive
- Use low power tap on exciter or attenuator pad
- Easy to align with built-in test points

Frequency Schemes Available:

MODEL	INPUT(MHz)	OUTPUT(MHz)
XV2-1	28-30	50-52
XV2-2	28-30	220-222
XV2-3	28-30	222-224
XV2-4	28-30	144-146
XV2-5	28-29	145-146
XV2-6	26-28	144-146

ONLY $59.95!

VHF RECEIVING CONVERTERS

LET YOU RECEIVE OSCAR AND OTHER EXCITING SIGNALS ON YOUR PRESENT HF RECEIVER!

MODEL	RF RANGE	I-F RANGE
C28	28-32MHz	144-148MHz
C50	50-52	28-30
C144	144-146	28-30
C145	145-147	28-30
C146	146-148	28-30
C110	Aircraft	26-30
C220	220-222	28-30
C222	222-224	28-30
Special	Inquire About Other Ranges	

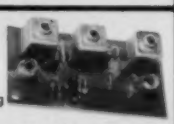
ONLY $34.95

FAMOUS HAMTRONICS PREAMPS

let you hear the weak ones!

Great for OSCAR, SSB, FM, ATV. Over 10,000 in use throughout the world on all types of receivers.

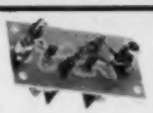
P9 Kit $12.95
P14 Wired $24.95
Specify Band When Ordering



- Deluxe vhf model for applications where space permits
- 1-1/2 x 3"
- Models avail to cover any 4 MHz band in the 26-230 MHz range
- 12 Vdc
- 2 stages
- Ideal for OSCAR
- 20 db gain
- Diode transient protection
- Easily tunable

P8 Kit $10.95
P16 Wired $21.95
Specify Band

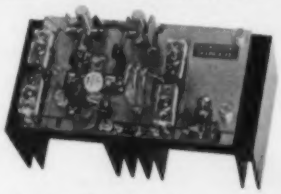
- Miniature vhf model for tight spaces - size only 1/2x2-3/8
- Models avail to cover any 4 MHz band in the range 20-230 MHz
- 20 db gain
- 12V



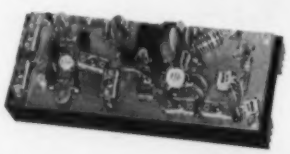
P15 Kit $18.95
P35 Wired $34.95
- Covers any 6 MHz band in UHF range of 380-520 MHz
- 20 dB gain
- 2 stages
- Low noise

VHF Linear PA's

- Use as Linear or Class C PA's
- For XV-2 Xmtg Converters, T50 Exciters, or any 2W Exciter



LPA 2-15 Kit $59.95
- 15W out (linear) or 20W (class C)
- Solid State T/R Switching
- Models for 6M, 2M, or 220 MHz

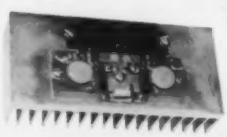


LPA 2-45 Kit $109.95
- 45W out (linear) or 50W (class C)
- Models for 6M or 2M

LPA 8-45 Kit $89.95
For 2M, 8-10W in, 45W out

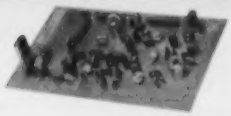
T80 UHF POWER AMP

- Broadband PA
- No Tuning Required
- Class C PA
- 430-470 MHz
- 13-15W Out
- 200 mW Drive



Model T80-450
$79.95
Wired & Tested

UHF RECEIVING CONVERTERS



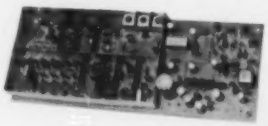
MODEL	RF RANGE	I-F RANGE
C432-2	432-434	28-30MHz
C432-4	432-436	144-146
C432-5	435-437	28-30
C432-7	427.25	61.25
C432-9	439.25	61.25
Special	Inquire About Other Ranges	

ONLY $34.95

A9 Extruded Alum Case with BNC's for above Converters (Optional) ... $12.95

VHF&UHF FM RECEIVERS

- NEW GENERATION RECEIVERS
- MORE SENSITIVE
- MORE SELECTIVE (70 or 100 dB)
- COMMERCIAL GRADE DESIGN
- EASY TO ALIGN WITH BUILT-IN TEST CKTS
- LOWER OVERALL COST THAN EVER BEFORE



R70 6-channel VHF Receiver Kit for 2M, 6M, 10M, 220 MHz, or com'l bands..... $69.95
Optional xtal filter for 100 dB adj chan 10.00

R90 UHF Receiver Kit for any 2 MHz segment of 380-520 MHz band..... $89.95

NEW FM/CW EXCITER KITS

BUILD UP YOUR OWN GEAR FOR MODULAR STATIONS, REPEATERS, & CONTROL LINKS
- Rated for Continuous Duty
- Professional Sounding Audio
- Built-in Testing Aids

T50 Six Channel, 2W Exciter for 2M, 6M, or 220 MHz (Specify band)..... $49.95

T50U Six Channel, 1W Exciter for 430-450 MHz uhf operation $49.95

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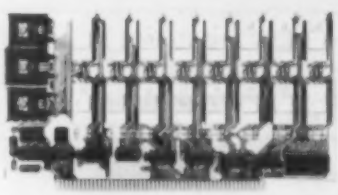
--Dealer Inquiries Invited--

16K EPROM CARD-S 100 BUSS



$59.95 KIT

OUR BEST SELLING KIT!

USES 2708's!

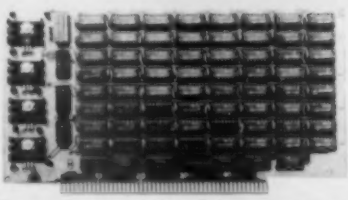
Thousands of personal and business systems around the world use this board with complete satisfaction. Puts 16K of software on line at **ALL TIMES!** Kit features a top quality soldermasked and silk-screened PC board and first run parts and sockets. All parts (except 2708's) are included. Any number of EPROM locations may be disabled to avoid any memory conflicts. Fully buffered and has WAIT STATE capabilities.

OUR 450NS 2708'S ARE $8.95 EA. WITH PURCHASE OF KIT

ASSEMBLED AND FULLY TESTED ADD $25

8K LOW POWER RAM KIT-S 100 BUSS

250 NS SALE!



ADD $5 FOR 250NS!

$129 KIT

Use 21L02 450 NS RAMS!

Thousands of computer systems rely on this rugged, work horse, RAM board. Designed for error-free, NO HASSLE, systems use.

KIT FEATURES:

1. Doubled sided PC Board with solder mask and silk screen layout. Gold plated contact fingers.
2. All sockets included.
3. Fully buffered on all address and data lines.
4. Phantom is jumper selectable to pin 67.
5. FOUR 7805 regulators are provided on card.

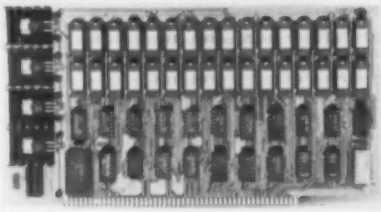
Blank PC Board w/Documentation **$29.95**
Low Profile Socket Set...**13.50**
Support IC's (TTL & Regulators) **$9.75**
Bypass CAP's (Disc & Tantalums) **$4.50**

ASSEMBLED AND FULLY BURNED IN ADD $30

16K STATIC RAM KIT-S 100 BUSS

$295 KIT

FULLY STATIC, AT DYNAMIC PRICES



WHY THE 2114 RAM CHIP?

We feel the 2114 will be the next industry standard RAM chip (like the 2102 was). This means price, availability, and quality will all be good! Next, the 2114 is FULLY STATIC! We feel this is the **ONLY** way to go on the S-100 Buss! We've all heard the HORROR stories about some Dynamic Ram Boards having trouble with DMA and FLOPPY DISC DRIVES. Who needs these kinds of problems? And finally, even among other 4K Static RAM's the 2114 stands out! Not all 4K static Rams are created equal! Some of the other 4K's have **clocked** chip enable lines and various timing windows **just as critical** as Dynamic RAM's. Some of our competitor's 16K boards use these "tricky" devices. But not us! The 2114 is the ONLY logical choice for a trouble-free, straightforward design.

KIT FEATURES:
1. Addressable as four separate 4K Blocks.
2. ON BOARD BANK SELECT circuitry. (Cromemco Standard!) Allows up to 512K on line!
3. Uses 2114 (450NS) 4K Static Rams.
4. ON BOARD SELECTABLE WAIT STATES.
5. Double sided PC Board, with solder mask and silk screened layout. Gold plated contact fingers.
6. All address and data lines fully buffered.
7. Kit includes ALL parts and sockets.
8. PHANTOM is jumpered to PIN 67.
9. LOW POWER: under 2 amps TYPICAL from the +8 Volt Buss.
10. Blank PC Board can be populated as any multiple of 4K.

BLANK PC BOARD W/DATA—**$33**
LOW PROFILE SOCKET SET—**$12** ASSEMBLED & TESTED—**ADD $30**
SUPPORT IC'S & CAPS—**$19.95** 2114 RAM'S—**8 FOR $69.95**

16K STATIC RAM KIT SWTPC (SS-50) 6800 BUSS

USES 2114 4K RAMS!

$295 COMPLETE KIT

WHY PAY MORE FOR FINNICKY DYNAMIC BOARDS?

At last an affordable static RAM board for this popular buss. Quality PC Board with solder mask and silk-screen. Fully buffered with plenty of bypassing for reliable operation. FOUR ON-BOARD REGULATORS.

16K DYNAMIC RAM CHIP

16K X 1 Bits. 16 Pin Package. Same as Mostek 4116-4. 250 NS access. 410 NS cycle time. Our best price yet for this state of the art RAM. 32K and 64K RAM boards using this chip are readily available. These are new, fully guaranteed devices by a major mfg. **VERY LIMITED STOCK!**

8 FOR $89.95

NOT ASSOCIATED WITH DIGITAL RESEARCH OF CALIFORNIA, THE SUPPLIERS OF CPM SOFTWARE.

450 NS! **2708 EPROMS**

Now full speed! Prime new units from a major U.S. Mfg. 450 N.S. Access time. 1K x 8. Equiv. to 4-1702 A's in one package.

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NATIONAL SEMICONDUCTOR

JUMBO CLOCK MODULE

MA1008A BRAND NEW!

$6.95

2 FOR $13

(AC XFMR $1.95)

FEATURES:
- FOUR JUMBO ½ INCH LED DISPLAYS
- 12 HR REAL TIME FORMAT
- 24 HR ALARM SIGNAL OUTPUT
- 50 OR 60 Hz OPERATION
- LED BRIGHTNESS CONTROL
- POWER FAILURE INDICATOR
- SLEEP & SNOOZE TIMERS
- DIRECT LED DRIVE (LOW RFI)
- COMES WITH FULL DATA

ASSEMBLED! NOT A KIT!

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We have a limited number of the 24 HR Real time version of this module in stock.

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MANUFACTURER'S CLOSEOUT!

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TR1602A. PIN FOR PIN SUB FOR AY5-1013 AND TMS6011. FOR SERIAL I/O

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SALE!

1N4148 DIODES. SILICON. Same as 1N914. New, factory prime, Full Leads. **100 FOR $2 1000 FOR $17.50**

New! REAL TIME Computer Clock Chip

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COMPUTER PARTS

Z-80	19.95	8212	2.25
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$4.95 (Complete Kit)

Uses MM5369 CMOS divider IC with high accuracy 3.579545 MHZ Crystal. Use with all MOS Clock Chips or Modules. Draws only 1.5 MA. All parts, data, and PC Board included.

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PNP Silicon. TO-5. House no. VCEO-60V. 3 watts. HFE is 40 to 120 at 150 MA. 100 MHZ.

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MOS CLOCK CHIP WITH 7 SEGMENT AND BCD OUTPUTS

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We bought a load from a very large manufacturer of COM. gear! Please order by part #.

- #5009-011: .7 TO 1.3 UH VARIABLE INDUCTOR (C.T.)
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NOTE: The 5009-011 Variable Inductor can also be used as a 10.7 MHZ I.F. by using a 240 PF CAPACITOR

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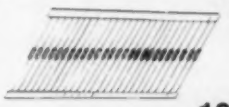

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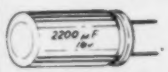

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Please specify voltage and part number when ordering.

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GE Ni-Cad Battery Pack

3 Cell pack, gives 4 volts at 900MAH. Brand new, factory fresh. Each cell is 2/3 "C" size. **$2.95.**

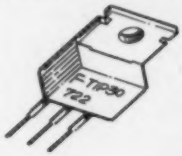
Buy 3 packs (12 volts) for $6.95. Limited stock!

COMPLEMENTARY POWER TRANSISTORS

SILICON NPN AND PNP. TO-220 CASE.

VCEO - 40V PD - 30 WATTS

FOR AUDIO POWER AMPS, ETC.



TIP29 - NPN

TIP30 - PNP

YOUR CHOICE

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MOTOROLA POWER TRIAC

TO-220 CASE

15 AMP 400 PRV

SPECIAL: **89¢ each**

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FAIRCHILD SUPER JUMBO LED READOUT

A full .80 inch character. The biggest readout we have ever sold! Super efficient. Compare at up to $2.95 each from others!

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2N4402. TO-92 Plastic. Silicon PNP Driver. High Current. VCEO-40 HFE-50 to 150 at 150 MA. FT-150 MHZ. A super "BEEFED—UP" Version of the 2N3906.

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#FLV5057. Medium Size. Clear Case. RED EMITTING. These are not retested off-spec units as sold by some of our competition. These are factory prime, first quality, new units.

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We do not know what these boards were used in, but they do contain a wealth of quality components. Board has: 2-12VDC 200 OHM SPDT Mini Relays, 1-CD4001 CMOS, 4-LM358 High Performance OP AMPS (same as 1/2 LM324), 1-MOTOROLA MC3340 Mini Dip, 1-Audio Output Transformer, 1-TIP30 30 WATT PNP Power Transistor, plus 70 more assorted components. All parts easily removed.

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QUESTION: WHAT'S BETTER THAN AN MA1003 CLOCK MODULE? ANSWER: AN MA1003 IN A BEAUTIFUL CASE . . . FOR ONLY $19.95!

That's right, not just the module — but module **and** case — for **$19.95.** The MA1003 has blue-green flourescent readouts, a highly accurate built-in timebase (excellent for mobile applications and/or battery backup), and easy assembly: add 12 Volts DC with 3 time-setting switches and you're ready to go.

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Here's your chance to get a good-looking, easy to assemble clock . . . we've made it really simple for you.

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2102L-1 (high speed/low power) **1K static RAMs are now only 99¢.** Sorry, this price is only good on orders of 10 or more ICs.

1N571A zeners (5.1V) now available at **6/$1.** Stock up while the getting's good.

"BARE BOARD" HEATH MEMORY SPECIAL

Don't need the full 12K of our standard H8 compatible memory board? Then check this out: we'll sell you the bare board, mounting bracket, edge connector, and print for only **$35.** Remember, this is a quality board — solder masked, legended, and double-sided. Populate it with readily available, low lost 2102s to build your memory up to full 12K whenever your budget permits full expansion.

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Cost-effective, low power, reliable memory . . . backed with a 1 year warranty. Available as **unkits** (sockets, bypass caps pre-soldered in place for easy assembly), **assembled/tested,** or qualified under the **Certified System Component** (CSC) program. CSC boards are burned-in for 200 hours and immediately replaced if failure occurs within 1 year of invoice date.

Name	Storage	Design	Buss	Guar. Speed	Unkit	Assm	CSC
ECONORAM II™	8K X 8	static	S-100	2 MHz	**$139**	**$159**	N/A
ECONORAM IV™	16K X 8	static	S-100	4 MHz	**$279**	**$314**	**$414**
ECONORAM VI™	12K X 8	static	H8	2 MHz	**$200**	N/A	N/A
ECONORAM VII™	24K X 8	static	S-100	4 MHz	**$445**	**$485**	**$605**
ECONORAM X™	32K X 8	static	S-100	4 MHz	**$599**	**$649**	**$789**
ECONORAM IX™	32K X 8	static	DigGrp	4 MHz	**$649**	N/A	N/A
ECONORAM XI™	32K X 8	static	SBC	4 MHz	N/A	N/A	**$1050**

TRS-80 CONVERSION KIT $109 (3/$320)

Our kit includes DIP shunts, 250 ns chips for 4 MHz operation, and 1 year guarantee. Upgrades 4K TRS-80 to 16K or populates Memory Expansion Module — our novice level instructions show you how. **Also suitable for APPLE computers.**

FREE CATALOGUE: No one ever said our flyer has a great plot, but what a cast of characters! Linears, CMOS, low power Schottky TTL, standard TTL, specials, music kits, power supplies, and much more cavort (in glorious black and white) on 40 pages of the cheapest paper we could find. If you're looking for bargains, this is the place. Send us your name and address, we'll take care of the rest. For 1st class delivery add 41¢ in stamps.

TERMS: Orders under $15 add $1 handling. Cal res add tax. VISA®/Mastercharge® ($15 min) call (415) 562-0636, 24 hrs. Allow 5% shipping, excess refunded. COD OK with street address for UPS.

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REMOTE CONTROL TRANSMITTER & RECEIVER

- CAN BE USED AS REMOTE CONTROL FOR TV
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- TRANSMITS BETWEEN 30MHz AND 61.5MHz
- THOUSANDS OF USES FOR REMOTE CONTROL APPLICATIONS
- TRANSMITTER USES A 12V BATTERY
- SCHEMATIC INCLUDED

$19.95

Custom Cables & Jumpers

DB 25 Series Cables

Part No.	Cable Length	Connectors	Price
DB25P-4-P	4 Ft.	2-DP25P	$15.95 ea.
DB25P-4-S	4 Ft.	1-DP25P/1-25S	$16.95 ea.
DB25S-4-S	4 ft.	2-DP25S	$17.95 ea.

Dip Jumpers

DJ14-1	1 ft.	1-14 Pin	$1.59 ea.
DJ16-1	1 ft.	1-16 Pin	1.79 ea.
DJ24-1	1 ft.	1-24 Pin	2.79 ea.
DJ14-1-14	1 ft.	2-14 Pin	2.79 ea.
DJ16-1-16	1 ft.	2-16 Pin	3.19 ea.
DJ24-1-24	1 ft.	2-24 Pin	4.95 ea.

For Custom Cables & Jumpers, See JAMECO 1979 Catalog for Pricing

CONNECTORS

25 Pin-D Subminiature

DB25P (as pictured)	PLUG (Meets RS232)	$2.95
DB25S	SOCKET (Meets RS232)	$3.50
DB51226-1	Cable Cover for DB25P or DB25S	$1.75

PRINTED CIRCUIT EDGE-CARD

156 Spacing-Tin-Oxidize Read-Out — Bifurcated Contacts — Fits .054 to .070 P.C. Cards

15/30	PINS (Solder Eyelet)	$1.95
18/36	PINS (Solder Eyelet)	$2.49
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50/100 (.100 Spacing)	PINS (Wire Wrap)	$6.95
50/100 (.125 Spacing)	PINS (Wire Wrap) RBB1-1	$5.95

MINI-BUZZER

- Thousands of applications
- Operates on +6 to +9 VDC
- Output Frequency 800 Hz
- Draws only 15 MA @ 600 ohms
- Size: 1¼" x ⅝"

PART NO. MB-1

1-24	25-49	50-99
$1.95 ea	$1.75 ea	$1.49 ea

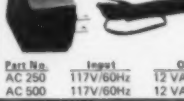
SONALERT® AUDIBLE SIGNAL DEVICE

"Use as a warning Device or Audible Reminder"

- Turns on and off with low power transistor, SCR or IC
- Can be battery operated 6-28 volts
- Solid State - No moving parts.
- Panel mounts in 1.25" round hole
- Black Plastic case includes MTG. hdl.
- Operating Volts (DC): 6 (Min) – 28 (Max)
- Current MA: 3 (Min) – 14 (Max)
- dBA: 68 (Min) – 80 (Max)
- Frequency: 2900Hz ±500

#SC620 $7.50 each

AC Wall Transformer



Ideal for use with clocks, power supplies or any other type of AC application.

Part No.	Input	Output	Price
AC 250	117V/60Hz	12 VAC 250mA	$3.95
AC 500	117V/60Hz	12 VAC 500mA	$4.95

Regulated Power Supply

- Uses LM 309K
- Heat sink provided
- P.C. board construction
- Provides a solid 1 amp @ 5V
- Includes components, hardware and instructions
- Sizes: 3-1/2" x 5" x 2" high

JE200 $14.95

INSTRUMENT/CLOCK CASE

This case is an injection molded unit that is ideal for uses such as DVM, COUNTER, or CLOCK cases. It has dimensions of 4¼" in length by 4" in width by 1-9/16" in height. It comes complete with a red bezel.

PART NO: IN-CC $3.49 each

MICROPROCESSOR COMPONENTS

6800A/6800A SUPPORT DEVICES

6800A	CPU	$ 9.95
6810	8-Bit Input/Output	3.25
6814	Priority Interrupt Control	5.95
6216	Bi-Directional Bus Driver	3.49
6234	Clock Generator/Driver	3.95
6226	Bus Driver	3.49
6328	System Controller/Bus Driver	5.95
6238	System Controller	5.95
6301	Prog. Comm. I/O (UART)	7.95
6253	Prog. Interval Timer	14.95
6255	Prog. Periph. I/O (PPI)	9.95
6257	Prog. DMA Control	19.95
6259	Prog. Interrupt Control	19.95

6800/6500 SUPPORT DEVICES

MC6800	MPU	$14.95
MC6802CP	MPU with Clock and Ram	24.95
MC6810AP1	128X8 Static Ram	5.95
MC6821	Periph. Inter. Adapt (MC6820)	7.49
MC6828	Priority Interrupt Controller	12.95
MC6830L8	1024X8 Bit ROM (MC6830-8)	14.95
MC6850	Asynchronous Comm. Adapter	7.95
MC6852	Synchronous Serial Data Adapt.	9.95
MC6860	0-600 bps Digital MODEM	12.95
MC6862	2400 bps Modulator	14.95
MC6880A	Quad 3-State Bus. Trans. (MC8T26)	2.25

MICROPROCESSOR CHIPS—MISCELLANEOUS

Z80(TM)C	CPU	$19.95
Z80A(TM)-1	CPU	24.95
COP1802	CPU	19.95
2650	MPU	19.95
6935	8-Bit MPU w/clock, RAM, 1/0 Lines	19.95
P8080	CPU	19.95
TMS9900JL	16-Bit MPU w/hardware, multiply & divide	49.95

SHIFT REGISTERS

MM5009H	Dual 25 Bit Dynamic	$.59
MM5009H	Dual 50 Bit Dynamic	.59
MM5004H	Dual 16 Bit Static	.59
MM5006H	Dual 100 Bit Static	.59
MM5018H	Dual 64 Bit Accumulator	.99
MM5016H	500/512 Bit Dynamic	.99
2504T	1024 Dynamic	3.95
2518	Hex 32 Bit Static	4.95
2537	Dual 132 Bit Static	2.95
2524	512 Static	.99
2525	1024 Dynamic	2.99
2527	Dual 256 Bit Static	2.95
2528	Dual 250 Static	4.99
2529	Dual 240 Bit Static	4.00
2532	Quad 80 Bit Static	2.99
2533	1024 Static	2.95
3341	Fifo	9.95
74LS670	4X4 Register File (TriState)	1.95

UART'S

A-Y-5-1013	30K BAUD	5.95

MICROPROCESSOR MANUALS

M-280	User Manual	$7.50
M-COP1802	User Manual	7.50
M-2650	User Manual	5.00

ROM'S

2513(2140)	Character Generator(upper case)	29.95
2513(3621)	Character Generator(lower case)	9.95
2316	Character Generator	19.95
MM5328N	2048-Bit Read Only Memory	1.95

RAM'S

1101	256X1 Static	$1.49
1103	1024X1 Dynamic	.99
2101(9101)	256X4 Static	3.95
2102	1024X1 Static	1.75
2112L02	256X4 Static	1.95
2114	1024X4 Static 450ns	9.95
2114L	1024X4 Static 450ns low power	10.95
2114-3	1024X4 Static 300ns	10.95
2114L-3	1024X4 Static 300ns low power	11.95
2125	256X4	7.95
5290-2107	4096X1 Dynamic	4.95
7489	16X4 Static	1.75
74S289	256X1 Static Tristate	4.95
93421	256X1 Static	2.95
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TMS4044-45NL	4K Static	14.95
TMS4046	1024X4 Static	14.95
2117	16,384X1 Dynamic 300ns (Sousa market)	9.95
MM5262	8KX1 Dynamic	4/1.99

PROM'S

1702A	256X8	FAMOS	$9.95
TMS2516 (2716)	16K* EPROM(Intel 2716)	Fully TTL	49.95
TMS2532	4K32 EPROM		69.95
2708	8K EPROM		19.95
2716 T.I	16K** EPROM		29.95

*Requires single +5V power supply
**Requires 3 voltages, —5V, +5V, +12V

5203	32X8	FAMOS	14.95
6301-1(7611)	256X4	Tristate Bipolar	3.49
6330-1(7680)	256	Open C Bipolar	2.95
82S23	32X8	Open Collector	3.95
6331/5	4096	Bipolar	19.95
6331/3	32X8	Tristate	3.95
74188	512	TTL Open Collector	9.95
74188	256	TTL Open Collector	3.95
74S287	1024	Static	2.95

The Incredible "Pennywhistle 103"

$139.95 Kit Only

The Pennywhistle 103 is capable of recording data to and from audio tape without critical speed requirements for the recorder and it is able to communicate directly with another modem and terminal for telephone "hamming" and communications. In addition, it is free of critical adjustments and is built with non-precision, readily available parts.

Data Transmission Method	Frequency-Shift Keying, full-duplex (half-duplex selectable)
Maximum Data Rate	300 Baud
Data Format	Asynchronous Serial (return to mark level required between each character)
Receive Channel Frequencies	2805 Hz for space, 2225 Hz for mark.
Transmit Channel Frequencies	Switch selectable. Low (normal) = 1070 space, 1270 mark; High = 925 space, 2225 mark.
Receive Sensitivity	-46 dbm automatically coupled.
Transmit Level	-15 dbm nominal. Adjustable from -6 dbm to -20 dbm.
Receive Frequency Tolerance	Frequency reference automatically adjusts to allow for operation between 1800 Hz and 2400 Hz.
Digital Data Interface	EIA RS-232C or 20 mA current loop (receiver is optoisolated and non-polar)
Power Requirements	120 VAC, single phase; 10 Watts.
Physical	All components mount on a single 5" by 9" printed circuit board. All components included.

Requires a VOM, Audio Oscillator, Frequency Counter and/or Oscilloscope to align.

TRS-80 16K Conversion Kit

Expand your 4K TRS-80 System to 16K. Kit comes complete with:

* 8 each UPD416 (16K Dynamic Rams)
* Documentation for conversion

TRS-16K $115.00

Special Offer - Order both your TRS-16K and the Sup'R' MOD II Interface kit together (retail value $144.95) **for only $139.95**

COMPUTER CASSETTES

- 6 EACH 15 MINUTE HIGH QUALITY C-15 CASSETTES
- PLASTIC CASE INCLUDED 12 CASSETTE CAPACITY
- ADDITIONAL CASSETTES AVAILABLE #C-15-$2.50 ea

CAS-6 $14.95

(Case and 6 Cassettes)

NEW!! IN STOCK... POWERACE

ALL-CIRCUIT EVALUATORS WITH POWER

- 1680 solderless, plug-in tie points...will hold up to 18 14-pin DIP's.
- Breadboard elements accept all DIP sizes...including RTL, DTL, TTL and CMOS devices. TO-5's and discretes with leads up to .032" dia.
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- Interconnect with any solid 20 to 30 AWG wire.
- Breadboard elements are mounted on ground planes...ideal for high-frequency and high-speed/low-noise circuits.
- Short-circuit-proof fused power supplies.
- Operate on 110 to 130 VAC at 60 Hz
- Epoxy-age permanent. Styling and high-grade components permit convenient, organized and quick prototyping.
- All models are 7.5" wide 11.5" deep and 4.0" high (rear) 0.75" high (front) and weigh approx. 2.5 lbs.

POWERACE 101 -General purpose model for prototyping all types of circuit.
#923161 $ 84.95

POWERACE 102 -Complete digit prototyping lab with built-in logic probe
#923162 $114.95

POWERACE 103 -Triple-output power supply for prototyping both linear and digit circuits.
#923163 $124.95

SUP 'R' MOD II

UHF Channel 33 TV Interface Unit Kit

Wide Band B/W or Color System

* Converts TV to Video Display for home computers, CCTV camera, Apple II, works with Cromaco Dazzler, SOL-20, IRS-80, Challenger, etc.
* MOD II is preturned to Channel 33 (UHF).
* Includes coaxial cable and antenna transformer.

MOD II $29.95 Kit

RS-232 CONTROL CENTER

Plug in your modem, computer prom programmer, terminal, printer, etc. and selectively control data flow.

- Same Contour as "Pennywhistle 103"
- Totally self-contained
- Includes 2 master ports and 3 slave ports

PART NO. RS-232CC $89.95 kit only

CASSETTE CONTROLLER

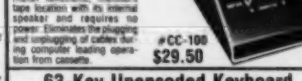
Ideal for use with the TRS 80 and others.

"Plug/Jack interface to any computer system requiring remote control of cassette functions"

The CC100 controls cassette motor functions, monitors tape location with its internal speaker and requires no power. Eliminates the plugging and unplugging of cables during computer loading operation from cassette.

#CC-100 $29.50

63-Key Unencoded Keyboard

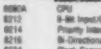


This is a 63-key, terminal keyboard newly manufactured by a large computer manufacturer. It is unencoded with SPST keys, unattached to any kind of PC board. A very solid molded plastic 13 x 4" base suits most application. IN STOCK **$29.95/each**

Hexadecimal Unencoded Keypad

19-key pad includes 1-10 keys, ABCDEF and 2 optional keys and a shift key. **$10.95/each**

Mini-Max 6 Digit 50MHz Frequency Counter



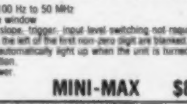
- Guaranteed frequency range of 100 Hz to 50 MHz
- Full 6 digit display with antiglare window
- Fully-automatic-range, polarity- slope, trigger- input level switching not required.
- Lead-zero blanking—All zeros to the left of the first non-zero digit are blanked. Kilo Hertz and Mega Hertz decimal points automatically light up when the unit is turned on.
- Built in input overvoltage protection.
- Use 9V Battery or 110/220V power.
- Complete with mini antenna.
- Lightweight — Only 8oz.

MINI-MAX $89.95

Accessories For Mini-Max

Part No.	Description	Price
MM-A4	Antenna	$ 3.95
MM-C5	Carrying case	5.95
MM-IPC	Input cable with clip leads	3.95
MM-AC1	110V adapter	9.95
MM-AC3	220V adapter	9.95

100 MHz 8-Digit Counter



- 20 Hz-100 MHz Range
- .6" LED Display
- Crystal-controlled timebase
- Fully Automatic
- Portable — completely self-contained
- Size — 1.79" x 7.38" x 5.63"
- Four power sources, i.e. batteries, 110 or 220V with charger 12V with auto lighter adapter and external 7.2-10V power supply

MAX-100 $134.95

ACCESSORIES FOR MAX 100:

Mobile Charger Eliminator use power from car battery — Model 100 — CLA $3.95

Charger/Eliminator use 110 V AC — Model 100 — CAI $9.95

3½-Digit Portable DMM

- Overload Protected
- .3" high LED Display
- Battery or AC operation
- Auto Zeroing
- 1mv, 1Va, 0.1 ohm resolution
- Overrange reading
- 10 meg input impendence
- DC Accuracy 1% typical

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Model 2800 $99.95

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☐ 20	15	9 for $1	18 for $1.01
☐ 20	25	8 for $1	16 for $1.01
☐ 20	50	6 for $1	12 for $1.01
☐ 50	25	4 for $1	8 for $1.01
☐ 100	15	3 for $1	6 for $1.01
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All PC type except for noted *Axial

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	$ .10	$ .10	Type	Sale	2 For
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☐ SN7406	.29	.30	☐ SN7474	.35	.36
☐ SN7410	.18	.10	☐ SN7480	.30	.31
☐ SN7420	.30	.31	☐ SN7486	.55	.56
☐ SN7426	.29	.30	☐ SN74164	.89	.90
☐ SN7437	.25	.26	☐ SN74165	.89	.90
☐ SN7440	.30	.31	☐ SN74181	.89	.90
☐ SN7450	.30	.31	☐ SN74182	.79	.80
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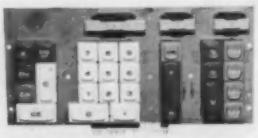

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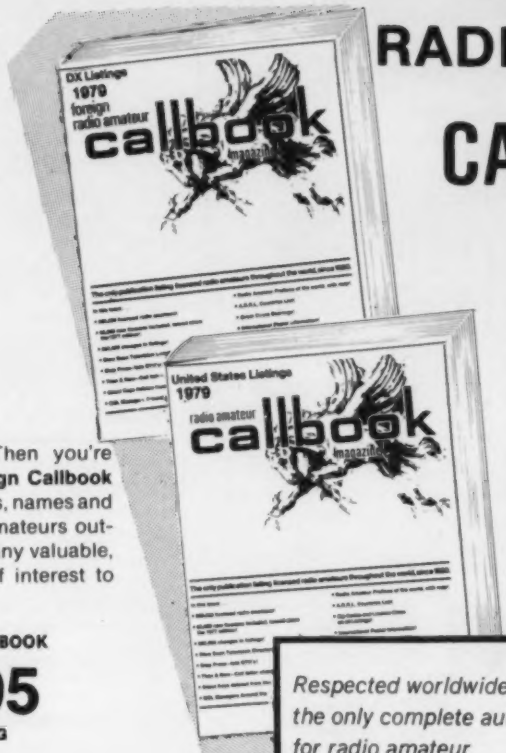

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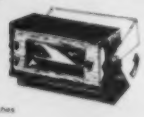

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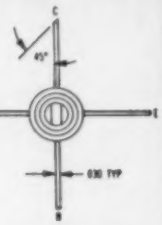

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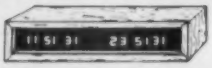

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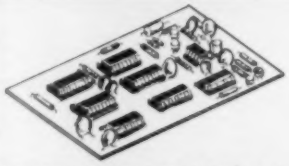

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1N758A	10v	"	.25
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1N5243	13v	"	.25
1N5244B	14v	"	.25
1N5245B	15v	"	.25

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4010	.35
4011	.20
4012	.20
4013	.40
4014	.75
4015	.75
4016	.35
4017	.75
4018	.75
4019	.35
4020	.85
4021	.75
4022	.75
4023	.20
4024	.75
4025	.20
4026	1.95
4027	.35
4028	.75
4029	1.15
4030	.30
4033	1.50
4034	2.45
4035	.75
4037	1.80
4040	.75
4041	.69
4042	.65
4043	.50
4044	.65
4046	1.25
4048	.95
4049	.45
4050	.45
4052	.75
4053	.75
4066	.55
4069/74C04	.35
4071	.25
4081	.30
4082	.30
4507	.95
4511	.95
4512	1.10
4515	2.95
4519	.85
4522	1.10
4526	.95
4528	1.10
4529	.95
MC 14409	14.50
MC 14419	4.85
74C151	1.50

LINEARS, REGULATORS, etc.

QTY.		QTY.		QTY.	
MCT2	.95	LM323K	5.95	LM380 (8-14 Pin)	1.19
8038	3.95	LM324	1.25	LM709 (8-14 Pin)	.35
LM201	.75	LM339	.75	LM711	.45
LM301	.45	7805 (340T5)	.95	LM723	.40
LM308	.85	LM340T12	.95	LM725	2.50
LM309H	.65	LM340T15	.95	LM739	1.50
LM309K (340K-5)	1.50	LM340T18	.95	LM741 (8-14)	.35
LM310	.85	LM340T24	.95	LM747	1.10
LM311D	.75	LM340K12	1.25	LM1307	1.25
LM318	1.75	LM340K15	1.25	LM1458	.65
LM320H6	.79	LM340K18	1.25	LM3900	.50
LM320H15	.79	LM340K24	1.25	LM75451	.65
LM320H24	.79	LM373	2.95	NE555	.45
7905 (LM320K5)	1.65	LM377	3.95	NE556	.85
LM320K12	1.65	78L06	.75	NE565	.95
LM320K24	1.65	78L12	.75	NE566	1.25
LM320T5	1.65	78L15	.75	NE567	.95
LM320T12	1.65	78M05	.75		
LM320T15	1.65				

— TTL —

QTY.		QTY.		QTY.		QTY.	
7400	.10	7482	.75	74221	1.90	74LS02	.30
7401	.15	7483	.75	74367	.95	74LS04	.30
7402	.15	7485	.55	75108A	.35	74LS05	.35
7403	.15	7486	.25	75491	.50	74LS08	.35
7404	.10	7489	1.05	75492	.50	74LS09	.35
7405	.25	7490	.45	74H00	.15	74LS10	.35
7406	.25	7491	.70	74H01	.20	74LS11	.35
7407	.55	7492	.45	74H04	.20	74LS20	.30
7408	.15	7493	.35	74H05	.20	74LS21	.35
7409	.15	7494	.75	74H08	.35	74LS22	.35
7410	.15	7495	.60	74H10	.35	74LS32	.35
7411	.25	7496	.80	74H11	.25	74LS37	.35
7412	.25	74100	1.15	74H15	.45	74LS38	.45
7413	.25	74107	.25	74H20	.25	74LS40	.40
7414	.75	74121	.35	74H21	.25	74LS42	.75
7416	.25	74122	.55	74H22	.40	74LS51	.45
7417	.40	74123	.35	74H30	.20	74LS74	.45
7420	.15	74125	.45	74H40	.25	74LS76	.50
7426	.25	74126	.35	74H50	.25	74LS86	.45
7427	.25	74132	.75	74H51	.25	74LS90	.65
7430	.15	74141	.90	74H52	.15	74LS93	.65
7432	.20	74150	.85	74H53	.25	74LS107	.50
7437	.20	74151	.65	74H55	.20	74LS123	1.20
7438	.20	74153	.75	74H72	.35	74LS151	.85
7440	.20	74154	.95	74H74	.35	74LS153	.85
7441	1.15	74156	.70	74H101	.75	74LS157	.85
7442	.45	74157	.65	74H103	.55	74LS160	.95
7443	.45	74161	.55	74H106	.95	74LS164	1.20
7444	.45	74163	.85	74L00	.25	74LS193	1.05
7445	.65	74164	.60	74L02	.20	74LS195	.95
7446	.70	74165	1.10	74L03	.25	74LS244	1.70
7447	.70	74166	1.25	74L04	.30	74LS367	.95
7448	.50	74175	.80	74L10	.20	74LS368	.95
7450	.25	74176	.85	74L20	.35	74S00	.35
7451	.25	74180	.55	74L30	.45	74S02	.35
7453	.20	74181	2.25	74L47	1.95	74S03	.25
7454	.25	74182	.75	74L51	.45	74S04	.25
7460	.40	74190	1.25	74L55	.65	74S05	.35
7470	.45	74191	1.25	74L72	.45	74S08	.35
7472	.40	74192	.75	74L73	.40	74S10	.35
7473	.25	74193	.85	74L74	.45	74S11	.35
7474	.30	74194	.95	74L75	.85	74S20	.25
7475	.35	74195	.95	74L93	.55	74S40	.20
7476	.40	74196	.95	74L123	.85	74S50	.20
7480	.55	74197	.95	74LS00	.30	74S51	.25
7481	.75	74198	1.45	74LS01	.30	74S64	.15
						74S74	.35
						74S112	.60
						74S114	.65
						74S133	.40
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						74S257 (8123)	1.05
						8131	2.75

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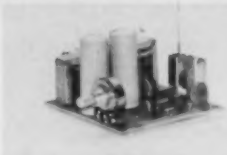

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LM318CN	High Speed Op Amp 50V/μs mDIP	$0.94
LM318D	High Speed Op Amp 50V/μs DIP	.90
LM339N	Quad Comparator Single or Dual Supply	.79
LM380N-8	½W Audio Power Amplifier 8-22V	.90
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1N4007	10/$1	2N3564	5/$1	2N4857*	2/$1	2N5005	$3.00	LM747CN	.65
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XR2206CP	Function Generator with applic. data	4.40
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1 YEAR TIMER	Kit-2 XR2242's and Applic. Note	3.00
LM2901N	Quad Comparator +5V or 2 to 36VDC	$1.20
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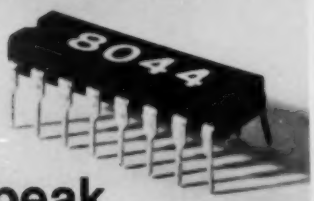

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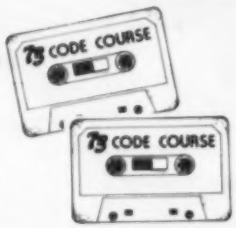

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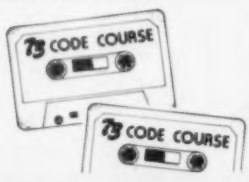

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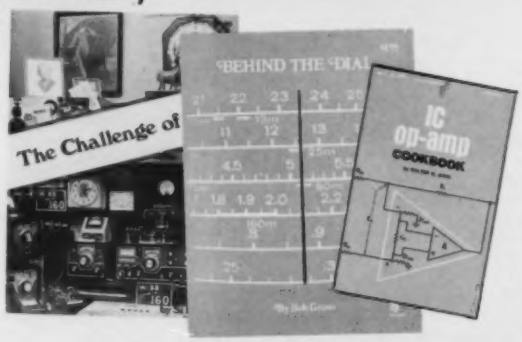

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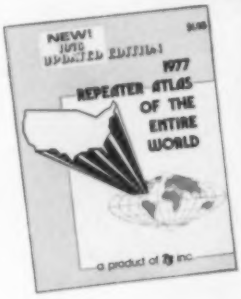

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HAWAII	21A	21A	21	14	7	7	7	7	14	21	21A	21A
INDIA	7B	14A	14	7B	7B	7B	7B	7B	7A	7A	7B	7B
JAPAN	21A	21A	14	7B	7	7	7	7	7	7B	7B	14A
MEXICO	21A	14	7A	7	7	7	7	14	21	21A	21A	21A
PHILIPPINES	21A	21A	14	7B	7B	7B	7B	7	14	14	14B	14
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A = Next higher frequency may also be useful
B = Difficult circuit this period
F = Fair
G = Good
P = Poor
SF = Chance of solar flares

february

sun	mon	tue	wed	thu	fri	sat
				1 G	2 G	3 G
4 G	5 G	6 G	7 F	8 F	9 P	10 F
11 G	12 G	13 G	14 G	15 G	16 P	17 G
18 G	19 F	20 F	21 F	22 P	23 G	24 G
25 G/SF	26 F/SF	27 P/SF	28 P/SF			

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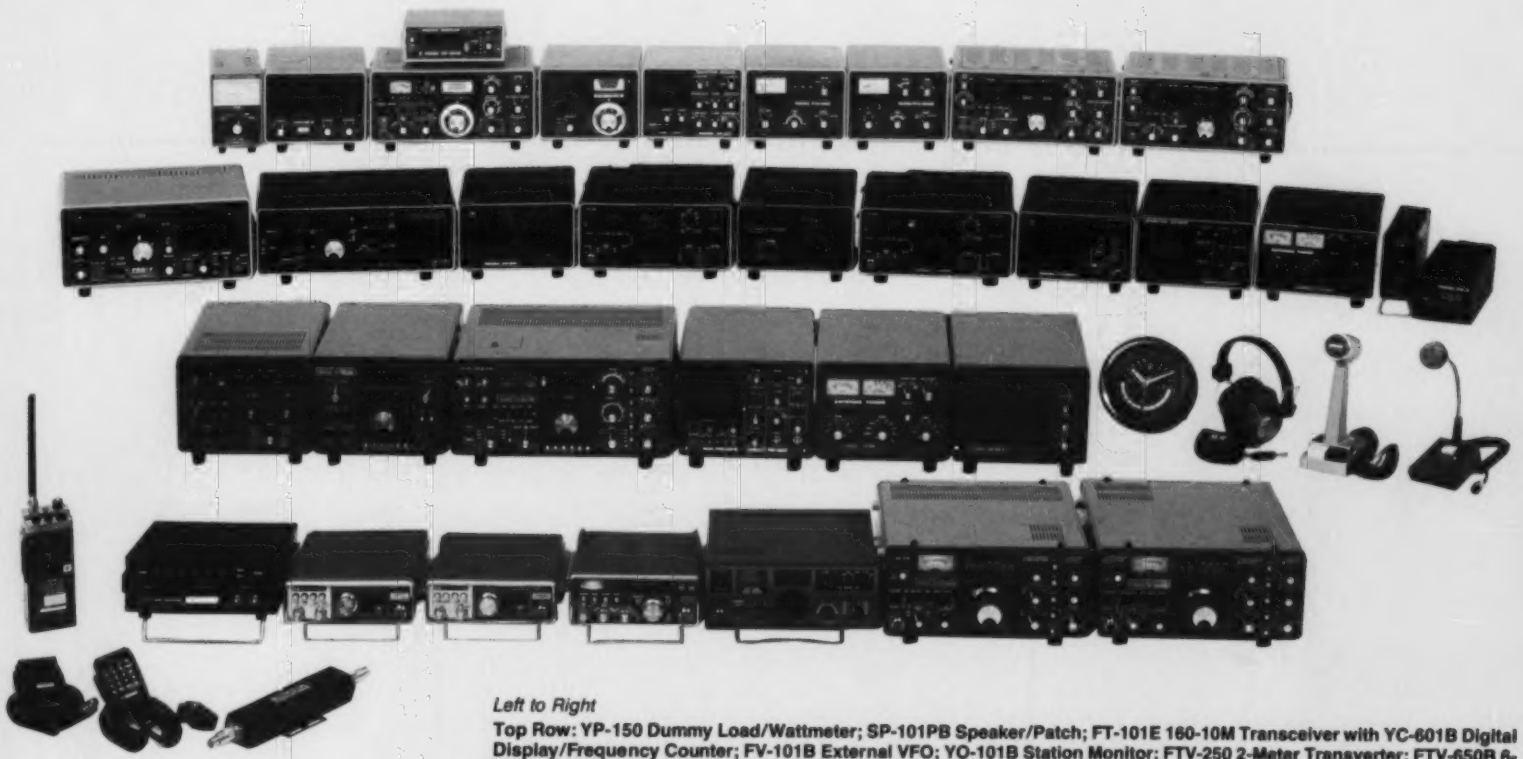

Left to Right

Top Row: YP-150 Dummy Load/Wattmeter; SP-101PB Speaker/Patch; FT-101E 160-10M Transceiver with YC-601B Digital Display/Frequency Counter; FV-101B External VFO; YO-101B Station Monitor; FTV-250 2-Meter Transverter; FTV-650B 6-Meter Transverter; FR-101 Digital 160M-10M Receiver; FL-101 All Band Transmitter.

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